XVIII. Contributions to Terrestrial Magnetism.—No. VIII.

By Lieut.-Colonel Edward Sabine, R.A., For. Sec. R.S.

Received June 15,-Read June 18, 1846.

Containing a Magnetic Survey of the Southern Hemisphere between the Meridians of 0° and 125° East, and Parallels of -20° and -70°.

THE Antarctic Expedition, under Captain Sir James Clark Ross, R.N., has furnished the materials for maps of the three magnetic elements in the high latitudes of the southern hemisphere for nearly two-thirds of its circumference. The first and second portions of the results, comprising between the meridians of 125° and 300°, have already been communicated to the Royal Society, and are contained in the Vth and VIth Numbers of these Contributions\*; a third portion, comprehending between the meridians of 300° and 360°, is in preparation and will shortly be laid before the In order to complete the magnetic survey of the high latitudes of the southern hemisphere as far as they are accessible, there remained the portion between the longitudes of 0° and 125°, or thereabouts. The tracks of vessels in the employ of the enterprising merchants, the Messrs. Enderby, had shown that no difficulties of serious importance obstructed the navigation of the ocean in the vicinity of the Antarctic Circle between the meridians specified: and there appeared to be little reason to doubt, that a vessel, despatched from the Cape of Good Hope, might accomplish this remaining portion of the survey in a single season, without encountering any particular risk.

Lieut. CLERK, of the Royal Artillery, had been attached by Lord VIVIAN, Master-General of the Ordnance, to the Magnetic Observatory at the Cape of Good Hope, with the express view of being engaged in a magnetic survey, either of the colony itself, or of such portion of the globe as might be conveniently accessible from it; and on his passage from England to the Cape had had an opportunity of practising with the instruments employed in a magnetic survey conducted on the ocean. The completion of the survey of the high latitudes appeared the most important service which Lieut. Clerk could render to magnetical science; and on its being proposed to him, he most readily undertook it.

In June 1844 the subject was brought under the consideration of the Committee of Physics of the Royal Society, by a letter from myself to Sir John F. W. Herschel, Bart., Chairman of the Committee, accompanied by one addressed by Sir John Herschel to the Committee, expressing his earnest hope that the measures suggested for the

\* Philosophical Transactions, 1843, Art. X., and 1844, Art. VII.

completion of the survey might receive the attention which they appeared to him to merit. These letters were submitted by the Committee to the Council of the Royal Society, with a recommendation that an application should be made by the President and Council to the Lords Commissioners of the Admiralty, to authorize the completion of the southern survey in the manner suggested.

The Board of Admiralty having been pleased to accede to this request, the "Pagoda," a bark of 360 tons, was hired at the Cape of Good Hope by the Admiral commanding on the station, and was fitted for a voyage of some months duration, receiving a complement of four officers and thirty-eight seamen from the flag-ship. Lieut. T. E. L. Moore, of the Royal Navy, who had been one of the officers of Her Majesty's ship Terror in the Antarctic Expedition, and was consequently accustomed to the navigation of the high latitudes, as well as practised in magnetic observations, (having taken a very prominent share in those of Her Majesty's ship Terror, recorded in Nos. V. and VI. of these Contributions,) was selected to command the Pagoda, and instructed to cooperate with Lieut. Clerk, and to give him every assistance and support in the execution of the service on which they were jointly employed. At the time of his appointment, Lieut. Moore was serving in the Caledonia at Lisbon, and some little delay occurred in his recall, and also in his subsequent departure from England, in consequence of which he did not join the Pagoda at the Cape until the 4th of January, when she had been some days ready for sea.

It may be useful to officers desirous of making magnetic observations on board ship, to be acquainted with the precautions which, at the period in question, were deemed desirable for the employment of magnetic instruments on board ship under the most advantageous conditions, and for eliminating the disturbing effects of the ship's iron: a copy of the instructions with which Lieut. Clerk was furnished is therefore subjoined:—

Instructions for Lieut. H. Clerk, R.A., on points connected with the Magnetic Observations on Board Ship.

"1. Influence of the Ship's Iron.—Before the ship is fitted, you had better select, in concert with the naval officer appointed to command her, suitable positions for the standard compass and for your Fox. They should both be on the midship line of the ship; the standard compass sufficiently high to see well over the bulwarks when taking azimuths: the Fox lower for the sake of steadiness: it is generally found convenient to use the Fox a few feet in front of the standard. When the positions have been chosen, have any iron that may be near them removed, (as far as can conveniently be done,) and do not let any fresh iron be placed within at least six feet of either of them.

"When the ship is perfectly ready for sea, take a day for the determination of the effect of the ship's iron on the standard compass. You are already acquainted with the usual process of doing this, and are furnished with the printed instructions issued

by the Admiralty; therefore I do not enter into further details on this point, except to suggest that you should be particularly careful that the ship's boats, davits, &c. are all in the positions they will occupy at sea; and that it will be quite sufficient for your purpose that the deviation should be tried on the sixteen principal points of the compass, instead of on thirty-two, as is sometimes done.

"2. Whilst engaged with the standard compass, have a second compass, of which the compass error (meaning thereby the index error) is known, placed in the gimball table of your Fox, and observe generally (by means of the lubber-line) whether the effect of the ship's iron is nearly the same at the two positions, viz. at the position of the standard compass and at that of the Fox. Observe particularly whether the points of no deviation are the same. It simplifies matters greatly that they should be so, and that at both positions the points of no deviation should be nearly the north and south points. This they will most probably be in a vessel which will not have much iron near either position; but it will be advantageous, when first choosing the positions, to try roughly,—by means of a couple of compasses, one in the proposed position of the standard compass, and the other in that of the Fox,—whether they point alike when the ship's head is either north or south. By interchanging the compasses in these positions, you will prevent any deception which might arise from compass errors.

"The observations which have been described will give you the value of the constants a and b, for the corrections of all the declinations observed on board throughout the voyage, and you will probably find that they will give you work enough for one day.

"3. I shall suppose therefore that you take a second day for the determination of the four constants at the position of the Fox. For this you will require the inclination and intensity with the ship's head on the same sixteen points as before, employing a deflector for the intensity on this occasion, in preference to weights, as more convenient. You will find of course that the points of no deviation with the compass become the points of extreme deviation of the inclination and intensity; for convenience I shall suppose them north and south points. Having completed the observations with the Fox, remove it and observe the horizontal intensity with the head successively north, east, south and west, and north again\*, placing the apparatus for the horizontal intensity on the gimball stand of the Fox. This will give you a and b for that position more satisfactorily than the observations of the Fox; from these latter, with the shore observations, you will have c and d.

"The formulæ applicable to all the proceedings which have been described, will be found in Mr. Smith's Memorandum in No. V. of the Contributions to Terrestrial Magnetism. But besides the induced magnetism to which these formulæ refer, the

<sup>\* &</sup>quot;These are compass points, the compass being supposed in strictness to be placed on the spot of the gimball table; if a compass placed at this spot has been found to agree with the standard compass, the latter gives directly the required azimuth of the ship's head."

iron of a ship is found sometimes to exercise upon its compasses a magnetic influence of a distinct character, to which it may become in some instances desirable to give a separate consideration. This influence may be either from permanent magnetism strictly so called, or from a polarity which is temporarily retained, and undergoes alterations consequent upon changes in the inducing action in which it originated, but following after them at a greater or less interval of time. This additional magnetic force may be represented by additional symbols, P, Q and R, i. e. the force resolved along the principal section of the ship, transversely to it, and in the vertical direction.

"The alterations which the introduction of this force makes in Mr. Smith's formula are stated in a second memorandum now printing in No. VI. of the Contributions, a copy of which will be in your hands before you sail.

"This memorandum furnishes equations by which all the constants may be determined by observations in different magnetic latitudes,—of the horizontal force on the *four* principal points,—and of the dip on the *two* principal, together with the dip and horizontal force observed on shore or on the ice. These are part of the observations already directed.

- "4. The observations described in No. 3 must be repeated on the return to the Cape at the conclusion of the voyage, before any change has been made in the iron of the ship. If polarity due to the inducing action of a higher magnetic latitude has been retained, the observations on the return will be found to differ from those made before you sailed. If the disturbing influence of the ship's iron be solely the effect either of instantly induced magnetism, or of permanent magnetism strictly so called, the observations will agree with those made before the departure of the vessel.
- "5. If in the course of the voyage you should anchor in any port in a high latitude, at Enderby's Land for example, or at the Adelie Land of d'Urville, it will be extremely desirable to repeat the same observations. Whenever a choice exists between the shore and fixed ice, as a place for observation out of the influence of the ship's iron, always prefer the fixed ice.
- "6. The approximate value of a, the most important of the constants, may be obtained on board at any time during the voyage when the weather is sufficiently favourable, by azimuths at the north or south points and at the east or west points for the position of the standard compass, and by the horizontal intensity observed on the north and south points for the position of the Fox. If Hansteen's needles are used for the latter purpose, and n, s, be the number of vibrations at north and south in a certain time, commencing at the same arc, and performed in a nearly uniform temperature, then  $\frac{n}{s} = \tan \lambda$ , and  $\cos 2 \lambda = a \tan \theta$ ; also if  $\Delta =$  the deviation when  $\zeta' = 90^{\circ}$ ,

$$\Delta = 90^{\circ} - 2\lambda$$
.

"7. The horizontal intensity at the north and south points should be observed on

board frequently; those on the north, south, east and west points, occasionally; and the dip and horizontal intensity on shore or on the ice, with corresponding observations on board, as often as possible.

"8. Index Correction.—The most convenient mode of employing Mr. Fox's apparatus at sea being to use it with the face of the circle in one direction only (i. e. east or west, I shall here assume it east), the index correction with the face east must be sought, by a comparison of the Inclinations observed in that position of the instrument on shore and on fixed ice, with the true Inclinations determined with needles whose poles may be reversed and a complete observation made with them. As the index correction is liable to vary as a function of the Inclination, it should be determined in different Inclinations, and for this purpose it will be desirable to obtain at least one determination in a high latitude.

"When observing on shore or on the ice for the index correction with the face east, do not omit to observe with the face west also, as the mean index correction is useful in showing the kind of separation which exists between the centre of gravity and the point of suspension in the needle for which it is determined. Mr. Fox's apparatus is furnished with three needles; one to be used when the poles are required to be reversed; the magnetism of the other two should be preserved from change if possible; it has been found a convenient practice to employ one of the latter always as the mounted needle, and the other as a deflector.

"9. Comparison of the Weights and Deflectors.—Experience has shown that the intensity may be more conveniently and satisfactorily determined on board ship by the use of deflectors than by constant weights.

"It is necessary however that the 'equivalent weights' of the deflectors employed should be carefully ascertained. Besides the table which you will form for this purpose in the manner practised by Mr. Fox, it will be necessary to have comparisons between the angles of deflection produced by the deflectors and the constant weights at the Cape before and after the voyage, and on any opportunity which you may have in a high latitude either on shore or on the ice. You may also get occasional comparisons on board in very favourable weather.

"In the choice of constant weights to be employed during the voyage, use none that give a less angle of deflection than 15°. In the observations at the Cape, as your base station, make a double series (i. e. the same observations repeated on two separate days) both before and after the voyage.

"10. Azimuths.—You will find it a convenient practice to deduce your azimuths from the hour angle, instead of from the altitude, which is the more usual custom. First take the altitudes which will give you the hour angle corresponding to the time by chronometer (at least until you materially change your geographical position); and as soon as you have completed this observation, take the sun's azimuth, noting the time of observation by chronometer; the hour angle will then give you the true azimuth. Blank forms are sent suited to this mode of observation.

- "11. General Remarks.—You cannot do better than follow the admirable example of the Antarctic Expedition, in observing the three magnetic elements on board every day on which the weather will permit you to use the instruments.
- "12. Frequent reference has been made in these instructions to the importance of at least one opportunity of observing on shore or on the ice in a high latitude, for various objects connected with the reduction and correction of the whole body of magnetic observations made during the voyage. If Enderby's Land, or land connected with it, should not be accessible, it is by no means necessary that the ship should *enter* the ice in order to give you the opportunity of landing on a piece of ice of sufficient magnitude. A favourable day being chosen, she may approach the ice sufficiently near, and remain four or five hours, whilst her boat takes you to make the observations and to return.

"If the ice be not 'fixed' you must be careful to detect an azimuthal motion, should there be any, by which the inclination circle might otherwise be removed from the plane of the magnetic meridian without your being aware of it. You will also take care that the magnetic instruments are sufficiently distant from the boat.

"EDWARD SABINE."

"Woolwich."

The Pagoda sailed from the Cape of Good Hope on the 9th of January, proceeding, pursuant to instructions, towards the Antarctic Circle in the meridian of Greenwich. She crossed the 60th parallel in the longitude of 4° east, and being impeded by ice in her direct progress to the southward, coasted its margin to the south-east, and attained her greatest southing on the 10th of February in latitude  $-68^{\circ}$  10' and longitude 35°. She was then according to the chart in the vicinity of the western extremity of Enderby's Land, but from strong south-east gales and the position of the ice was unable to approach it sufficiently even to see the land: from thence she continued a general progress to the eastward, keeping in as high a parallel as the ice and weather permitted. On the 10th of March she had obtained the 96th degree of east longitude in about the 60th degree of latitude, when the season was considered to be so far advanced that it would not be prudent to persevere in the completion of the survey in the high latitudes; and a course was therefore taken for King George's Sound in Australia, where the ship arrived on the 1st of April. During the whole of this voyage observations of the three magnetic elements were made twice in each day, except in extreme circumstances of weather, by Lieut. Moore in the afternoon and Lieut. CLERK in the forenoon, each being furnished with a separate (Fox's) apparatus for the Inclination and Force; and on the arrival of the ship at King George's Sound, the two instruments were found to give an almost identical value for the intensity of the force, the results being by Lieut. Moore's Fox 1.680, and by Lieut. Clerk's 1.688.

After remaining a sufficient time to examine the index and other corrections of the instruments, and to obtain the necessary data for eliminating the effects of the ship's iron on the magnetic results obtained during the voyage, the Pagoda quitted King George's Sound on the 27th of April and returned to the Cape of Good Hope, touching at Mauritius by the way for the purpose of repeating the observations on the influence of the ship's iron. She arrived at the Cape on the 20th of June, having continued the practice of observing the magnetic elements daily on the return passage, in the same manner as in the high latitudes.

The voyage was performed without accident or loss of life, and the crew returned in perfect health, due doubtless in great degree to the supplies of warm clothing and preserved meats, which, by direction of the Admiralty, Lieut. Moore had taken with him from England.

No failure occurred in any of the instruments notwithstanding the continual use in which they were kept by the zeal of the observers. If where so much was so well accomplished it is permissible to feel or to express regret on any account, it can be only that circumstances should have prevented the completion of the survey in the high latitudes as far as the 125th degree of longitude according to the original design, whereby the observations of the magnetic force would have been carried up to the principal axis of the isodynamic oval of 2.00.

On the conclusion of the voyage Lieut. CLERK received directions from the Master-General of the Ordnance to return to Woolwich, for the purpose of completing the reduction of his own observations and those of Lieut. Moore. The following pages contain Lieut. Clerk's report; in which he has also embodied a series of observations on the Inclination and Force with a Fox's apparatus, made in 1844 by Lieut. Alex-ANDER SMITH, R.N., one of the Assistants at the Hobarton Magnetic Observatory, on his passage to Van Diemen Island; and a second series, also of the Inclination and Force, made in 1845 by Lieut. DAYMAN, R.N., of the same observatory, in a passage in the bark "Leander" from Hobarton to the Cape. Both these officers had previously been employed in the Antarctic Expedition under Sir James Clark Ross, and their observations now communicated are a consequence of the zeal which they imbibed, and the practice in the use of instruments which they acquired, in that expedition. Their observations transmitted to the Admiralty were sent to Woolwich for reduction and publication. Lieut. CLERK has also embodied in his report the determinations of the three magnetic elements made by Sir James Ross in the Erebus in 1840 on her passage from the Cape of Good Hope to Kerguelen Island, and thence to Hobarton.

On inspecting the map, it will be seen that the tracks of the Erebus and Prince Regent held about a middle line between the outward and homeward tracks of the Pagoda, and are therefore extremely useful in connecting results which would otherwise have been somewhat too far apart.

Lieut. CLERK has taken the Cape of Good Hope as the base station of the observations of the magnetic force made in the Pagoda. The determinations of the absolute horizontal force made at the observatory at the Cape in February, March, April and May 1845 (page 362 in seq.), which are the last received from that station, give a mean result of 4.482, the mean inclination during the same month being  $-53^{\circ}$  25'.5. Combining these with the determination at Woolwich in No. VII. of these Contributions\*, we have the total force at the Cape in the arbitrary scale 0.993. The ratios determined by Mr. Fox's statical apparatus (page 363 in seq.) by separate needles are 1.000 and 1.006: the value of the total force at the Cape as a base station for the observations of the Pagoda has therefore been taken as 1.000.

As Lieut. Smith did not touch at the Cape on his passage to Hobarton, and as the needle which Lieut. Dayman had employed on his homeward passage was broken at the Cape before observations had been made with it, and consequently before the series between Hobarton and the Cape could be connected with the latter station, it has been necessary to employ Hobarton as the base station of both these series. I have already stated in Nos. V. and VI. of these Contributions, the results of the observations which were made to determine the absolute horizontal force at Hobarton between 1840 and 1844; viz. by Sir James C. Ross in 1840 and 1841, with magnets of fifteen inches in length ; by Lieut. Kay in 1841 and 1842, with magnets of the same length; by Lieut. Kay in 1844 with magnets of twelve inches, and with others of 9·18 and 7·50 inches. I have now to add the results of twenty-four determinations made by Lieut. Kay between November 1844 and September 1845, with magnets of various lengths, as shown in the following table:—

Magnets and their length.			No. of	Horizontal			
Suspended.	Deflecting.	Date.	distances.	force.			
in.	in.						
<b>——</b> 7·50	<b></b> 9·18	Nov. 7, 1844.	3	4.5108			
<b></b> 7·50	<b>——</b> 9·18	Sept. 9, 1845.	3	4:4810			
A 57 3.00	D xv. 3.67	Dec. 7, 1844.	3	4.5316			
A 57 3.00	D xv. 3.67	Dec. 9, 1844.	5	4.5118			
A 57 3.00	D xv. 3.67	Dec. 11, 1844.	5	4.4954			
A 57 3.00	D xv. 3.67	Jan. 12, 1845.	5	4.5058			
A 57 3.00	D xv. 3-67	May 5, 1845.	3	4.4997			
A 57 3.00	D xv. 3.67	Aug.15, 1845.	5	4.4762			
A 57 3.00	D 9 3.67	Aug. 19, 1845.	5	4.5104			
A 57 3.00	D 9 3-67	May 6, 1845.	3	4.5076			
A 57 3.00	A 19 3.02	Aug.20, 1845.	5	4.4905			
A 52 3.00	D xvi. 3.67	Jan. 19, 1845.	3	4.4940			
R 1 3.00	D xvi. 3.67	Aug.28, 1845.	4	4.4970			
I 12 2·45	A 19 3-00	Dec. 13, 1844.	5	4.4954			
I 12 2·45	A 19 3.00	Dec. 13, 1844.	5	4.4899			
I 12 2.45	A 19 3.00	Dec. 15, 1844.	5	4.4865			
I 12 2·45	A 19 3.00	Jan. 14, 1845.	5	4.4809			
I 12 2.45	A 29 3.00	Aug.26, 1845.	5	4.5016			
I 12 2.45	A 23 3.00	Aug. 22, 1845.	5	4.4994			
I 1 2.45	A 23 3.00	Dec. 20, 1844.	3	4.5046			
I 1 2.45	A 23 3.00	Dec. 23, 1844.	3	4.5121			
I 1 2.45	A 23 3.00	Dec. 26, 1844.	5	4.5020			
I 1 2.45	A 23 3.00	Jan. 15, 1845.	5	4.5082			
I 1 2·45	A 23 3-00	May 9, 1845.	3	4.4970			
Mean							

<sup>\*</sup> Philosophical Transactions, 1846, p. 246.

<sup>‡</sup> Ibid. p. 168 (note).

<sup>§</sup> Ibid. 1844, p. 111.

<sup>†</sup> Ibid. 1843, p. 168.

<sup>|</sup> Ibid. p. 112.

Collecting in one view the different mean results, we have

Ross, in 1840-41, 15 in. magnets	•	•			•	•			•		4.573
KAY, in 1841, 15 in. magnets .		•			•		•			•	4.553
Kay, in 1842, 15 in. magnets .			•				•		, .		4.513
KAY, in 1843, 12 in. magnets .	•							•	•		4.520
Kay, in 1843, 9.18 and 7.50 in. m	agı	net	5			•	•		•		4.501
Kay, in 1844-45, magnets of various	ous	ler	gt	hs,	9.1	8 1	to 2	2.45	in i		4.499

These results exhibit (with one exception) a progressive decrease, but between those of 1840-41, and subsequent years, there is a very great difference. The inclination has decreased from  $-70^{\circ}$  40'.7, observed in 1840-41\*, to  $-70^{\circ}$  37'.6, which is the mean of the results obtained twice in each week at the Hobarton Observatory in the first nine months of 1845. Assuming the total force at Hobarton as constant, the horizontal component should have been increased rather than diminished by the small secular change which appears to have taken place in the Inclination. discrepancy between the earlier and later results of the absolute determinations cannot therefore be a consequence of secular change in the Inclination; nor is it probable that the total force should have undergone a decrease of such magnitude. Presuming the results of 1840-41, with the 15-inch magnets, to have been affected with error from some cause as yet unexplained, (possibly from an erroneous value having been taken for the moment of inertia of the magnet,) the subsequent results exhibit only such differences as cannot be regarded as excessive. They have all to undergo recalculation, as Lieut. Kay does not consider the elements of reduction as yet finally determined; and they will all, in common with all the other determinations of the absolute horizontal force given in these Contributions, have to receive a small correction for the difference of the magnetic moment of the deflecting bar, caused by the earth's inducing action in the different positions in which the bar is placed in the experiments of deflection and vibration. If, therefore, we assume provisionally the mean of the four last results, or 4.508, as the best approximation to which we have yet arrived for the horizontal component at Hobarton, and  $-70^{\circ}$  39' as the corresponding Inclination, we have the total force in the arbitrary scale 1.797; and we may hence conclude, that influenced by the earlier determinations (those of 1840-41), the provisional value of the total force at Hobarton, employed in the Vth and VIth Numbers of the Contributions (1.82), was taken too high, and that all the values of the force dependent on Hobarton will require a correction to be applied, in amount about -0.02, before they are combined in the general map of the southern hemisphere. For Lieut. Smith's and Lieut. Dayman's observations, Lieut. CLERK has taken a base value of 1.80 at Hobarton.

A subsequent number of these Contributions will contain the Magnetic Observations of the Erebus and Terror in the summer of 1843-1844, between the meridians

<sup>\*</sup> Philosophical Transactions, 1843, p. 165.

of Cape Horn and of the Cape of Good Hope, which will complete the survey of the high latitudes of the southern hemisphere.

I propose then to combine in one general view the several portions of the southern survey which have been successively communicated; and I shall reserve until that occasion, as more convenient than the present, such general remarks as suggest themselves in reference to the magnetic lines determined in the present Number.

## "1. Calculation of Corrections for the Ship's Local Attraction.

"To obtain the corrections for the observations of the Declination, the deviations of the compass were observed on each of the sixteen principal points at the Cape of Good Hope, King George's Sound, the Mauritius, and again at the Cape on the return of the Expedition. The following are the observations:—

g: 1 1 1	Cape of C	Good Hope.	King George's	Mauritius.
Ship's head.	January.	June.	Sound.	
N. N.N.W. N.W. W.N.W. W.S.W. S.W. S.S.W.	0 12+ 0 57+ 0 08- 0 00 0 13- 0 28- 1 28- 1 06-	0 20+ Not observed. 0 50+ 0 50- 0 15- 0 30- 1 20- 1 25-	0 15+ 0 00 0 20+ 1 40- 1 50- 1 00- 0 15-	0 20+ 0 30+ 0 20- 0 30- 0 50- 1 10- 1 10- 0 50-
S. S.S.E. S.E. E.S.E. E. E.N.E. N.E. N.N.E.	*1 48+ 0 42+ 1 12+ 1 27+ 0 57+ 0 27+ 0 12+ 0 32+	0 18- Not observed. 1 50+ 1 40+ 1 45+ 1 50+ 1 35+ 1 13+	0 50+ 0 55+ 2 20+ 3 10+ 2 40+ 3 10+ 3 30+ 2 35+	0 20+ 1 00+ 1 20+ 0 55+ 1 20+ 0 50+ 1 20+ 1 20+

The + sign denotes a deviation of the north end towards the west.

"The values of  $\theta$  (the Inclination) being as follows, viz.—

Cape of Good Hope . . .  $\theta = -53^{\circ}$  44

King George's Sound . . .  $\theta = -65$  04

Mauritius . . . . . .  $\theta = -53$  56

<sup>&</sup>quot;Report on the Magnetic Observations made in Her Majesty's hired bark Pagoda, from January to June 1845, by Lieut. Henry Clerk of the Royal Artillery.

<sup>&</sup>quot;From these observations we can obtain the values of a and b by the formulæ in No. V. of the Contributions to Terrestrial Magnetism +, which give the following values, viz.—

<sup>\*</sup> This observation is evidently erroneous.

<sup>†</sup> Philosophical Transactions, 1843, Part II. p. 148.

Cape of Good Hope . . . 
$$a=.0148$$
 . . .  $b=.9848$  King George's Sound . . .  $a=.0199$  . . .  $b=1.0040$  Mauritius . . . . . . . . . . .  $a=.0158$  . . . .  $b=.9907$  Mean . . .  $a=.0168$  . . . .  $b=.9932$ 

"The values of a and b can also be obtained by observations of the horizontal intensity on the N., S., E. and W. points alone.

"If the card of the azimuth compass be deflected by another magnet (the small deflectors belonging to the dipping-needle for instance), and if  $v_n$ ,  $v_s$ ,  $v_w$ , and  $v_e$  be the angles of deflection observed on the N., S., W. and E. points respectively, then

$$a \tan \theta = \frac{\csc v_n - \csc v_s}{\csc v_n + \csc v_s}; \quad b = \frac{\csc v_w + \csc v_e}{2 \sqrt{\csc v_w \cdot \csc v_e}}.$$

"The deflections were obtained in this manner at the Cape of Good Hope, and at King George's Sound on the N. and S. points, viz.—

Cape of Good Hope.	King George's Sound.
At N. the deflection = $1\mathring{6}$ 20	At N. the deflection $. = 15^{\circ} 23^{\circ}$
At S = 15 35	At S = $14 \ 06$
Hence $a = \frac{1}{0168}$	And $a = 0.0198$

Agreeing very closely with the values determined above.

"After an inspection of the observations at the several stations, Mr. Archibald Smith has kindly furnished the following Memorandum.

"'The formulæ for the correction of observations of magnetic declination, made on board ship, given in the Vth and VIth numbers of the Contributions, are deduced on the supposition that the soft iron of the ship is symmetrically distributed on each side of the fore and aft vertical section passing through the compass. The deviations observed in the Pagoda by Lieut. Clerk, seem to show that the soft iron was not so distributed in that vessel, and to require for their correction formulæ in which no supposition is made as to the distribution of the iron of the vessel, except that there is no iron very near the compass.

"'Using the notation of the memorandums in Nos. V. and VI. of the Contributions, let  $\varphi$  represent the total magnetic force of the earth at the place of observation,  $\theta$  the inclination,  $\zeta$  the azimuth of the ship's head, reckoning from (magnetic) north to west, and let  $\varphi'$ ,  $\theta'$ ,  $\zeta'$  represent the values of the same quantities, shown by an instrument placed at a fixed position in the vessel, and affected by the attraction of the iron in the vessel.

"'The first three equations in the memorandum in Contribution No. VI. may be transformed into the following, viz.—

$$\varphi \cos \theta \cos \zeta = \varphi' \cos \theta' \{A' \cos \zeta' + B' \sin \zeta'\} + \varphi' \sin \theta' C' + P'. \qquad (1.)$$

$$\varphi \cos \theta \sin \zeta = \varphi' \cos \theta' \{D' \cos \zeta' + E' \sin \zeta'\} + \varphi' \sin \theta' F' + Q'. \qquad (2.)$$

$$\varphi \sin \theta = \varphi' \cos \theta' \{G' \cos \zeta' + H' \sin \zeta'\} + \varphi' \sin \theta' K' + R'. \qquad (3.)$$

"'The coefficients A'B'...R' might, if required, be expressed in terms of the corresponding coefficients of Contribution No. VI. It is here however only important to observe that A'B'C'D'E'F'G'H'K' depend only on the amount and distribution of the soft iron. P'Q'R' depend partly on the amount and distribution of the soft iron, and partly on the amount and distribution of the permanently magnetic iron, and become zero when there is no permanently magnetic iron. If the soft iron is symmetrically distributed on each side of the fore and aft vertical section passing through the compass, B'D'F'H' are equal to zero.

"The above equations are deduced, it must be remembered, on the hypothesis that the soft iron of the vessel receives its full charge of induced magnetism instantly on the vessel assuming a new position, and that the rest of the iron in the vessel is in a permanently magnetic state. On this hypothesis, and supposing that no iron is very near the compass, the equations are accurate, and the coefficients A' B', &c. are constant, and independent of the latitudes. The hypothesis is however evidently not strictly true. The magnetic state of the hard, if not of the soft iron of the vessel, changes with a change of position and with time. In consequence of this, different values of the coefficients are derived from observations made at different places, and at the same place at different times.

"'Careful observations, made in a variety of circumstances and localities, and particularly, (for a reason which will appear in a subsequent part of this Memorandum,) observations made near the line of no dip, when the affected dip is zero, may hereafter throw light on the nature of the change which takes place in the magnetic state of a vessel, and furnish the means of determining the change which the coefficients undergo. In the present Memorandum they are supposed to be constant.

"'From equations (1.) and (2.) the following may be deduced:

$$\sin (\zeta - \zeta') = \frac{\varphi' \cos \theta'}{\varphi \cos \theta} \left\{ \frac{D' - B'}{2} - \frac{A' - E'}{2} \sin 2\zeta' + \frac{B' + D'}{2} \cos 2\zeta' \right\} \\
- \frac{\varphi' \sin \theta' C' + P'}{\varphi \cos \theta} \sin \zeta' + \frac{\varphi' \sin \theta' F' + Q'}{\varphi \cos \theta} \cos \zeta'$$
(4.)

"'This equation is rigorously accurate, on the assumptions which have been made. If  $\varphi'\cos\theta'$  and  $\varphi'\sin\theta'$  were known in terms of  $\varphi$ ,  $\theta$  and  $\zeta'$ , and the coefficients determined by observation, this equation would furnish accurate corrections for observations of Declination. The expression is very much simplified if we may assume  $\theta'=\theta$ , and  $\varphi'=\varphi$ . This assumption may I believe in general be safely made, except in high magnetic latitudes. Making this assumption, we have the following approximate formula,

$$\sin(\zeta - \zeta') = \frac{D' - B'}{2} - \left\{ C' \tan \theta + \frac{P'}{\varphi \cos \theta} \right\} \sin \zeta' + \left\{ F' \tan \theta + \frac{Q'}{\varphi \cos \theta} \right\} \cos \zeta'$$

$$- \frac{A' - E'}{2} \sin 2 \zeta' + \frac{B' + D'}{2} \cos 2 \zeta'$$

$$(5.)$$

"This equation may conveniently be put under the form  $\sin \delta = A + B \sin \zeta' + C \cos \zeta' + D \sin 2\zeta' + E \cos 2\zeta'$ . . . . . . . . (6.)

 $\delta = \zeta - \zeta'$  is the deviation of the compass; B corresponds to the coefficient a tan  $\theta$  of the former memorandum; D to the coefficient 1-b. A, B, C, D, E are coefficients, which are to be determined by observations of deviation made with the ship's head on different azimuths. A, D and E, it will be seen, are independent of the dip, and, to the extent to which the hypothesis above mentioned is correct, will have the same values in different latitudes. B and C depend on the dip, and also on the proportion of the soft to the permanently magnetic iron. This ratio cannot be determined from observations made in one place. If P', Q', C', F' remain constant, they can severally be determined from values of B and C deduced in *two* different latitudes, and the values of B and C in any other latitude may be deduced from the equations

$$\mathbf{B} = -\left\{ \mathbf{C}' \tan \theta + \frac{\mathbf{P}'}{\varphi \cos \theta} \right\} \dots (7.) \qquad \mathbf{C} = \mathbf{F}' \tan \theta + \frac{\mathbf{Q}'}{\varphi \cos \theta} \dots (8.)$$

the accurate values of B and C being

$$\mathbf{B} = -\frac{\varphi' \sin \theta' \mathbf{C}' + \mathbf{P}'}{\varphi \cos \theta'}, \qquad \mathbf{C} = \frac{\varphi' \sin \theta' \mathbf{F}' + \mathbf{Q}'}{\varphi \cos \theta}.$$

If the affected dip is zero, we have

$$R = -\frac{P'}{\phi}, \qquad C = \frac{Q'}{\phi}.$$

So that from observations on the line of no dip, or more accurately when the affected dip is zero, the effect of the permanent magnetism may be obtained.

"'If we distinguish the points of the compass, reckoning from north to west, by the numbers from 1 to 32, north being 0 or 32, and north by west being 1; and if we designate by  $\delta_0$ ,  $\delta_1$ , &c. the westerly deviation when the ship's head is north, or north by west, &c., so that  $\delta_8$  represents the deviation at W.,  $\delta_{16}$  at S.,  $\delta_{24}$  at E., it is evident from the equations that we have at once the following simple expressions for the values of the coefficients:—

$$A = \frac{1}{4} \left\{ \sin \delta_0 + \sin \delta_8 + \sin \delta_{16} + \sin \delta_{24} \right\}. \qquad (9.)$$

$$C = \frac{1}{2} \left\{ \sin \delta_0 - \sin \delta_{16} \right\}. \qquad (11.$$

$$\mathbf{D} = \frac{1}{4} \left\{ \sin \delta_4 - \sin \delta_{12} + \sin \delta_{20} - \sin \delta_{28} \right\}. \qquad (12.)$$

$$E = \frac{1}{4} \left\{ \sin \delta_0 - \sin \delta_8 + \sin \delta_{16} - \sin \delta_{24} \right\}. \qquad (13.)$$

"' More accurate values of the coefficients may be obtained by combining observations of deviation, made with the ship's head on the several points, in the following manner:—

"'1. Suppose the deviation to have been observed on all the thirty-two points. Let MDCCCXLVI. 2 z

 $\zeta'_1, \zeta'_2, \ldots, \zeta'_{32}$  be the observed azimuths, which of course are 11° 15′, 22° 30′, &c. Then we have

$$\sin \delta_{0} = A + C + E$$

$$\sin \delta_{1} = A + B \sin \zeta'_{1} + C \cos \zeta'_{1} + D \sin 2\zeta'_{1} + E \cos 2\zeta'_{1}$$

$$\sin \delta_{2} = A + B \sin \zeta'_{2} + C \cos \zeta'_{2} + D \sin 2\zeta'_{2} + E \cos 2\zeta'_{2}$$

$$&c. &c.$$

$$\sin \delta_{31} = A + B \sin \zeta'_{31} + C \cos \zeta'_{31} + D \sin 2\zeta'_{31} + E \cos 2\zeta'_{31}$$
(14.)

Combining these equations by the method of least squares, we obtain by virtue of a well-known property of circular functions,

$$A = \frac{1}{32} \sum \sin \delta$$

$$B = \frac{1}{16} \sum \sin \delta \sin \zeta'$$

$$C = \frac{1}{16} \sum \sin \delta \cos \zeta'$$

$$D = \frac{1}{16} \sum \sin \delta \sin 2\zeta'$$

$$E = \frac{1}{16} \sum \sin \delta \cos 2\zeta'$$

$$E = \frac{1}{16} \sum \sin \delta \cos 2\zeta'$$

where

$$\Sigma \sin \delta = \sin \delta_0 + \sin \delta_1 \dots + \sin \delta_{31},$$

$$\Sigma \sin \delta \sin \zeta' = \sin \delta_0 \sin \zeta'_0 + \sin \delta_1 \sin \zeta'_1 + \&c. + \sin \delta_{31} \sin \zeta'_{31}$$
&c. &c. &c.

"'If we represent  $\sin \delta_0$ ,  $\sin \delta_1$ , &c. by  $s_0$ ,  $s_1$ , &c., and remember that all the values of  $\sin \zeta'$ ,  $\cos \zeta'$ ,  $\sin 2\zeta'$ ,  $\cos 2\zeta'$  which occur in these formulæ can be represented by the quantities  $s_1$ ,  $s_2$ ,  $s_3$ ,  $s_4$ ,  $s_5$ ,  $s_6$ ,  $s_7$ , we shall find

$$\mathbf{C} = \frac{1}{16} \{s_0 - s_{16}\},$$

$$+ \cdot 0613 (\log = \overline{2} \cdot 78745) \{s_1 + s_{31} - s_{15} - s_{17}\},$$

$$+ \cdot 0577 (\log = \overline{2} \cdot 76149) \{s_2 + s_{30} - s_{14} - s_{18}\},$$

$$+ \cdot 0520 (\log = \overline{2} \cdot 71572) \{s_3 + s_{29} - s_{13} - s_{19}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_4 + s_{28} - s_{12} - s_{20}\},$$

$$+ \cdot 0347 (\log = \overline{2} \cdot 54062) \{s_5 + s_{27} - s_{11} - s_{21}\},$$

$$+ \cdot 0239 (\log = \overline{2} \cdot 37872) \{s_6 + s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0122 (1c^{-} = \overline{2} \cdot 08611) \{s_7 + s_{25} - s_9 - s_{23}\}. \qquad (18.)$$

$$\mathbf{D} = \cdot 0577 (\log = \overline{2} \cdot 76149) \{s_1 - s_{31} - s_{15} + s_{17} + s_7 - s_{25} - s_9 + s_{23}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 - s_{30} - s_{14} + s_{18} + s_6 - s_{26} - s_{10} + s_{22}\},$$

$$+ \cdot 0229 (\log = \overline{2} \cdot 37872) \{s_3 - s_{29} - s_{13} + s_{19} + s_5 - s_{27} - s_{11} + s_{21}\},$$

$$+ \frac{1}{16} \{s_4 - s_{28} - s_{12} + s_{20}\}. \qquad (19.)$$

$$\mathbf{E} = \frac{1}{16} \{s_0 + s_{15} - s_8 - s_{24}\},$$

$$+ \cdot 0239 (\log = \overline{2} \cdot 37872) \{s_1 + s_{31} + s_{15} + s_{17} - s_7 - s_{25} - s_9 - s_{23}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0442 (\log = \overline{2} \cdot 64536) \{s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{26} - s_{10} - s_{22}\},$$

$$+ \cdot 0577 (\log = \overline{2} \cdot 76149) \{s_3 + s_{29} + s_{13} + s_{19} - s_5 - s_{27} - s_{11} - s_{21}. \qquad (20.)$$
"" 2. Using the deviations observed on the sixteen principal points only, we have
$$\mathbf{A} = \frac{1}{16} \{s_0 + s_2 + s_4 + \dots + s_{30}\}. \qquad (21.)$$

$$\mathbf{B} = \cdot 0478 (\log = \overline{2} \cdot 67975) \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$+ \cdot 0884 (\log = \overline{2} \cdot 67975) \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$+ \cdot 0884 (\log = \overline{2} \cdot 67975) \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$+ \cdot 0884 (\log = \overline{2} \cdot 67975) \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$C = \frac{1}{8}(s_0 - s_{16}),$$

$$+ \cdot 1155 (\log = \overline{1} \cdot 06252) \{s_2 + s_{30} - s_{14} - s_{18}\},$$

$$+ \cdot 0884 (\log = \overline{2} \cdot 94639) \{s_4 + s_{28} - s_{12} - s_{20}\},$$

$$+ \cdot 0478 (\log = \overline{2} \cdot 67975) \{s_6 + s_{26} - s_{10} - s_{22}\}. \qquad (23.)$$

$$\mathbf{D} = 0884 (\log = \overline{2} \cdot 94639) \{ s_2 - s_{30} - s_{14} + s_{18} + s_6 - s_{26} - s_{10} + s_{22} \},$$

$$+ \frac{1}{8} \{ s_4 - s_{28} - s_{12} + s_{20} \}. \qquad (24.)$$

$$\mathbf{E} = \frac{1}{8} \{ s_0 + s_{16} - s_8 - s_{24} \},$$

$$+ \cdot 0884 \ (\log = \overline{2} \cdot 94639) \{ s_2 + s_{30} + s_{14} + s_{18} - s_6 - s_{10} - s_{22} - s_{26} \}. \quad . \quad (25.)$$

$$2 \ z \ 2$$

"'3. Using the deviations observed on the eight principal points only, we have

$$A = \frac{1}{8} \{s_0 + s_4 + s_8 \dots + s_{28}\}. \dots (26.)$$

$$B = 1768 (\log = \overline{1} \cdot 24742) \{s_4 - s_{28} + s_{12} - s_{20}\},$$

$$+ \frac{1}{4} \{s_8 - s_{24}\}. \dots (27.)$$

$$C = \frac{1}{4} \{s_0 - s_{16}\},$$

$$+ 1768 (\log = \overline{1} \cdot 24742) \{s_4 + s_{28} - s_{12} - s_{20}\}. \dots (28.)$$

$$D = \frac{1}{4} \{s_4 - s_{28} - s_{12} + s_{20}\}. \dots (29.)$$

$$\mathbf{E} = \frac{1}{4} \{ s_0 + s_{16} - s_8 - s_{24} \}. \qquad (30.)$$

"'Having found A, B, C, D, E by any of the above methods, a table of the deviations on all the points may then be computed. The computation will be facilitated by using the following Table:—

"' Let  $B_1$ ,  $B_2$  ....  $B_7$ ,  $C_1$ ,  $C_2$  ....  $C_7$  represent the values of B and C multiplied by  $\sin 11^\circ 15'$ ,  $\sin 22^\circ 30'$ , and let  $D_2$ ,  $D_4$ ,  $D_6$ ,  $E_2$ ,  $E_4$ ,  $E_6$  represent the values of D and E multiplied by  $\sin 22^\circ 30'$ ,  $\sin 45^\circ$ , and  $\sin 67' 30^\circ$ , we have then

$$\begin{split} &\sin \delta_0 = A + C + E \\ &\sin \delta_{16} = A - C + E \\ &\sin \delta_1 = A + B_1 + C_7 + D_2 + E_6 \\ &\sin \delta_{31} = A - B_1 + C_7 - D_2 + E_6 \\ &\sin \delta_{15} = A + B_1 - C_7 - D_2 + E_6 \\ &\sin \delta_{15} = A + B_1 - C_7 + D_2 + E_6 \\ &\sin \delta_1 = A - B_1 - C_7 + D_2 + E_6 \\ &\sin \delta_2 = A + B_2 + C_6 + D_4 + E_4 \\ &\sin \delta_3 = A - B_2 + C_6 - D_4 + E_4 \\ &\sin \delta_{30} = A - B_2 + C_6 - D_4 + E_4 \\ &\sin \delta_{14} = A + B_2 - C_6 - D_4 + E_4 \\ &\sin \delta_{18} = A - B_2 - C_6 + D_4 + E_4 \\ &\sin \delta_3 = A + B_3 + C_5 + D_6 + E_2 \\ &\sin \delta_{29} = A - B_3 + C_5 - D_6 + E_2 \\ &\sin \delta_{29} = A - B_3 - C_5 + D_6 + E_2 \\ &\sin \delta_{19} = A - B_3 - C_5 + D_6 + E_2 \\ &\sin \delta_{19} = A - B_3 - C_5 + D_6 + E_2 \\ &\sin \delta_{19} = A - B_4 + C_4 - D \\ &\sin \delta_{28} = A - B_4 + C_4 - D \\ &\sin \delta_{20} = A - B_4 - C_4 + D \end{split}$$

$$\begin{split} &\sin \delta_5 = A + B_5 + C_3 + D_6 - E_2 \\ &\sin \delta_{27} = A - B_5 + C_3 - D_6 - E_2 \\ &\sin \delta_{11} = A + B_5 - C_3 - D_6 - E_2 \\ &\sin \delta_{21} = A - B_5 - C_3 + D_6 - E_2 \\ &\sin \delta_2 = A - B_6 + C_2 + D_4 - E_4 \\ &\sin \delta_{26} = A - B_6 + C_2 - D_4 - E_4 \\ &\sin \delta_{10} = A + B_6 - C_2 - D_4 - E_4 \\ &\sin \delta_{22} = A - B_6 - C_2 + D_4 - E_4 \\ &\sin \delta_7 = A + B_7 + C_1 + D_2 - E_6 \\ &\sin \delta_7 = A + B_7 + C_1 - D_2 - E_6 \\ &\sin \delta_9 = A + B_7 - C_1 - D_2 - E_6 \\ &\sin \delta_9 = A + B_7 - C_1 + D_2 - E_6 \\ &\sin \delta_8 = A + B - E \\ &\sin \delta_{24} = A - B - E. \end{split}$$

- "'If the deviations are under 7° or 8°, the angles of deviation may be used in the formulæ instead of the sines of the angles without producing a sensible error in the result.
- "'It may be observed that  $\varphi' \cos \theta'$  and  $\varphi' \sin \theta'$  would be themselves properly expressed in a series containing sines and cosines of  $\zeta'$  and  $2\zeta'$ , and this would introduce into the expression for  $\sin \delta$  terms of the form

F sin 
$$3\zeta' + G \cos 3\zeta' + H \sin 4\zeta' + K \cos 4\zeta'$$
.

"'The omission of these terms from the formula we have used does not affect the values we have found for A, B, C, D, E; and the values of the additional coefficients may be determined from the following expressions, in which we make use of the observations on the sixteen principal points only:—

$$F = 1155 (\log = 1.06252) \{s_2 - s_{30} + s_{14} - s_{18}\},$$

$$+ 0884 (\log = 2.94639) \{s_4 - s_{28} + s_{12} - s_{20}\},$$

$$- 0478 (\log = 2.67975) \{s_6 - s_{26} + s_{10} - s_{22}\},$$

$$- \frac{1}{8} (s_8 - s_{24}). \qquad (31.)$$

$$G = \frac{1}{8} (s_0 - s_{16})$$

$$+ 0478 (\log = 2.67975) \{s_2 + s_{30} - s_{14} - s_{18}\},$$

$$- 0884 (\log = 2.94639) \{s_4 + s_{28} - s_{12} - s_{20}\},$$

$$- 1155 (\log = 1.06252) \{s_6 + s_{26} - s_{10} - s_{22}\}. \qquad (32.)$$

$$H = \frac{1}{16} \{s_2 - s_{30} - s_{14} + s_{18} - s_6 + s_{26} + s_{10} - s_{22}\}. \qquad (33.)$$

$$K = \frac{1}{16} \{s_0 + s_{16} + s_8 + s_{24} - s_4 - s_{28} - s_{12} - s_{20}\}. \qquad (34.)$$

- "'If the deviations are so small that the angles may be used instead of their sines, then the differences between the observed deviations and the deviations calculated with the first five terms may be used instead of  $s_2$ ,  $s_4$ , &c. in finding F and G or H and K. There is however no advantage gained thereby, as the quantities within the brackets in F and G have already been found in calculating B and C.
- "'As an example of the use of these formulæ, we may take the deviations observed on board Her Majesty's ship Erebus at Gillingham, in Sept. 1839\*.
  - "'From the deviations observed on the sixteen principal points, I find

$$\delta = 17' + 235' \cdot \sin \zeta' - 13' \cos \zeta' + 21' \cdot \sin 2\zeta' - 1' \cdot 23 \cos 2\zeta'$$
.

"'From the deviations on the eight principal points, I find

$$\delta = 16' + 233' \cdot 5 \sin \zeta' - 14' \cdot \cos \zeta' + 21 \sin 2\zeta' - 0' \cdot 75 \cos 2\zeta'$$

"'Applying the correction derived from the first formula, the residuary differences on the sixteen principal points, beginning with north, are respectively—

$$-3'$$
, 0,  $+6'$ ,  $+14'$ ,  $-6'$ ,  $-18'$ ,  $+12'$ ,  $+7'$ ,  $+1'$ ,  $-11'$ ,  $-12'$ ,  $-9'$ ,  $+5'$ ,  $+7'$ ,  $+6'$ , 0.

"These differences evidently nearly follow the law of  $\sin 3\zeta'$ ; they give  $F=5'\cdot 5$ ; G=-7'.

" After applying the correction 
$$5' \cdot 5 \sin 3\zeta' - 7' \cos 3\zeta'$$
, the residuary difference is  $+4' -2', -3', +9', 0', -9', +13', -1', -6', -9', -3', -4', -1', -2', +5', +8'$ .

"'The differences, it will be seen, are smaller, and do not distinctly follow any regular law. If we calculate H and K we shall find

$$H=2'; K=1'.$$

But these corrections are so much within the errors of observation, that there could be no advantage in using them.

"'The expression for sin & may be put under the following form, viz.—

$$\sin \delta = A + \sqrt{B^2 + C^2} \sin (\zeta' + \alpha) + D \sin 2\zeta' + E \cos 2\zeta', \quad . \quad . \quad (35.)$$

in which  $\alpha$  is the angle whose tangent is  $\frac{C}{B}$ , and is nearly the easterly azimuth of the line of no deviation.

"It seems probable that in ordinary cases A,  $\alpha$ , D and E will not change materially with a change of latitude, while  $\sqrt{B^2+C^2}$  will vary nearly as the tangent of the dip. The last-mentioned term is also the most important, from its magnitude and its dependence on the changes which the permanent magnetism undergoes. It may therefore be useful to have the means of obtaining this quantity separately. This may be done from observations of the horizontal force, made in the position of the standard compass, with the ship's head on any two opposite (affected) courses, from the formula

$$\sqrt{B^2+C^2} = \frac{\sqrt{H_1^2+H_2^2+2H_1H_2\cos(\text{diff. of true azimuth})}}{H_1+H_2}, \quad . \quad . \quad (36.)$$

<sup>\*</sup> Contributions, No. V., p. 150.

in which  $H_1$   $H_2$  represent the observed horizontal force in the two positions of the ship's head.

"'If the difference of the true azimuths of the ship's head is 180°, the expression

becomes 
$$\sqrt{B^2+C^2} = \pm \frac{H_1-H_2}{H_1+H_2}, \quad (37.)$$

which is the same expression as that for the value of  $\alpha \tan \theta$  in the Memorandum in No. V. of these Contributions.

- "'The value of the horizontal force may be determined by vibrating a horizontal needle, or by deflecting the compass needle in the manner described by Lieut. CLERK in page 347. The difference of azimuths may be determined by the bearings of a distant object, or astronomically.
- "'This method seems to be adapted to the case of a ship lying at moorings in a tideway. The observations may be made before and after the change of tide, and the rudder adjusted so that the difference of the compass bearings of the ship's head may be exactly 180°.
- "'This formula is more accurate the more nearly the dip approaches to 90°; and the method seems therefore particularly applicable in high magnetic latitudes.
- "'If the true magnetic azimuth of the ship's head on the two positions is determined, the values of B and C may be obtained by the formula

$$B = -\frac{H_2 \cos \zeta_1 + H_1 \cos \zeta_2}{H_1 + H_2},$$

$$C = \frac{H_2 \sin \zeta_1 + H_1 \sin \zeta_2}{H_1 + H_2}.$$

" 'A. S.'

" 'Lincoln's Inn, March 3, 1846."

"The constants for correcting the declination observations were (in consequence of this Memorandum) calculated by the equations 21, 22, 23, 24 and 25, taking the mean of the two series at the Cape of Good Hope.

"The following are the deduced values of the constants:-

Station.	θ.	q.	Α.	В.	C.	D.	Е.
Cape of Good Hope	-53 56	1.158	+·00600 +·00479 +·01453	-·01550	+.00514	+.00448	+.00335
Means	-57 35	1.291	+.00844	02086	+.00638	+.00401	+.00028

"From the three values of B, and C, values of C' and P', F' and Q' were obtained by the equations

B=-
$$\left(C'\tan\theta+\frac{P}{\phi\cos\theta}\right)$$
; and C=F' tan  $\theta+\frac{Q}{\phi\cos\theta}$ ;

for we have

Hence by elimination we obtain

$$C' = -.0209$$
;  $F' = -.0006$ ;  $P' = +.0088$ ;  $Q' = -.0034$ .

"From the values of C', P', F' and Q', a table of the values of B and C in different dips and intensities was formed, and from them with the mean values of A, D and E, a table for correcting the observations of Declination was calculated by equ. 35. The corrections thus obtained appear to give very closely the true corrections, at all events much within the limits of observation errors. The following is a comparison between the observed and calculated deviations at King George's Sound,  $\theta$  being  $=-65^{\circ}$  04', and  $\varphi=1.70$ .

Ship's head.	δ by calcula- tion.	δ by observa- tion.	Difference.	Ship's head.	δ by calcula- tion.	δ by observa- tion-	Difference.
N. N.N.W. N.W. W.N.W. W. S.W. S.W.	+0 52 +0 17 -0 21 -0 58 -1 25 -1 16 -0 54 -0 24	+0° 15′ 0 00° +0 20° -1 40° -1 50° -1 00° -0 24	-0 37 -0 17 +0 41 -0 42 -0 15 -0 34 -0 06 +0 09	S. S.S.E. S.E. E.S.E. E. N.E. N.E. N.N.E.	+0 03 +0 47 +1 25 +2 02 +2 25 +2 17 +1 52 +1 22	+0° 50° +0° 55° +2° 20° +3° 10° +2° 40° +3° 10° +3° 30° +2° 35°	+0° 47° +0° 08° +0° 55° +1° 08° +0° 15° +0° 53° +1° 38° +1° 13°

+ Sign denotes a deviation towards the west.

"It appears from this comparison, that the calculated corrections are smaller in amount than the observed. As the ship had just returned from a high magnetic latitude, it is probable that the observed corrections belonged to a greater dip than the one at the station, and therefore that the corrections would be more nearly represented by taking them out from the Table for a larger Inclination and Intensity. The great differences on the E.S.E., N.E. and N.N.E. points are caused most probably by errors of observation.

"The correctness of equation (6.) will be more easily perceived by the accordance of observations made at sea, in a high dip, making due allowance for the difficulty of observing in bad weather.

# "2. Calculation of Corrections for the Inclination Observations.

"To obtain these corrections four constants are necessary, viz. a, b, c, d; a and b are obtained from the deviations of a compass (placed on the same spot as the dipping-

needle) on the sixteen principal points.	The following are the observations at King
George's Sound, the Mauritius, and the	Cape of Good Hope.

Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.
N. N.W. N.W. W.N.W. W. W. S.W. S.W. S.W.	-0° 45′ -1° 15′ -2° 05′ -3° 20′ -3° 35′ -3° 45′ -1° 55′ *3° 00′	$\begin{array}{cccc} -0 & 05 \\ -1 & 25 \\ -1 & 45 \\ -2 & 25 \\ -3 & 05 \\ -3 & 05 \\ -1 & 35 \\ -1 & 05 \end{array}$	-0 25 Not observed0 05 -0 35 -0 50 -1 15 -1 45 -0 35	S. S.S.E. S.E. E.S.E. E. E.N.E. N.E.	Not observed. +2 40 +3 25 +3 25 +3 25 +2 35 +2 45 +2 20	$\begin{array}{c} + 1 & 25 \\ + 1 & 15 \\ + 1 & 10 \\ + 1 & 50 \\ + 2 & 15 \\ + 1 & 05 \\ + 0 & 35 \\ + 0 & 25 \end{array}$	-0 50 Not observed. +1 55 +2 35 +2 40 +1 10 +0 45 +0 05

<sup>&</sup>quot;Allowing for the errors of observation, it appears from these observations that the iron is symmetrically distributed in reference to the compass placed on the same spot where the observations of inclination and intensity were made, and therefore that we may use the equations in Contributions V. and VI.

"From these equations the values of a and b are found,—

At King George's Sound . . . 
$$a=0296$$
;  $b=9867$ ; Mauritius . . . . . . . .  $a=0272$ ;  $b=9910$ ; Cape of Good Hope . . . . .  $a=0192$ ;  $b=9766$ .

"The values of a and b can be found independently of the compass, from the observations of dip and intensity themselves, A' being supposed = 1, by means of the formulæ

"Values of  $\varphi'$  and  $\theta'$  were obtained from observations on the sixteen principal points of the compass made at King George's Sound, Mauritius, and the Cape of Good Hope. They are as follows:—

Values of  $\theta'$ .

	Obs	erved Inclinati	on.		Observed Inclination.			
Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	
N. N.N.W. N.W. W.N.W. W. S.W. S.W.	-66 15 -66 33 -66 19 -66 07 -65 44 -65 42 -65 31 -64 48	-54 38 -54 44 -54 47 -55 02 -55 21 -54 39 -54 29 -54 07	$\begin{array}{rrrrr} -5\mathring{4} & 0\mathring{1} \\ -5\mathring{4} & 35 \\ -5\mathring{4} & 56 \\ -5\mathring{4} & 47 \\ -5\mathring{4} & 46 \\ -5\mathring{4} & 31 \\ -5\mathring{3} & 45 \\ -5\mathring{3} & 09 \\ \end{array}$	S. S.S.E. S.E. E.S.E. E. E.N.E. N.E.	$\begin{array}{c} -6\mathring{4} & 5\acute{2} \\ -65 & 00 \\ -65 & 29 \\ -65 & 52 \\ -66 & 23 \\ -66 & 07 \\ -66 & 17 \\ -66 & 31 \end{array}$	-53 46 -53 41 -54 20 -54 25 -54 50 -54 55 -54 47 -54 27	-53 28 -53 50 -53 51 -54 24 -54 46 -54 53 -54 37 -54 25	

<sup>\*</sup> This observation is not taken into account, being obviously erroneous.

- araci	σοι φ.		
		. 01	oserved
pe of Good Hope.	Ship's head.	King George's Sound.	Mau

Values of  $\phi'$ .

	Ob	served Intens	ity.		Observed Intensity.			
Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	Ship's head.	King George's Sound.	Mauritius.	Cape of Good Hope.	
N.	1.737	1.150	1.024	s.	1.799	1.206	1.066	
N.N.W.	1.736	1.152	1.020	S.S.E.	1.797	1.204	1.055	
N.W.	1.734	1.151	1.025	s.E.	1.790	1.182	1.045	
W.N.W.	1.752	1.158	1.025	E.S.E.	1.773	1.189	1.032	
w.	1.758	1.166	1.028	E.	1.753	1.169	1.029	
w.s.w.	1.775	1.198	1.036	E.N.E.	1.757	1.166	1.024	
s.w.	1.790	1.191	1.049	N.E.	1.736	1.159	1.023	
s.s.w.	1.805	1.200	1.061	N.N.E.	1.735	1.155	1.023	

<sup>&</sup>quot;The observed values of  $\theta$  and  $\varphi$  are approximately—

King George's Sound . . 
$$\theta = -65^{\circ} 11^{\circ}$$
;  $\varphi = 1.733$   
Mauritius . . . .  $\theta = -54 14$ ;  $\varphi = 1.158$   
Cape of Good Hope . . .  $\theta = -53 37$ ;  $\varphi = 1.027$ .

"Substituting these values in equations (1.) and (2.), we have

King George's Sound . . 
$$a=.0242$$
;  $b=.9905$ ; Mauritius . . . . .  $a=.0234$ ;  $b=1.0105$ ; Cape of Good Hope . . .  $a=.0186$ ;  $b=.9916$ .

"Including these values with those obtained from the compass observations, we get the mean values for a and b,

$$a=.0237$$
;  $b=.9912$ .

"The constants c and d are calculated from the formula

$$c\cos\zeta + d\tan\theta = b\sin\zeta\csc\zeta'\tan\theta'$$

for the observations between N.N.W. and S.S.W., and N.N.E. and S.S.E.; and for the other points, viz. N. and S., by the formula

$$c\cos\zeta+d\tan\theta=(\cos\zeta+a\tan\theta)\sec\zeta'\tan\theta'$$
.

"The values of  $\zeta$  and  $\theta$  were given by the observations at the several stations. The values of c and d are as follows:—

King George's Sound . . 
$$c=010$$
;  $d=1.054$ ; Mauritius . . . . .  $c=014$ ;  $d=1.011$ ; Cape of Good Hope . . .  $c=003$ ;  $d=1.033$ .

The values of c and d were also obtained from the observations of dip and intensity, independently of a and b, by the formula

$$c\cos\theta\cos\zeta-d\sin\theta=\frac{\phi'}{\phi}\sin\theta'$$
,

A being supposed equal to unity; which gives the following values:-

King George's Sound . . c=028; d=1.023; Mauritius . . . . . c=024; d=1.017;

Cape of Good Hope . . . c=021; d=1.020.

"The mean of these six values makes

$$c=0.017$$
;  $d=1.026$ .

"From these values of a, b, c and d, a table of corrections was found by means of equations (12.) and (13.) (Contribution V.), employing calculated values of  $\zeta$ .

"In order to test the accuracy of the table, we may compare observed and calculated values of the dip at King George's Sound. It will be seen that on the northerly points the correction is rather too large, on the easterly and westerly too small, and nearly correct on the S., S.S.W. and S.S.E. points. The differences however are within the limits of observation errors.

Ship's head.	Observed Inclination.	Tabular correction.	Corrected Inclination.
N. N.N.w. and N.N.E. N.W. and N.E. W.N.W. and E.N.E. W. and E. S.W. and E.S.E. S.W. and S.E. S.S.W. and S.S.E.	$\begin{array}{c} -6\mathring{6} \ 1 \acute{5} \\ -66 \ 3 2 \\ -66 \ 18 \\ -66 \ 07 \\ -66 \ 03 \\ -65 \ 47 \\ -65 \ 30 \\ -64 \ 54 \\ -64 \ 52 \\ \end{array}$	+1 23 +1 23 +1 31 +1 09 +0 46 +0 23 +0 02 -0 16 -0 18	$ \begin{array}{c} -6\mathring{4} & 5\mathring{2} \\ -65 & 09 \\ -64 & 47 \\ -64 & 58 \\ -65 & 17 \\ -65 & 24 \\ -65 & 28 \\ -65 & 10 \\ -65 & 10 \end{array} $

The mean inclination observed on shore with the same needle being  $-65^{\circ}$  11'.

"3. Calculation of Corrections for Intensity Observations.

"The constant A is calculated from the above observations by means of the formula

$$\frac{\phi'}{A'\phi}\sin\theta' = c\cos\theta\cos\zeta + d\sin\theta.$$

"The values of  $\theta$ ,  $\varphi'$  and  $\zeta$ , are all given by the observations on the sixteen points of the compass; those of  $\varphi$  and  $\theta$  by the observations on shore. The following are the resulting values for A', viz.—

King George's Sound . . . A'=0.998 Mauritius . . . . . . A'=0.992 Cape of Good Hope . . . A'=0.992 Mean . . A'=0.994

"This value being so near unity, A is assumed =1.0, with which and the values of c and d already determined, a table of corrections was formed by means of the equation

$$\frac{\phi'}{\phi} = A'c(\frac{d}{c}\tan\theta + \cos\zeta)\cos\theta \csc\theta' *,$$

 $\theta$  and  $\zeta$  being obtained from the tables for correcting the dips and declinations.

<sup>\*</sup> Philosophical Transactions, 1843, Part II. p. 162.

### "II. Determination of Index Corrections.

#### "1. Declination Observations.

"The compass used was one of the Admiralty compasses (B. 20). It was supplied with two cards, one considerably heavier than the other to be used in bad weather; but as it was found that in all weathers the heavy card was the steadiest and gave the best results, it was accordingly generally used. The index corrections of both cards were determined at the Magnetic Observatory, Cape of Good Hope. The following are the means of several observations with each card; the mean monthly declination by the observatory declinometer being  $+29^{\circ}$  07'.

Card A (the light card) gave 
$$.+2\mathring{8} \ 20'$$
; correction  $+47'$ .  
Card J (the heavy card) gave  $.+28 \ 15$ ; correction  $+52$ .

"These corrections have been applied to all the observations, according to the card employed.

### "2. Inclination Observations.

"Two of Mr. Fox's instruments were kept in constant use, one observed in the forenoon and the other in the afternoon. In order to distinguish them, we may call the one observed in the morning No. 1, the other was marked C. 9. In No. 1, needle 1 was mounted and used throughout, the spare needle 2 being used as a deflector. The index correction for 1 was determined at the Magnetic Observatory at the Cape, both before and after the Expedition, by comparing the inclination with the face of the instrument west (that being the way the observations were taken on board) with the mean monthly inclination shown by the observatory needles. The following are the observations with the deflectors at  $40^{\circ}$  from the apparent dip:—

```
November 10, 1844, needle 1, face west -5\mathring{3} 3\mathring{9}; correction +8 November 10, 1844, needle 1, face east -53 59; correction +28 November 21, 1844, needle 1, face west -53 38; correction +7 November 21, 1844, needle 1, face east -53 58; correction +27 The mean monthly inclination being -53^{\circ} 31'.
```

"After the 13th of January it was found more convenient to adjust the deflectors at the apparent dip, and make the same observations serve both for dip and intensity. The index corrections to be applied in this case are given by the following observations:—

7. 1		Observed	Inclination.—I	Face West.	•	True Inclina-	Index correc-
Date.	Direct.	Def. N.	Def. S.	Def. N and S.	Mean.	tion.	tion.
1844. December 1 December 5 1845.	$-5\overset{\circ}{3} \overset{\circ}{52} \\ -53 \overset{\circ}{49}$	$-5\overset{\circ}{3}\overset{\circ}{21}$ $-5\overset{\circ}{3}\overset{\circ}{20}$	$-5\overset{\circ}{3} \overset{\prime}{44} \\ -53 & 43$	$ \begin{array}{c c} -53 & 39 \\ -53 & 38 \end{array} $	$-5\overset{\circ}{3} \overset{\circ}{3}\overset{\circ}{9} \\ -53 \overset{\circ}{3} \overset{\circ}{8}$	$\left.\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 07
June 30	-54 12 $-54$ 08	$-53 13 \\ -53 15$	$-53  ext{ } 46 \\ -53  ext{ } 46$	$ \begin{array}{c cccc} -53 & 51 \\ -53 & 43 \end{array} $	$-53  ext{ } 45 \ -53  ext{ } 43$	$\left.\right\} -53 25$	+19
Mean	-54 01°	-53 17	-53 45	$-53 \ 43$	-53 41	-53 28	+13

"Magnets N and S are the small magnets belonging to the apparatus used conjointly; deflector N and deflector S are the respective poles of the spare needle. +13' has been applied in all cases except when only magnets N and S have been used, in which case +24' has been used, that being the mean correction for direct and magnets N and S.

"For the index corrections for needle A of C. 9, we have only an observation in Simon's Bay, Cape of Good Hope, before starting. Needle A was used from the Cape to King George's Sound, and was observed on shore at King George's Sound on the 7th of April. On the 10th it was found, from the discordance of the observations, that its axle had been damaged since the observations on the 7th, it was therefore taken out and needle B mounted in its place. The instrument had a third needle C which was used as a deflector. The small magnets were also used, both conjointly and separately. The observation in Simon's Bay gives,—

For C. 9, needle A . . . . . . . 
$$-53^{\circ} 24'$$
 Corrected inclination, needle 1 . . .  $-53^{\circ} 50'$  Index correction  $-26'$ .

This correction has been applied to all observations made with needle A of C. 9. For the correction of needle B, we have a comparison at the Cape of Good Hope after the return of the Expedition, and also at Woolwich, in January 1846. All observations with this instrument were taken with the face east.

"The following are the observations at the Cape:-

Date.			Observed	Inclination.—I	Face East.			True Inclination.	Index correc-	
Dutte	Direct.	Def. N.	Def. S.	Def. S. Mag. N and S. Mag. N. Mag. S. Mean.						
1845. June 30. July 2.		$-5\overset{\circ}{4} \ 1\overset{\circ}{5} \\ -54 \ 11$	$\begin{array}{c c} -52 & 47 \\ -52 & 55 \end{array}$	$-5\mathring{4} 06'$ $-54 15$	$-5\overset{\circ}{3}\ 2\overset{\prime}{9} \\ -53\ 49$	$-53^{\circ} 23^{\circ}  -53^{\circ} 41^{\circ}$	$-5\overset{\circ}{3} \overset{40}{45}$	$-5\overset{\circ}{3} \ 2\overset{\prime}{5} \\ -53 \ 25$	+15 +20	
Mean	-53 48	-54 13	-52 51	-54 10	-53 39	-53 32	-53 43	-53 25	+18	

"And at Woolwich:-

Date.			Observed	Inclination.—I	ace East.			True	Index
Date.	Direct.	Def. N.	Def. S.	Mag. N and S.	Mag. N.	Mag. S.	Mean.	Inclination.	correc- tion.
1846. Jan. 13. 15.	$+68^{\circ}58^{\circ}  +68^{\circ}56^{\circ}$	$+68 02 \\ +68 21$	$+68 \ 37 \ +68 \ 52$		$+68 \ 32 \ +68 \ 35$	$+68 \ 30 \ +68 \ 34$	$+68 \ 31 \ +68 \ 41$	$\left.\begin{array}{c} \\ +68 \\ 58 \end{array}\right.$	, +22
Mean	+68 57	+68 12	+68 44	+68 35	+68 33	+68 32	+68 36	+68 58	+22

<sup>&</sup>quot;The index correction obtained at the Cape has been used for all the observations taken with this needle.

- "3. Elements of Calculation of the Intensity Observations.
- "Fox No. 1.—For the observations with this instrument, the Cape of Good Hope has been taken as a base station, the intensity having been observed there both before and after the Expedition, so that any change in the magnetism of the deflectors or needles can be detected.
- "The intensity at Woolwich being assumed =1.372, it is necessary to get the corresponding intensity at the Cape. This can be got independent of the dippingneedles, by means of the absolute horizontal intensity and inclination observed at each station.
- "The value of the horizontal intensity at the Cape is given as follows by observations made at the observatory in February, March, April and May 1845:—
- "Observations of the Absolute Horizontal Intensity, at the Magnetic Observatory, Cape of Good Hope, 1845.

Bar. A. 21. Suspended . . . length 3.00 inch . . . 
$$\left(1 + \frac{H}{F}\right) = 1.00084$$
.

Bar. V. Deflecting . . . length 3.67 inch . . . q = .00008 . . .  $\log \pi^2 \cdot k = 1.57254$ .

Date.	Angles of Deflection.		Corrected time of	Temperature during		Bifilar readings at 60 during		Results.		
G.	Dist. 1.2 ft.	Dist. 1·3 ft.	vibration.	Deflection.	Vibration.	Deflection.	Vibration.	<i>m</i> .	X.	
1845. Feb. 10, 11, 12. Mar. 10, 11, 12. Apr. 13, 14, 15. May 14, 15, 16.	6 01·1 5 57·5	\hat{4} 47.5 4 44.0 4 41.2 4 39.2	s 4·4970 4·5310 4·5570 4·5650	71·4 71·4 62·9 60·7	7 <sup>°</sup> 1·7 71·9 62·6 59·9	Scale dir. 185·9 186·0 176·9 177·2	185·8 177·4	0·4118 0·4064 0·4019 0·4001	4·480 4·478	4.482

<sup>&</sup>quot;The value of k is obtained by means of two cylindrical weights in the usual manner; the value employed is the mean of several determinations. Bifilar magnetometer k=000218, q=000218. Increase of reading denotes increase of force.

Whence 
$$X=4.482$$
,  $\theta$  being  $=-53^{\circ} 25'.5$ .

"The corresponding values at Woolwich are

$$X=*3.7284$$
,  $\theta$  being =  $+68^{\circ}$  57'.9.

- "From these values of X and  $\theta$ , we obtain the relative value of the intensity at the Cape (that at Woolwich being 1.372), I=0.993.
- "The relative intensity given by the needles of No. 1, from observations made at Woolwich and the Cape and given in the sequel, are as follows:—

Needle 1. 
$$\{ \begin{array}{ll} \text{Weight 1 gr. I=0.996} \\ \text{Weight 2 grs. I=1.017} \\ \end{array} \} 1.006. \quad \text{Needle 2.} \{ \begin{array}{ll} \text{Weight 1 gr. I=0.994} \\ \text{Weight 2 grs. I=1.006} \\ \end{array} \} 1.000.$$

<sup>\*</sup> Contributions, No. VII.; Philosophical Transactions, 1846, p. 246.

"The value of I at the Cape has therefore been assumed provisionally as unity; subject to future correction should any appear to be required.

"The spare needle 2 was always used as a deflector; the two small magnets were used conjointly only with this apparatus.

"Tables of equivalent weights were made at the Cape both before and after the Expedition, according to the method given in the instructions for the use of Mr. Fox's instrument. The following Table contains the mean of the two series.

De	ef. N.	De	ef. S.	Mag. N and S.		Def. N. (Continued.)		Def. S. (Continued.)		Mag. N. and S (Continued.)	
v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.
2°i	gr. 1.816	2ž	gr. 1.950	4î	grs. 3.608	3î	gr. 1.843	3 <u>2</u>	gr. 1.935	5 î	grs. 2·786
22	1.835	23	1.964	42	3.522	32	1.828	33	1.918	52	2.717
$\frac{23}{24}$	1.850 1.861	24 25	1.972	43 44	3·438 3·350	33 34	1.814 1.801	34 35	1.903	53 54	2.654 2.595
25 26	1.867	26 27	1.983	45 46	3.262	35 36	1.788	36 37	1.868	55 56	2.535 2.480
27	1.867	28	1.977	47	3.093	37	1.756	38	1.833	57	2.428
28 29	1.866	29 30	1.968 1.960	48	3·013 2·933	38 39	1.744	39 40	1.812	58 59	2·377 2·330
30	1.858	31	1.946	50	2.853	40	1.707	41	1.775	60	2.278

"With these values of w', and the following values of v and w, the values of I' have been calculated by the formula

$$I' = I \frac{\sin v \cdot w'}{\sin v' \cdot w}$$
 when deflectors are used, and

$$I' = I \frac{\sin v}{\sin v'}$$
 when weights are used.

Values of v at the Cape of Good Hope.

Date.	Def. N. $w = 1.721$ .	Def. S. $w = 1.782$ .	Mag. N and S. $w = 2.337$ .	Weight 1 grain.	Weight 2 grains.	Weight $2\frac{1}{2}$ grains.
1844. Dec. 1. 5.	39 06 39 01	40 38 40 37	59 23 59 22	21 36 21 34	46 54 46 33	65 22 65 20
June 30. July 2.		40 39 40 39	58 16 58 21	21 38 22 06	46 32 46 21	65 30 65 30
Mean	39 15	40 38	58 51	21 42	46 35	65 25

"From this Table it is evident that, with the exception of magnets N and S, the needles preserved their magnetism throughout the voyage. Magnets N and S lost magnetism to the amount of 033. The mean of the four observations have been taken; the early intensities by this method will therefore be rather too small, the latter ones rather too great.

"The formulæ for calculation are as follows:-

"Fox C. 9.—The values of the intensity at the Cape by the observations before and after the Expedition, by Fox, No. 1, are:—

Before . . . . . 
$$I=0.999$$
  
After . . . .  $I=1.001$  diff. .002.

"These values agreeing so closely, we may assume that the intensity at King George's Sound with this apparatus will be very near the truth, and that King George's Sound may therefore be taken as a base station for needle A of C. 9, which was not observed at the Cape before our departure. The intensities were observed with needle A mounted, from the Cape to King George's Sound, when the needle got unfortunately damaged, and it was necessary to replace it with needle B: one day's observations had however been made before the accident, and these observations serve for calculating the intensities taken on the voyage, assuming the intensity at King George's Sound to be that given by the other apparatus, viz. 1.688.

"The same deflectors and weights were used throughout; the spare needle C as a deflector, the two small magnets both conjointly and separately.

"Tables of equivalent weights for these deflectors, with needle A mounted, were obtained in the same way as in the case of the other apparatus. They are as follows:

De	f. N.	De	f. S.	Mag. N	I and S.	Ma	g. N.	Ma	g. S.
v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.
o.	grs.	_ 0	grs.	_0	grs.	50°	grs.	50°	grs.
5ů	2.175	5 0°	2.206	70°	2.625		1.578		1.975
49	2.200	49	2 247	69	2.675	49	2.028	49	2.025
48	2.225	48	2.288	68	2.725	48	2.078	48	2.075
47	2.263	47	2.323	67	2.775	47	2.130	47	2.125
46	2.300	<b>4</b> 6	2.357	66	2.825	46	2.182	46	2.175
45	2.338	45	2.388	65	2.875	45	2.235	45	2.240
44	2.375	44	2.419	64	2.925	44	2.288	44	2.304
43	2.413	43	2.460	63	2.982	43	2.341	43	2.368
42	2.450	42	2.500	62	3.038	42	2.394	42	2.433
41	2.488	41	2.538	61	3.094	41	2.447	41	2.498
40	2.525	40	2.575	60	3.150	40	2.500	40	2.563
. 39	2.565	39	2615	59	3.222	39	2.570	39	2.623
38	2.605	38	2.655	58	3.294	38	2.640	38	2.683
37	2.645	37	2.695	57	3.365	37	2.710	37	2.743
36	2.685	36	2.735	56	3.436	36	2.780	<b>3</b> 6	2.803
35	2.725	35	2.775	<b>55</b>	3.507	35	2.850	35	2.863
34	2.755	34	2.806	54	3.595	34	2.900	34	2.937
33	2.785	33	2.837	<b>53</b>	3.683	33	2.950	33	3.011
32	2.815	32	2.869	52	3.770	32	3.000	32	3.085
31	2.845	31	2.901	51	3.857	31	3.050	31	3.158
30	2.875	30	2.932	50	3.944	30	3.100	30	3.232
29	2.900	29	2.954	49	4.047				
28	2.925	28	2.975	48	4.150		1		

"The angles of deflection observed at King George's Sound are as follows:-

Def. N. $w = 2.779$ .	Def. S. $w = 2.821$ .	Mag. N and S. $w = 3.909$ .	Mag. N. $w = 2.875$ .	Mag. S. 2·895.	Weight 1 grain.	Weight 1½ grain.	Weight 2 grains.	Weight $2\frac{1}{2}$ grains.	Weight 3 grains.
33 11	33° 32′	50° 24	34 3ó	34° 34	10° 44	1 <b>7</b> 16	22 55	28 18	3 <b>š</b> 10

"Employing the values of v and w (I being =1.688), we get formulæ for calculating the intensities, viz.—

Def. N . . . .  $I' = :3325 \csc v' \cdot w'$ .

Def. S . . . .  $I' = :3306 \csc v' \cdot w'$ .

Mag. N and S  $I' = :3327 \csc v' \cdot w'$ .

Mag. N . . . .  $I' = :3326 \csc v' \cdot w'$ .

Mag. S . . . .  $I' = :3308 \csc v' \cdot w'$ .

Weight 1 grain . . I'=:3144 cosec v'. Weight  $1\frac{1}{2}$  grain . . I'=:5010 cosec v'. Weight 2 grains . . I'=:6573 cosec v'. Weight  $2\frac{1}{2}$  grains . I'=:8003 cosec v'. Weight 3 grains . . I'=:9722 cosec v'.

Comparing observations made at sea near the Cape with those given by the other needle, the deflectors of this apparatus do not appear to have lost magnetism.

"From King George's Sound to the Cape, needle B was mounted, the same deflectors and weights being used as with needle A. The Cape of Good Hope has been taken as the base station in this case, the intensity having been observed there on the return of the Expedition.

"The table of equivalent weights is given below.

De	ef. N.	Def. S.		Mag. 1	V and S.	Mag. N.		Mag. S.	
v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.	v'.	w'.
<b>2</b> 9̈́	1.794	$3\mathring{5}$	2.104	5 <b>0</b>	2.763	3î	1.891	3Ĝ	2.174
30	1.782	36	2.076	51	2.701	32	1.862	37	2.122
31	1.765	37	2.046	<b>52</b>	2.638	33	1.833	38	2.069
32	1.748	38	2.015	<b>53</b>	2.576	34	1.804	39	2.012
33	1.734	39	1.986	<b>54</b>	2.513	35	1.773	40	1.954
34	1.719	40	1.956	<b>55</b>	2.457	36	1.741	41	1.903
35	1.697	41	1.927	<b>56</b>	2.401	37	1.705	42	1.851
36	1.675	42	1.898	57	2.345	38	1.669	43	1.801
37	1.657	43	1.865	<b>58</b>	2.288	39	1.635	44	1.751
38	1.638	44	1.832	59	2.247	40	1.600	45	1.707
., 39	1.619	45	1.799	60	2.203	41	1.563	46	1.663
40	1.600	46	1.766	61	2.167	42	1.525	47	1.626
41	1.582	47	1.740	62	2.110	43	1.494	48	1.588
42	1.563	48	1.713	63	2.071	44	1.463		
43	1.541	49	1.684	64	2.032	45	1.443		
44	1.519	50	1.654	65	1.996		1		
45	1.491			66	1.960				
				67	1.927				

"The following are the angles of deflection on three separate days at the Magnetic Observatory, Cape of Good Hope:—

Def. N. $w = 1.500$ .	Def. S. $w = 1.659$ .	Mag. N and S. $w = 1.953$ .	Mag. N. $w = 1.480$ .	Mag. S. $w = 1.615$ .	Weight 1 grain.	Weight 1½ grain.	Weight 2 grains.
4 <sup>3</sup> 3 <sup>2</sup> 45 00	49 48 49 59	66 02 66 20	43 21 43 45	4 <sup>°</sup> 7 13 47 23	28° 00	4 <b>å</b> 1 <b>ó</b>	69° 31′
44 33	49 42	66 16	43 15	47 20	28 26	44 16	69 15
44 42	49 50	66 13	43 27	47 19	28 13	44 13	69 23

"Assuming the intensity at the Cape as unity, we get the following formulæ for calculation:—

Def. N			• • •	•.	$I'=4692 \csc v' \cdot w'$ .
Def. S				•,	$l'=4606 \csc v' \cdot w'$ .
Mag. N and S.			•		$I'=4686 \csc v' \cdot w'$ .
Mag. N					$I' = \cdot 4634 \operatorname{cosec} v' \cdot w'$ .
Mag. S	•			•	$I'=4552 \operatorname{cosec} v' \cdot w'$ .
Weight 1 grain.		•		•,	$I'=4728\csc v'$ .
Weight 1½ grain		•.			$I' = 6974 \csc v'$ .
Weight 2 grains		•. /	•	•.	$I' = 9361 \csc v'$ .

"The value of the intensity at King George's Sound by this needle is-

By weights . . . . 1.688. By deflectors . . . 1.672.

"The intensity by the other apparatus No. 1 is 1.688.

"At the Mauritius the intensity is-

By weights . . . . . 1.156. By deflectors . . . . 1.155.

And by the other instrument 1.156.

"It is therefore evident that needle B preserved its magnetism from King George's Sound to the Cape. Comparing the results with the deflectors with those of the other instrument, the deflectors do not appear to have lost magnetism; the difference at King George's Sound of '01 arises probably from error of observation. As the results given by weights are the most accurate when the observations are made on land, they have been exclusively used in such cases; at sea both weights and deflectors have been used.

"Besides the correction for the effect of the ship's iron, a second correction for the effect of temperature on the needle and deflectors is necessary. The observations have all been reduced to a common temperature of 60° by means of the formulæ

$$c=\mathbf{I}'\cdot q(t'-t),$$

t being taken as  $60^{\circ}$  and q being the coefficient for  $1^{\circ}$  of Fahr. Values of q for each needle and deflector employed, were obtained at the Magnetic Observatory, Cape of Good Hope, in the usual manner. The following is an abstract of the observations:—

Needle or deflector.	Approximate distance.	Total deflection in scale divisions.	Mean alternation of temperature.	No. of alternations.	Corresponding mean differ- ence of deflection.	billar correc-	Values of $q$ .
$\begin{array}{c} \text{No. 1.} & \begin{cases} \text{A. 1.} \\ \text{A. 2.} \\ \text{Def. N} \\ \text{Def. S} \end{cases} \\ \text{C. 9.} & \begin{cases} \text{A.} \\ \text{B.} \\ \text{C.} \\ \text{Def. N} \\ \text{Def. S} \end{cases} \end{array}$	ft. in. 3 0 3 0 1 0 1 5 1 5 1 5 1 0 1 0	497.5 805.2 873.3 880.5 1019.0 1059.5 1065.9 1004.8 1021.7	38 35 38 76 40 43 40 02 34 68 43 35 43 46 45 85 47 38	5 5 5 5 3 4 5 5 5	1·36 3·88 4·33 2·82 4·21 3·18 3·67 7·08 6·45	+·000046 +·000004 ·000019 ·000054 -·000070 -·000004 +·000008 +·000004 -·000024	.000072 .000116 .000123 .000081 .000117 .000069 .000079 .000154 .000133

"From the values of q tables of corrections were formed; observing that when weights are used an increase of temperature gives an additive correction, and the contrary when the deflectors are used. As the values of q are small, and the greatest difference of temperature amounts only to  $30^{\circ}$ , the corrections are seldom of any importance; they have however always been applied.

"Besides the observations made on board the Pagoda, others have been laid down on the maps, in order to assist in drawing the magnetic lines. A series of observations made by Lieut. Smith, R.N., between the Cape and Van Diemen Island, and another by Lieut. Dayman, R.N., between Van Diemen Island and the Cape (with the same instrument), have been laid down on the map of the Inclination. The same needles and deflectors were used in both cases. Lieut. Smith's observations are all taken with the face of the instrument east; those of Lieut. Dayman's with it both east and west. The following observations, made at the Ross Bank Observatory, Van Diemen Island, will serve to obtain the index corrections; the inclination by the observatory needles being  $-70^{\circ}$  40'.

	Observer.	Direct.	Def. N.	Def. S.	Def. N and S.	Mean.	Index cor- rection.	Face of instrument.
١	Lieut. SMITH. Lieut. DAYMAN. Lieut. SMITH. Lieut. DAYMAN.	-7054	-69 54	-7042	-71 36 }}		+48 -27	East West

- "These corrections have been applied to all the observations made by Lieut. Smith\*.
- "As no observations were made for local attraction, we can only obtain approximate corrections, by comparing observations made on or near the same spot with the ship's head on different points of the compass. In the series made by Lieut. Smith we have the following observations:—

August 14.	August 18.	September 10.	September 13.		
E. $\frac{1}{2}$ S	E. by s $-67$ 32	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N.N.E $-72   09$		

- "From these comparisons it would appear that the correction is very small, especially on the easterly points which were those generally observed upon; the observations have therefore been entered without any correction for the effect of the ship's iron.
- "With regard to those of Lieut. DAYMAN, there are two cases where observations have been taken on different days, but in nearly the same position, and with the
- \* When observations have been made with the face both east and west, the correction becomes +10'; when weights as well as deflectors are used for the inclination, the correction face east and west becomes -13'; this has been applied to the observations made by Lieut. Dayman.

ship's head on different points of the compass, and also some in very nearly the same geographical position as the Pagoda. Comparing these, it appears that the effect of the iron is nearly the same in both ships; the observations have consequently been corrected from the Table that was used for those taken on board the Pagoda. The following comparisons will show how near these corrections approach the truth.

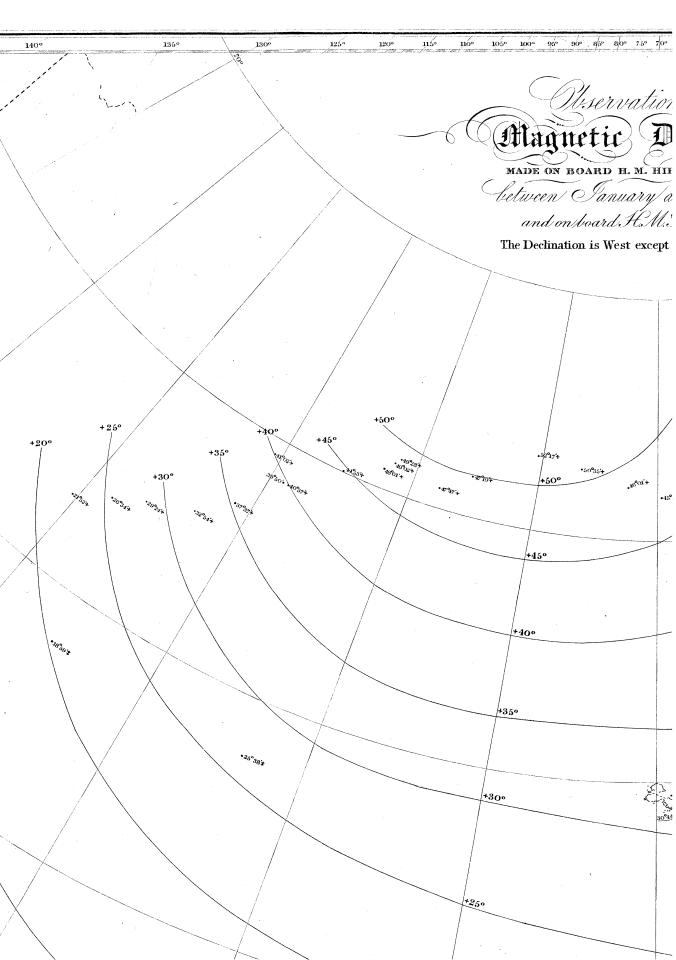
Lat.	Long.	Inclination.	Ship's head.	Tabular corrections.	Corrected Inclination.		Remarks.
-35 06 -34 58 -34 16 -24 00 -23 59 -34 36 -34 31 -34 48 -35 07 -36 42 -36 58		$ \begin{array}{rrrr} -66 & 47 \\ -55 & 32 \\ -57 & 01 \\ -56 & 09 \end{array} $		+1 31 +1 12 +0 18 +1 19	-65 14 -65 16 -64 44 -54 20 -54 07 -56 43 -57 06 -54 50 -67 03 -67 19 -66 27	Lieut. Dayman. Lieut. Clerk. Lieut. Dayman. Lieut. Clerk. Lieut. Dayman. Lieut. Clerk. Lieut. Clerk. Lieut. Clerk. Lieut. Clerk. Lieut. Dayman.	Difference + 6  Difference - 32  Difference - 13  Difference + 23  Difference + 18  January 9, 1845.  January 10, 1845.  January 11, 1845.  January 13, 1845.

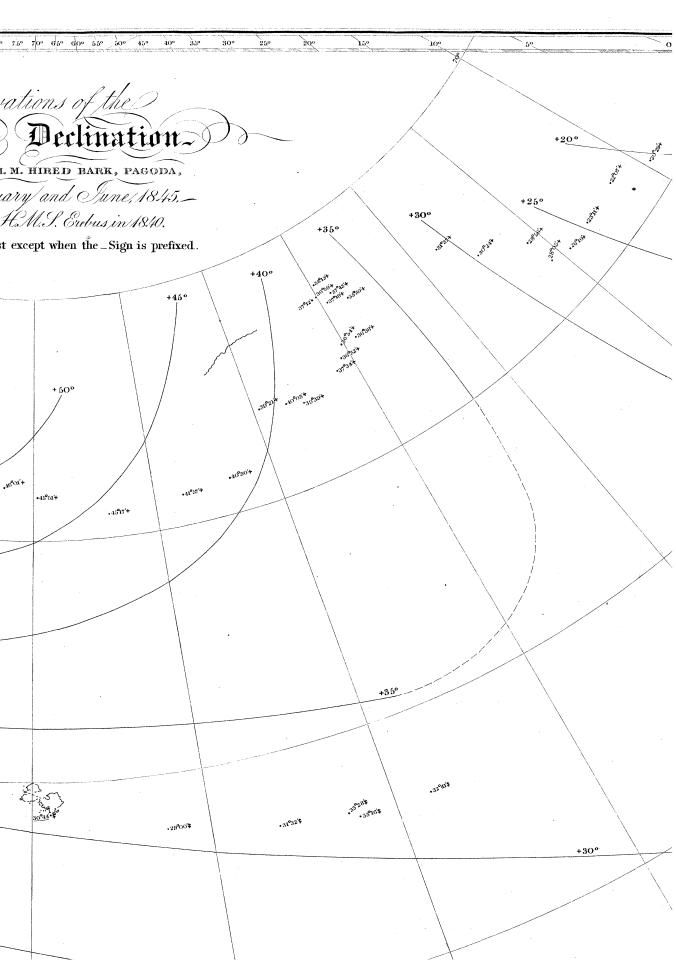
"The observations thus corrected have been entered in the chart. The lines on the chart are drawn by estimation, so as to conform as nearly as possible with the observations: some part of the lines laid down by Lieut.-Colonel Sabine (in No. V. of the Contributions) from Sir James C. Ross's observations have been dotted in, to show the agreement of the two series.

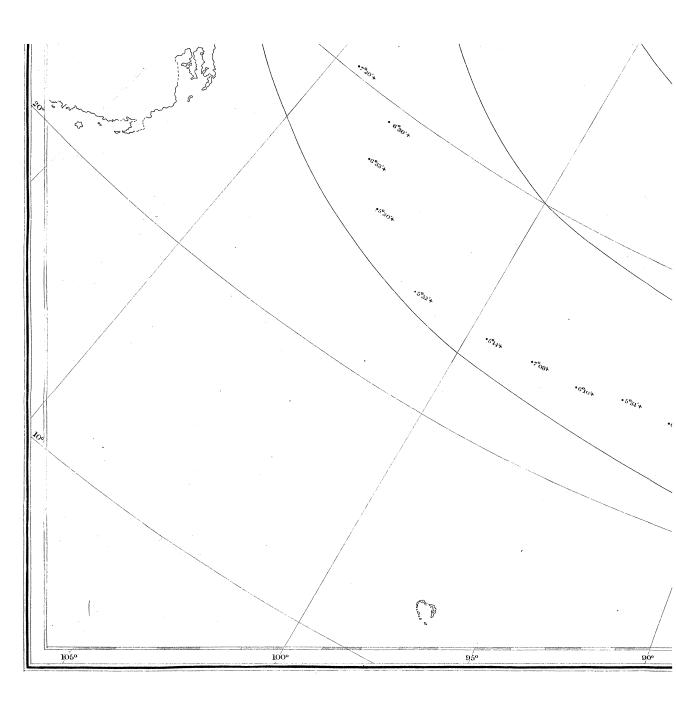
"In the Chart of 'Magnetic Declinations,' a series of observations made on board the 'Erebus' by Sir James C. Ross, between the Cape of Good Hope and Hobarton, have been laid down. These observations have been corrected for index error and local attraction, in the same way as the other observations during the Antarctic Expedition, the same constants being used.

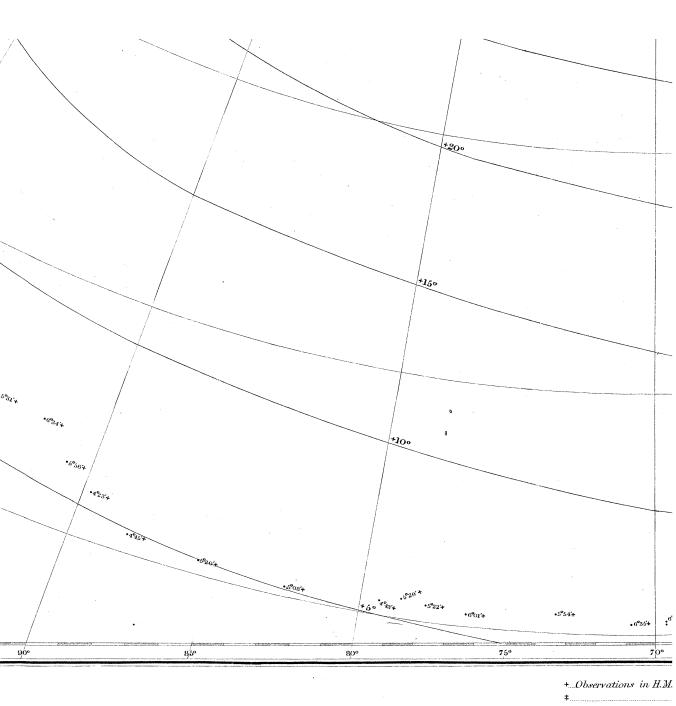
"In the chart of intensities, Sir James C. Ross's observations between the Cape of Good Hope and Hobarton have also been entered. These observations are contained in Lieut.-Colonel Sabine's Contributions, No. III. and V. The Cape of Good Hope is the base station in this case; but the intensity there has been taken as 0.981; it is therefore necessary to reduce them to an intensity at the Cape = 1.0, in order that they may compare with the intensities taken on board the Pagoda; this is done by multiplying each of them by  $\frac{.981}{1.000} = 1.02$  nearly. The observations thus corrected are given in a table at the end of the 'Pagoda' observations, together with those of variation and inclination by Sir J. Ross, and the inclinations and intensities by Lieuts. Smith and Dayman.

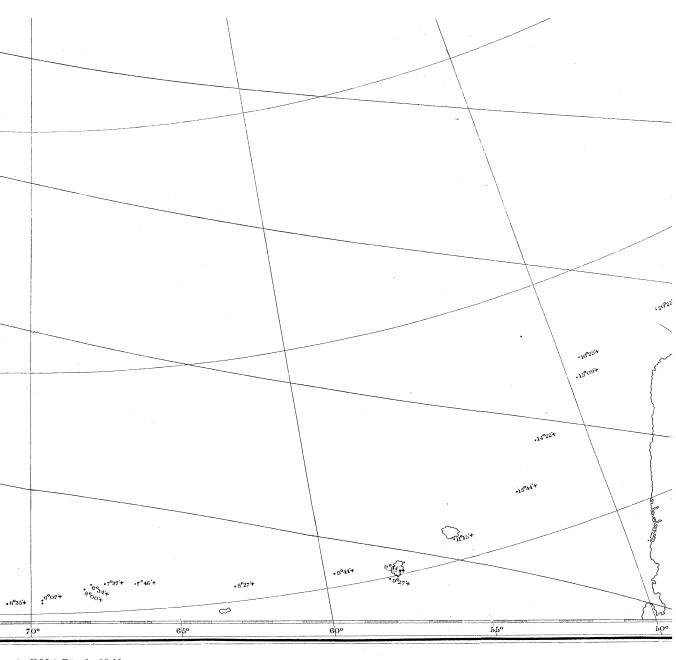
"In calculating the intensities observed by Lieut. SMITH, Hobarton has been taken as the base station, and the results by weights only used. The same has been done



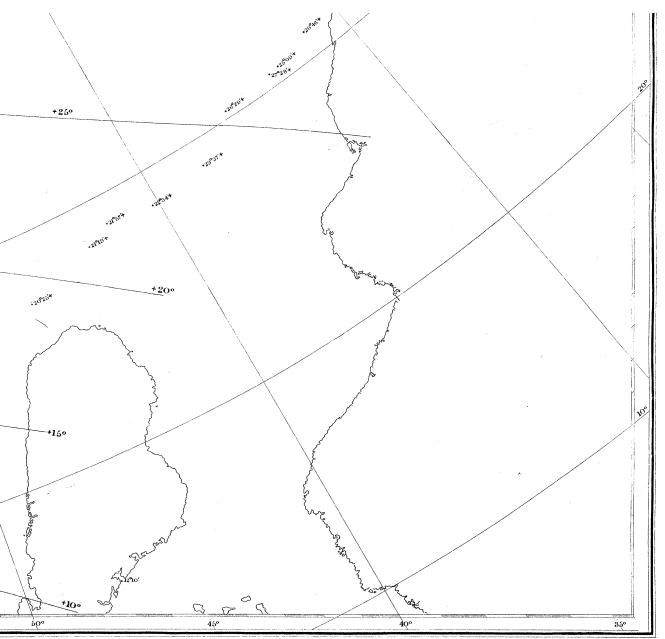




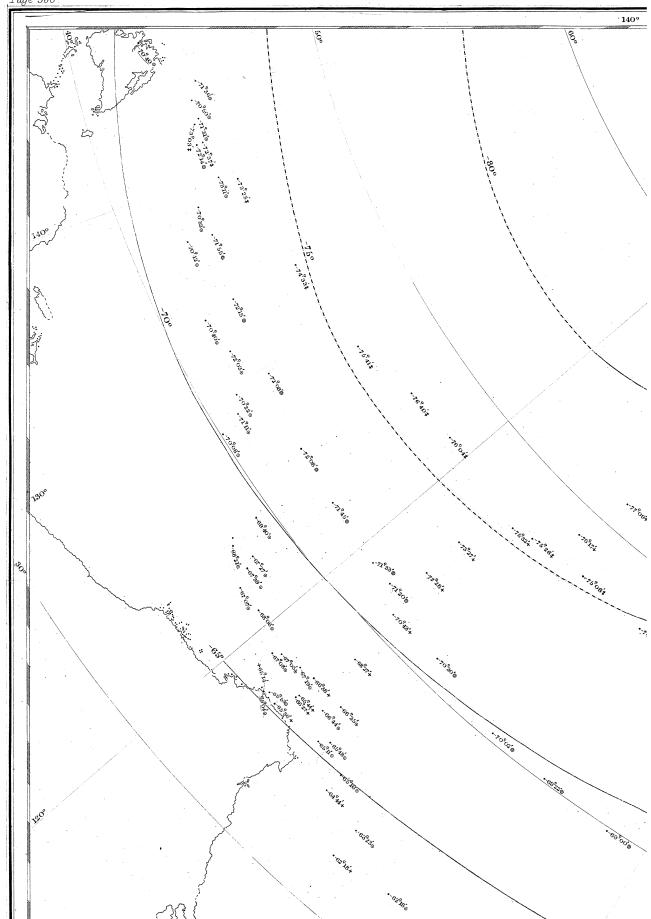


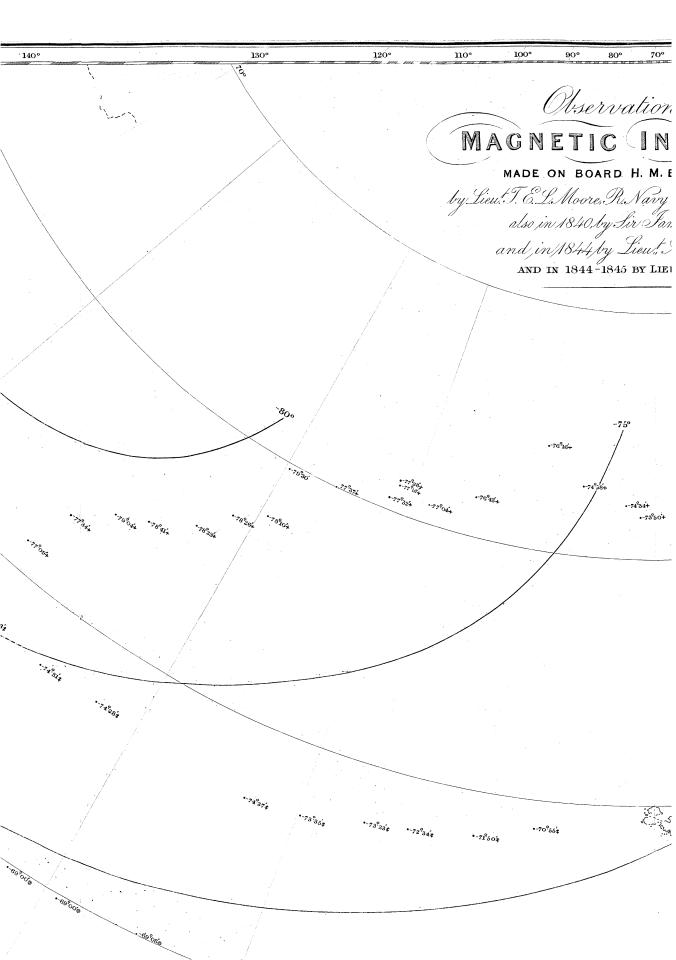


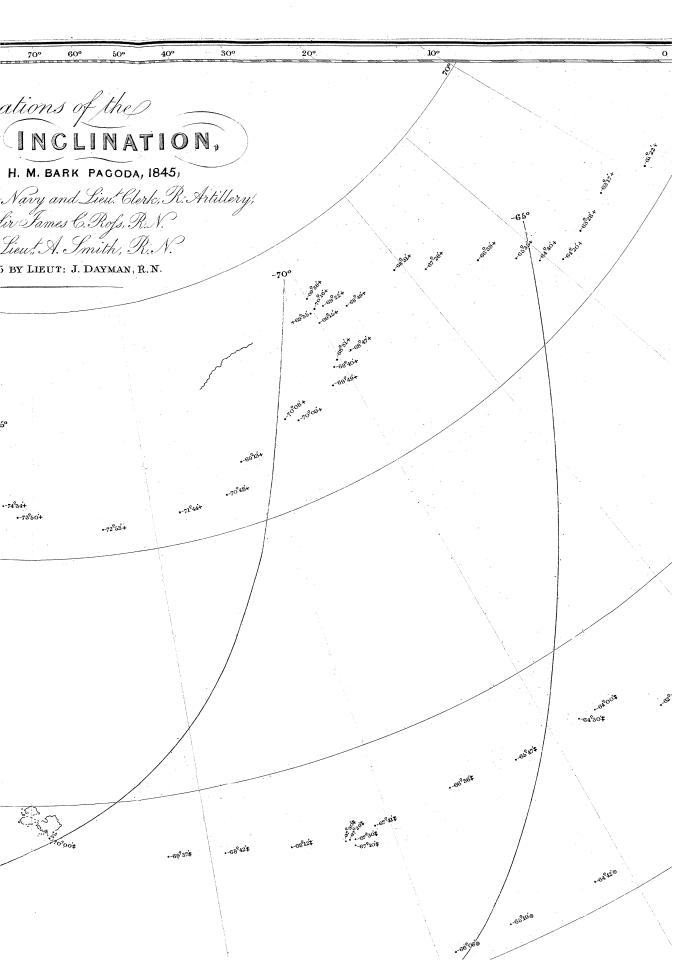
ns in H.M.S. Pagoda 1845. Erebus 1840.

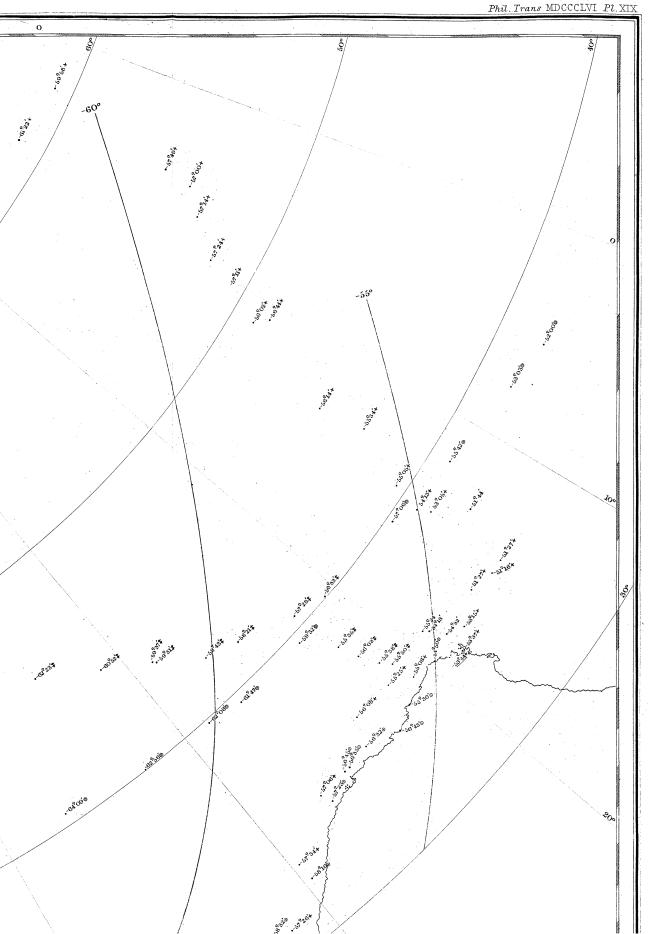


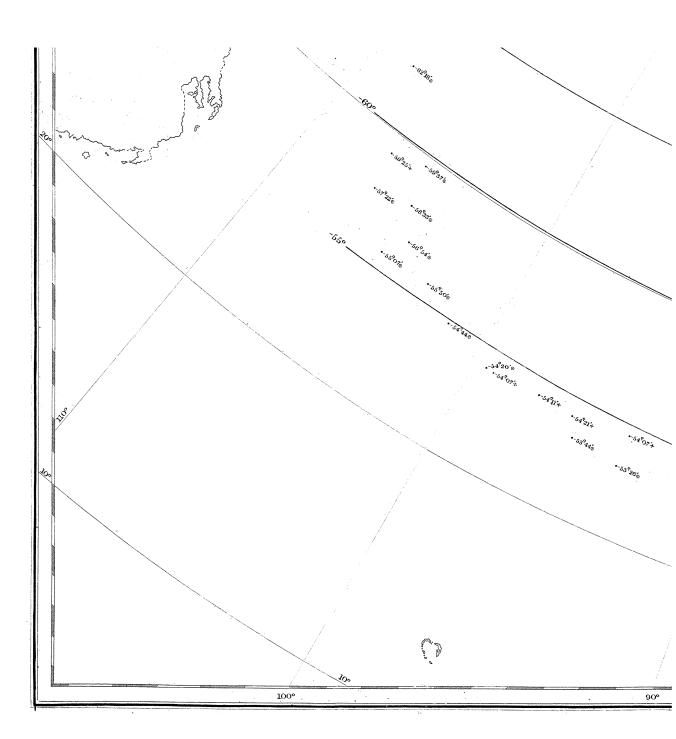
Engraved by J. & C.Walker.

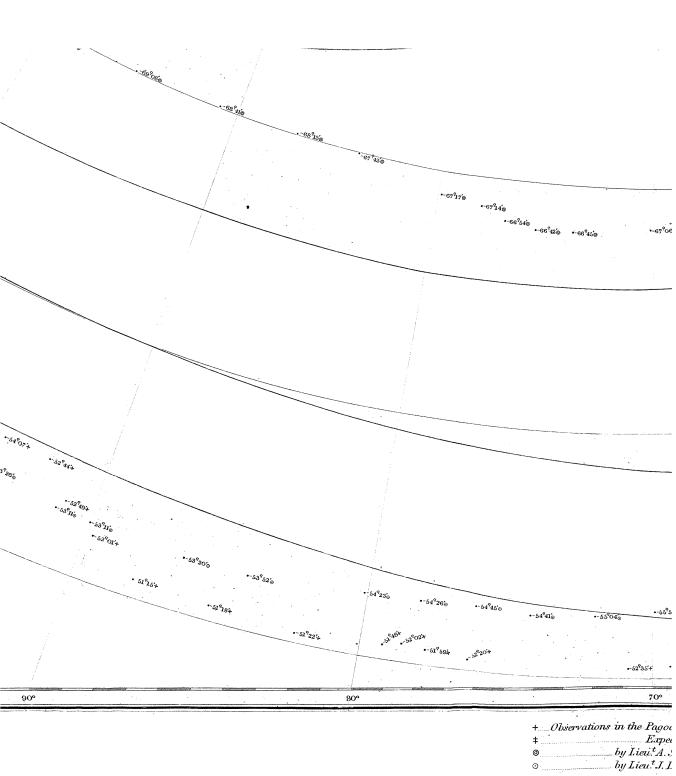


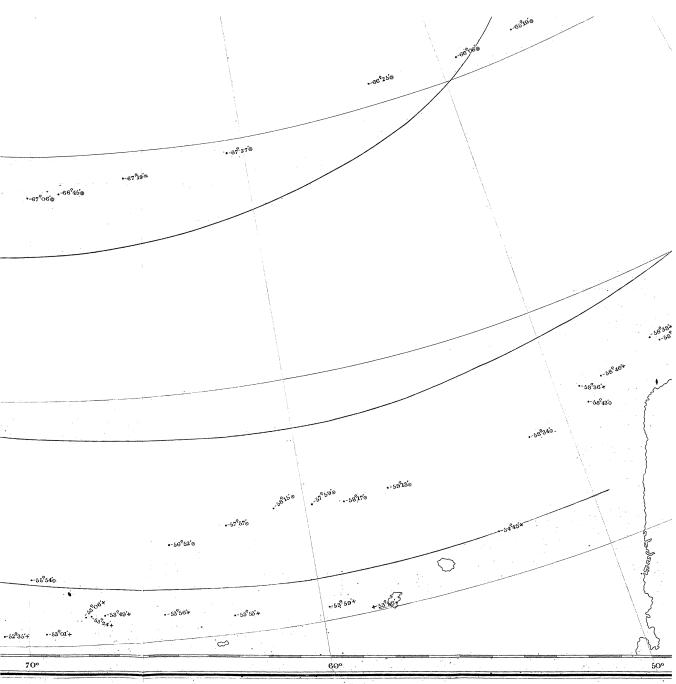




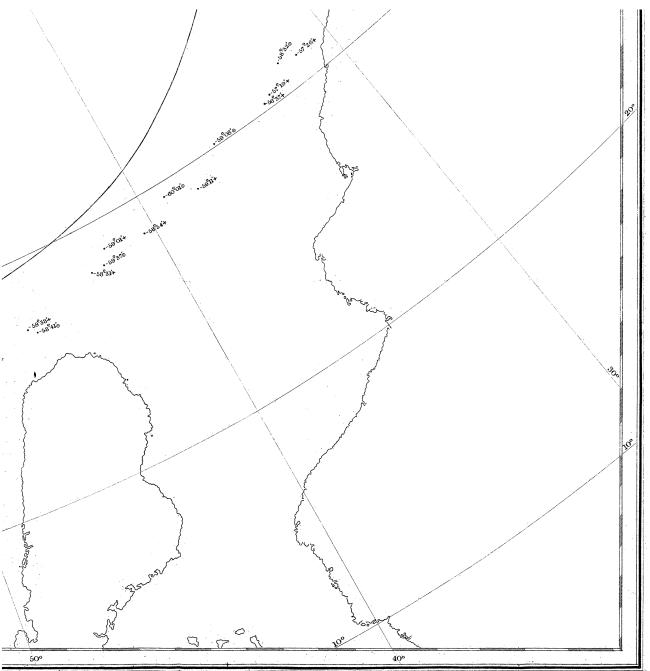




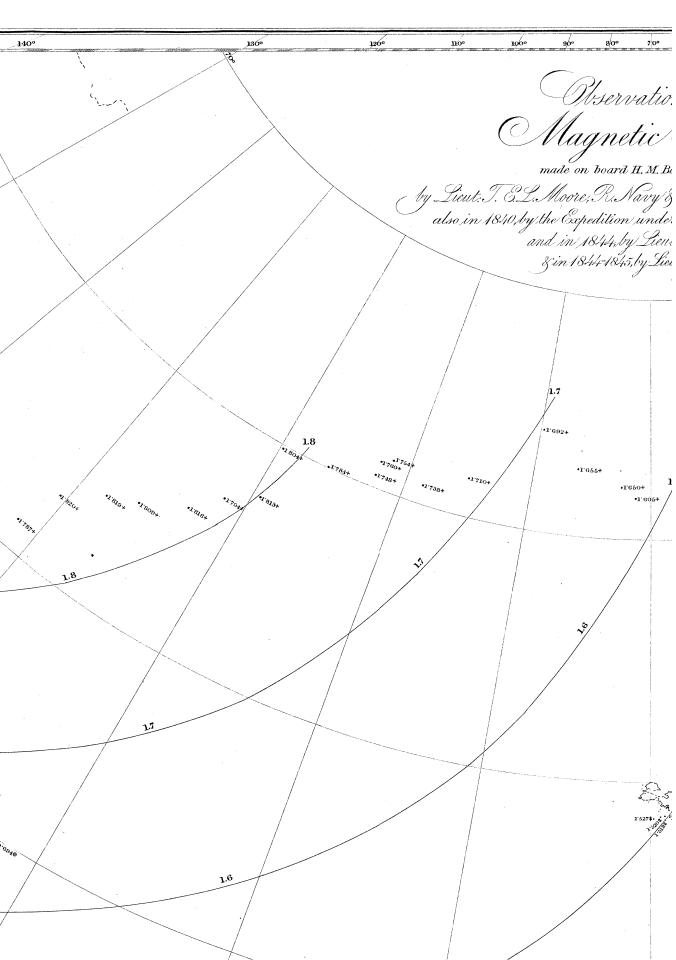


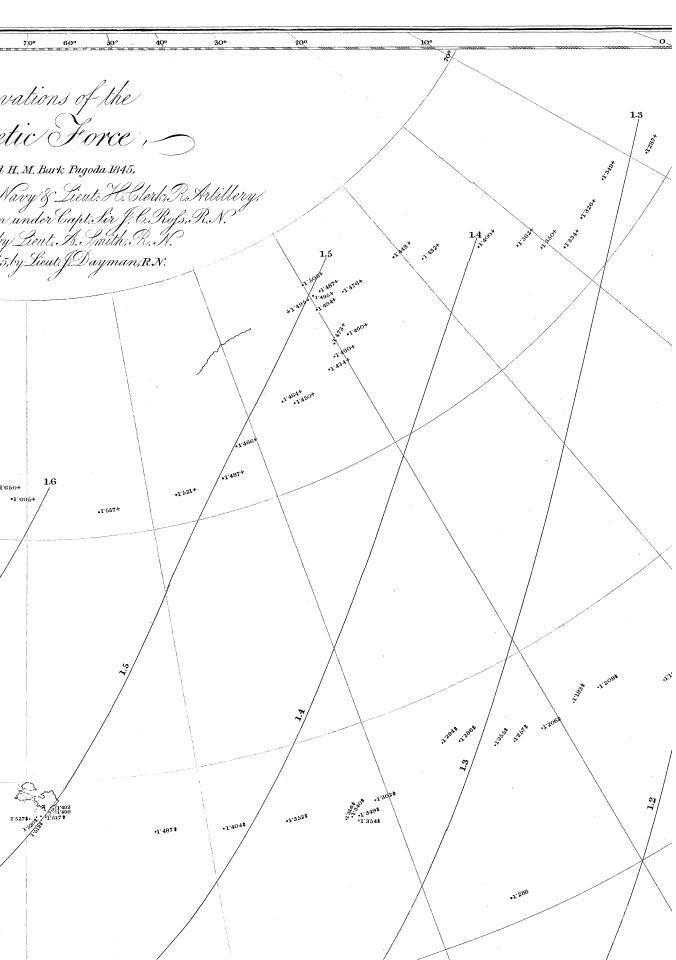


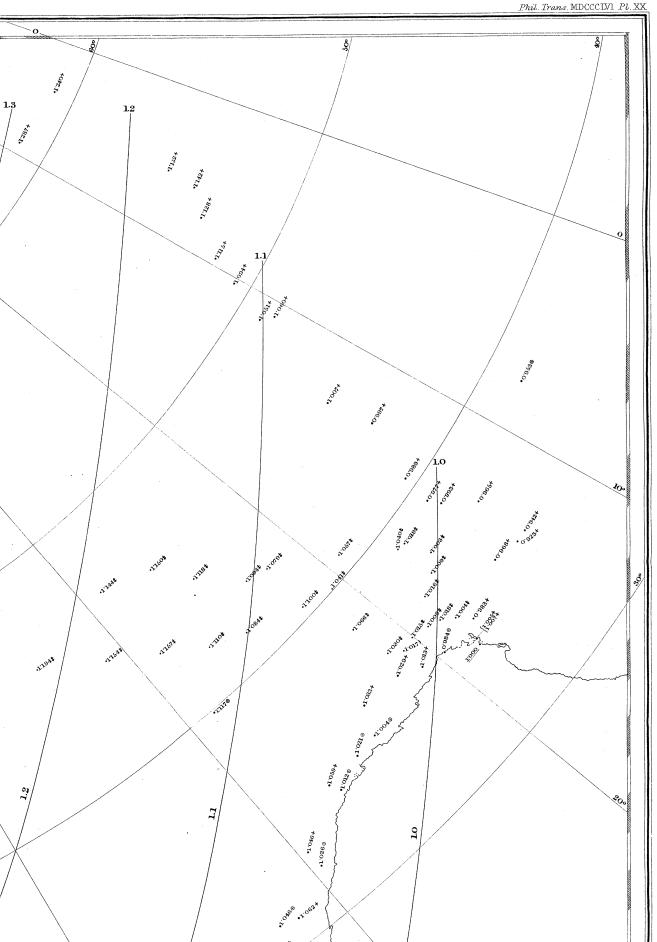
the Pagoda Expedition of Sir J. C. Ross Lieu<sup>t</sup> A. Smith R.N. Lieu<sup>t</sup> J. Dayman R.N.

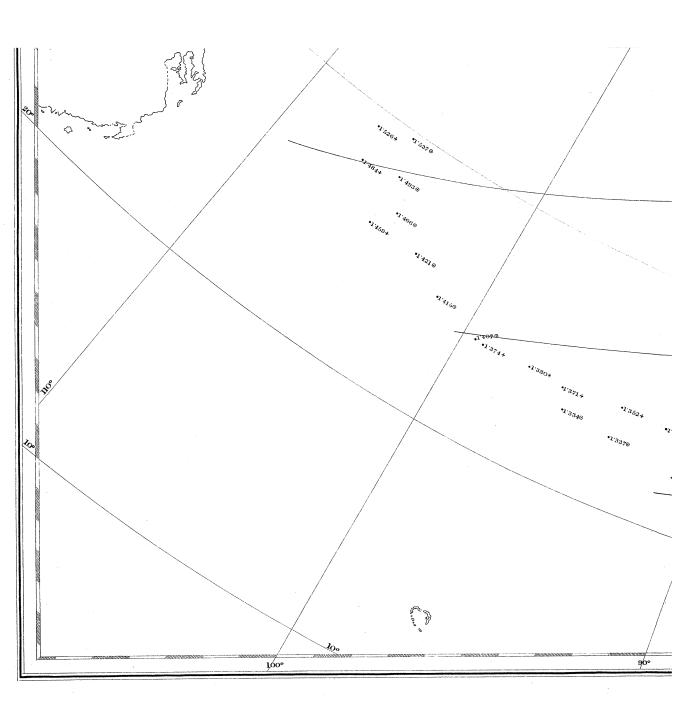


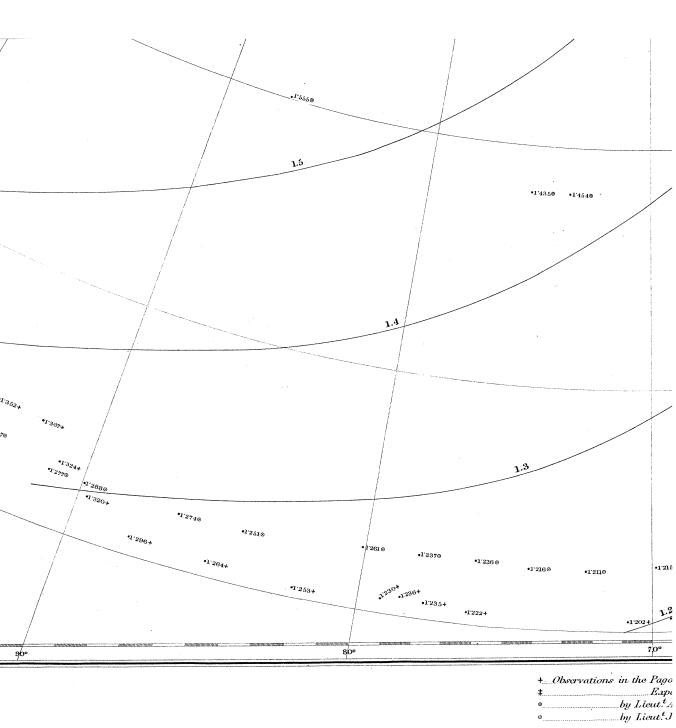
Engraved by J. & C. Walker.

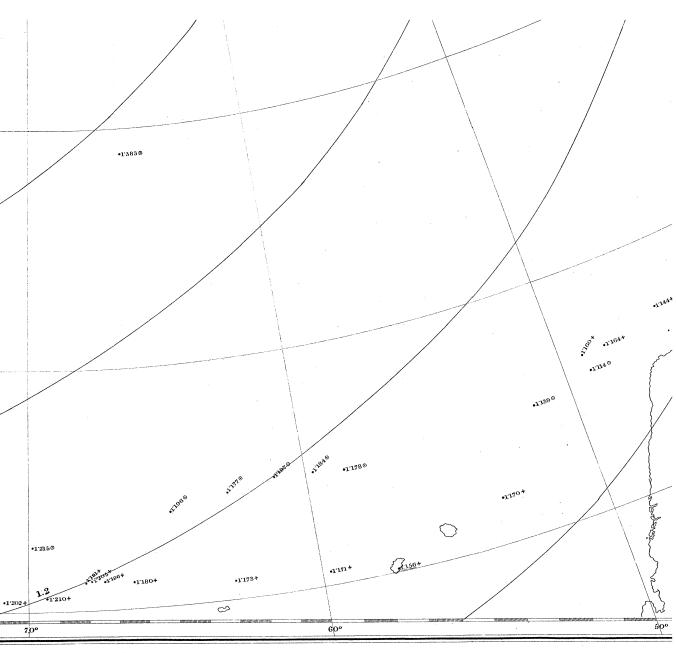




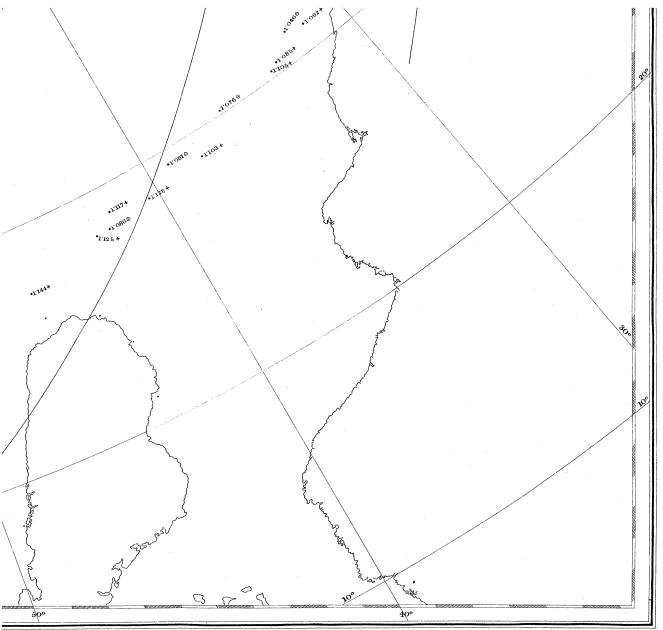








n the Pagoda \_\_\_\_Expedition of Sir J.C.Ross ny Lieut<sup>‡</sup>A.Smith R.N. ny Lieut<sup>‡</sup>J.Dayman R.N.



Engraved by J. & C. Walker.

with the series by Lieut. DAYMAN, the weights of two grains and three grains having been observed daily; the following observations with weights made at the observatory, Hobarton, give the formulæ for calculation:—

(II.) Lieut. Smith's. 
$$\begin{cases}
2 \text{ grains } v = 10 & 33 \\
3 \text{ grains } v = 16 & 05
\end{cases}; \quad
I = 1.80; \quad
I' = .3296 \text{ cosec } v'.$$
(II.) Lieut. Dayman's. 
$$\begin{cases}
1 \text{ grain } v = 5 & 19 \\
2 \text{ grains } v = 10 & 35 \\
3 \text{ grains } v = 16 & 20 \\
4 \text{ grains } v = 21 & 50 \\
5 \text{ grains } v = 27 & 41 \\
6 \text{ grains } v = 34 & 08
\end{cases}$$
From these we obtain the following values of  $v$  for 2 and 3 grains; viz.—

for 2 grains  $v = 10 & 43$ .

for 3 grains  $v = 16 & 11$ .

Hence for 2 grains  $I' = .3347$  cosec  $v'$ .

for 3 grains  $I' = .3347$  cosec  $v'$ .

"In correcting these observations the same plan has been pursued as with the dip observations. As Lieut. Smith's observations required no correction in the latter case, so none has been applied to the intensities; and Lieut. Dayman's have been corrected from the same table as was used for the 'Pagoda' observations. No corrections have been applied for the effect of temperature; but they are probably so small as not to affect the results."

Observations of the Declination made on board Her Majesty's hired Bark "Pagoda," from the 10th of January to the 23rd of June 1845.

The Observers are distinguished as follows:—M. Lieut. Moore; B. Mr. Bodie, Master; Cl. Lieut. Clerk; Cm. Mr. Comber, Mate; T. Mr. Tufnell, and Bn. Mr. Burdon, Midshipmen. West Declination characterized by the sign +.

Date.	Lat.	Long.	Observer.	Declination	Ship's head.	Inclination.	Correct Ship's	1	Corrected Declination.	Remarks.
			qo	observed.		-	attrac- tion.	Index.		
1845. Jan. 10 A.м.			М. М.	$+29 04 \\ +29 12$	w. w.		$+16 \\ +16$	$+47 \\ +47$	$\begin{vmatrix} +30 & 07 \\ +30 & 15 \end{vmatrix}$	
	$     \begin{array}{r rrr}     -34 & 42 \\     -34 & 42     \end{array} $	17 36 17 36	Cr.	+28 50 $+28 06$	W. ½ S. W.		$^{+15}_{+16}$	$ +47 \\ +47$	$\begin{bmatrix} +29 & 52 \\ +29 & 09 \end{bmatrix}$	Index correction +47' by observa- tions made at the
11 ам.	-35 26 $-35 26$	$15 08 \\ 15 08$	M. CL.	+27 31 +27 51 +27 43	W.S.W. W.S.W.	-51 27	$+11 \\ +11 \\ +11$	+47 +47	$\begin{vmatrix} +28 & 29 \\ +28 & 49 \\ +28 & 41 \end{vmatrix}$ $+28 & 39$	observatory, Cape of Good Hope.
12 а.м.	1 . (	15 08 14 00 14 00	М. В. В.	$\begin{array}{r} +27 & 41 \\ +25 & 45 \\ +26 & 23 \end{array}$	s.w.byw. <del>4</del> w. w. by n. w. by n.	$\left.\right\rangle_{-51}^{-51}$	$+10 \\ +03 \\ +03$	+47	$egin{pmatrix} +28 & 38 \ +26 & 35 \ +27 & 13 \ \end{pmatrix} +27 & 15 \ \end{pmatrix}$	
13 а.м.	$-35 17 \\ -35 10$	14 00	В. В. В.	$+27 06 \\ +24 37 \\ +25 04$	w. by n. s.w. by w. s.w. by w.	$\left.\right\}_{-51}$	$+03 \\ +07 \\ +07$	$+47 \\ +47$	$\begin{vmatrix} +27 & 56 \\ +25 & 31 \\ +25 & 58 \\ +25 & 40 \end{vmatrix}$	
15 P.M.	$     \begin{array}{r rrr}     -35 & 10 \\     -38 & 43     \end{array} $	13 25 14 25	В. М. М.	$+24 38 \\ +24 22$	s.w. by w. s.s.w. ½ w.	$\begin{bmatrix} -51 & 27 \\ -53 & 05 \end{bmatrix}$	$^{+07}_{00}$	$ +47 \\ +47$	$\begin{bmatrix} +25 & 32 \\ +25 & 09 \end{bmatrix}$ +25 09	
16 A.M. 16 P.M.	$-39 01 \\ -39 12$	14 45 14 42	См. М.	$+27  ext{ } 13 $ $+25  ext{ } 44 $ $+27  ext{ } 48$	s.w.byw. $\frac{1}{2}$ w.s.w.bys.s.w.bys.		$+18 \\ +06 \\ +06$	+47 +47	$\begin{vmatrix} +28 & 18 \\ +26 & 37 \\ +28 & 41 \end{vmatrix}$	
	-39 22 $-39 22$		M. B. B.	+28 25  +27 10  +28 28	s.w. by s. s.w. by s. s.w. by s.	$\rightarrow$ -54 13	$^{+06}_{+06}$	+47	$\left  { \begin{array}{*{20}{c}} {+29} & 18 \\ {+28} & 03 \\ {+29} & 21 \end{array}} \right $	
	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	14 25	В. В. В.	$     \begin{array}{r}     +27 & 01 \\     +27 & 49 \\     +27 & 28   \end{array} $	s.w. by s. s.w. by s. s.w. by s.		$^{+06}_{+06}$	+47  + 47	$egin{array}{c cccc} +27 & 54 \\ +28 & 42 \\ +28 & 21 \\ \hline \end{array}$	
17 а.м.	$     \begin{array}{rrr}     -39 & 22 \\     -39 & 22 \\     -40 & 08     \end{array} $	14 25	В. См. В.	+28 28  +26 26  +26 17	s.w. by s. s.w. by s. s.w. by w.		$^{+06}_{+06}$	+47 +47	$\begin{bmatrix} +29 & 21 \\ +27 & 19 \end{bmatrix} \\ +27 & 20 \end{bmatrix}$	
1, 11.19.	$     \begin{array}{rrr}     -40 & 08 \\     -40 & 09     \end{array} $	14 32	B. M. Cl.	+25 18  +25 33	s.w. by w. s.w. by w.		$^{+16}_{+16}$	+47 + 47	$\begin{array}{c cccc} +26 & 21 \\ +26 & 36 \end{array}$	
	-40 16 $-40 18$	14 36 14 35	T. T.	+27 34  +26 54	s.w. by w. s.w. by w. s.w. by w.	-55 05	$+16 \\ +16 \\ +16$	$ +47 \\ +47$	$\begin{vmatrix} +27 & 59 \\ +28 & 37 \\ +27 & 57 \\ +27 & 57 \\ \end{vmatrix}$	
	-40 14	14 37 14 37		+2600	s.w. by w. s.w. by w. s.w. by w.		$+16 \\ +16 \\ +16$	+47 +47	$egin{array}{c cccc} +28 & 07 \\ +28 & 15 \\ +27 & 03 \\ \hline \end{array}$	
19 а.м.	$     \begin{array}{r rrr}     -40 & 15 \\     -40 & 24 \\     -44 & 45     \end{array} $	14 32	Т. М. Сь.	$+26 00 \\ +27 57 \\ +25 09$	s.w. by w. s.w. by w. s.s.w. ½ w.	] ]	$^{+16}_{+16}$ $^{+04}$	+47	$\begin{bmatrix} +27 & 03 \\ +29 & 00 \\ +26 & 00 \end{bmatrix}$	
	$-44  45 \\ -44  45$	13 19	M. B.	$+23 05 \\ +27 40 \\ +27 00$	s.s.w. $\frac{1}{2}$ w. s.s.w.	-56 14	$^{+04}_{+02}$	$+47 \\ +47$	+23 56	Ship very unsteady; heavy sea.
20 A.M.	1	13 34 13 34	В. В.	+24 51  +24 31  +25 02	s.w. by w. s.w. by w. s.w. by w.	-56 08	+19	+47 + 47	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
22 А.М.	$-48 \ 27$ $-48 \ 27$ $-48 \ 27$	10 51 10 51	В. В. М.	$\begin{array}{r} +23 & 08 \\ +22 & 41 \end{array}$	s.w. by s. s.w. by s.	$-56 \ 44$	$+12 \\ +12$	+47 + 47	$\begin{array}{c} +24 & 07 \\ +23 & 40 \end{array}$	
	$-48 \ 27$		CL.	$\begin{array}{r} +24 & 40 \\ +24 & 54 \end{array}$	s.w. by s. s.w. by s.	J	$+12 \\ +12$		$+25 \ 39 + 25 \ 53$	

			ij				Correc	tions.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. Jan. 23 а.м.		1	M.	+22 30	s.w. ½ s.	ገ ° ′	+° 16		+23 33	
23 р.м.	$-50 \ 31$	10 25 10 25 10 17	CL. M.	$\begin{vmatrix} +23 & 38 \\ +24 & 27 \\ +23 & 18 \end{vmatrix}$	s.w. by s. s.w. ½ s. s.w.byw.½w.	57 11	$\begin{vmatrix} + & 16 \\ + & 16 \\ + & 16 \end{vmatrix}$	+47	$egin{bmatrix} +24 & 41 \ +25 & 30 \ +24 & 21 \ \end{bmatrix}$	
	3	10 20 10 10 10 10	M. CL.	$     \begin{array}{r}       +21 & 09 \\       +23 & 14 \\       +22 & 26     \end{array} $	s.w. by w. s.w. s.w.	-57 11	$\begin{vmatrix} + & 16 \\ + & 16 \\ + & 16 \end{vmatrix}$	+47	$\begin{vmatrix} +24 & 21 \\ +22 & 12 \\ +24 & 17 \\ +23 & 29 \end{vmatrix}$ $+23 \ 55$	
24 а.м.	-5058 $-5145$	10 09 9 34	Т. В.	$\begin{array}{r} +22 & 15 \\ +23 & 11 \end{array}$	s.w. s.w. by w.	]  }  }	+ 16 + 25	+47 + 47	$\begin{bmatrix} +23 & 18 \\ +24 & 23 \end{bmatrix}$	
24 р.м.	$     \begin{array}{r rrr}     -51 & 45 \\     -51 & 45 \\     -51 & 47      \end{array} $	9 34	М. Сь. См.	$\begin{vmatrix} +20 & 06 \\ +20 & 58 \\ +22 & 00 \end{vmatrix}$	s.w. by w. s.w. by w. s.w.byw.½w.	$\left.\right\}$ -57 39	$\begin{vmatrix} + & 25 \\ + & 25 \\ + & 25 \end{vmatrix}$	+47	$(+21 \ 18 > +22 \ 37 \ +22 \ 10 )$ $(+23 \ 16 )$	
	$     \begin{array}{r rrr}     -51 & 47 \\     -51 & 47 \\     -51 & 47     \end{array} $	1	См. См. Вм.	1	$\begin{array}{c} s.w.  byw.\frac{1}{2}w. \\ s.w.  byw.\frac{1}{2}w. \\ s.w.  byw.\frac{1}{2}w. \end{array}$		+ 29 + 29 + 29	+47	$\begin{pmatrix} +25 & 06 \\ +25 & 20 \\ +24 & 06 \end{pmatrix}$	
	$-51  45 \\ -51  45$	9 34 9 34	В. М.	$ +23 \ 11  +20 \ 06$	s.w. by w. s.w. by w.		+ 25 + 25	$\begin{vmatrix} +47 \\ +47 \end{vmatrix}$	$\left( egin{array}{cccccccccccccccccccccccccccccccccccc$	
	$     \begin{bmatrix}     -51 & 45 \\     -51 & 49 \\     -51 & 49     \end{bmatrix} $	9 32 9 32	CL. B.	$\begin{array}{r rrrr} +22 & 46 \\ +21 & 49 \end{array}$	s.w. by w. s.w. by w. s.w. by w.	$\begin{vmatrix} -57 & 39 \\ \end{vmatrix}$	+ 25	5 + 47 5 + 47	$\begin{pmatrix} 1 + 22 & 10 \\ + 23 & 58 \\ + 23 & 01 \end{pmatrix} + 23 = 46$	Card A.
		9 31	В. Сь. М.		s.w. byw. ½w. s.w. byw. ½w. s.w. byw. ½w.	.	+ 29   + 29   + 29	9 + 47	7 + 24 09  7 + 23 34  7 + 24 05	
25 A.M.	$\begin{bmatrix} -51 & 50 \\ -51 & 50 \end{bmatrix}$	9 31 9 31	CL. T. M.		s.w. by w. $\frac{1}{2}$ w. s.w. by w. $\frac{1}{2}$ w. s.w. by w. $\frac{1}{2}$ w	.]	+ 2: + 2: + 2:	$\begin{vmatrix} +47 \\ 9 \\ +47 \end{vmatrix}$	7 + 24 24 $7 + 23 52 $ $7 + 23 37$	
NO A.M.	$\begin{bmatrix} -53 & 00 \\ -53 & 00 \end{bmatrix}$	7 53 7 53	См.	$\begin{vmatrix} +22 & 50 \\ +22 & 06 \end{vmatrix}$	s w. by w. s.w. by w.	-57 14	+ 2	$5 + 47 \\ 5 + 47$	$7 \begin{vmatrix} +24 & 02 \\ +23 & 18 \end{vmatrix} + 23 4$	Card A.
26 л.м	$     \begin{array}{r rrr}     -53 & 00 \\     -53 & 59 \\     -53 & 59     \end{array} $	6 16 6 16	См. М. В.	$\begin{vmatrix} +19 & 49 \\ +20 & 18 \end{vmatrix}$	s.w. by w. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.	ļ	+ 2. + 3. + 3.	6 + 59 + 59	7 + 24 06 $2 + 21 17$ $2 + 21 46$	
	$     \begin{bmatrix}     -53 & 58 \\     -53 & 58 \\     -53 & 58     \end{bmatrix}   $	6 16	CL.	+20 24	w. by s. w. by s. w. by s.		+ 3	3 +59	$\begin{vmatrix} 2 + 22 & 21 \\ 2 + 21 & 49 \\ 2 + 22 & 01 \end{vmatrix}$	
26 р.м	$     \begin{array}{r rrr}     -53 & 58 \\     -53 & 58 \\     -53 & 58    \end{array} $	6 16	Bn. Cm. B.		w. by s. w. by s. E. $\frac{1}{2}$ S.	-57 00	+ 3	$\begin{vmatrix} 3 \\ +5 \\ 3 \\ +5 \end{vmatrix}$	$\begin{vmatrix} 2 & +22 & 53 \\ 2 & +22 & 01 \\ 2 & +20 & 38 \end{vmatrix} + 21 & 3$	Index correction
2011	-53 $58$ $-53$ $58$ $-53$ $58$	6 06 6 06	CL.	$\begin{vmatrix} +21 & 38 \\ +20 & 54 \end{vmatrix}$	E. ½ S. N.E.		$\begin{vmatrix} -1 & 2 \\ -1 & 1 \end{vmatrix}$	$\begin{vmatrix} 2 + 52 \\ 7 + 52 \end{vmatrix}$	$\begin{vmatrix} 2 + 21 & 08 \\ 2 + 20 & 29 \end{vmatrix}$	+52' by observa- tions made at the Magnetic Obser- vatory, Cape of Good Hope.
27 р.м	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	6 06 5 5 57	M.	$\begin{vmatrix} +20 & 53 \\ +22 & 03 \\ +19 & 56 \end{vmatrix}$	$\begin{array}{c} N. \\ E. \frac{1}{2} S. \\ s.w. by s. \frac{1}{2} S \end{array}$	<u> </u>	$\begin{bmatrix} -1 & 2 \\ + & 1 \end{bmatrix}$	$\begin{vmatrix} 2 + 5 \\ 2 + 5 \end{vmatrix}$	$2 + 20   54 \ 2 + 21   33 \ 2 + 21   00 \ $	
29 А.м		5 5 50	M.	$\begin{vmatrix} +19 & 48 \\ +16 & 07 \end{vmatrix}$	s.s.w. $\frac{1}{2}$ w. s.w. by s. s.w. $\frac{1}{2}$ s.	$\left  \right\} - 57 \ 48$	+ 1	2 + 5	$2   +22  ext{ } 16 > +21  ext{ } 2  2   +20  ext{ } 52  2   +17  ext{ } 18 $	3 Card unsteady.
29 р. м	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	3 4 00	M.		s.w. by s. s.w. $\frac{1}{2}$ s. s.w. $\frac{1}{3}$ s.	$\left  \right\rangle -59 0$	0 + 1 + 1	$\begin{vmatrix} 9 + 5 \\ 9 + 5 \end{vmatrix}$	0 1 1 4 5 6 1	O Card unsteady.
31 А.М	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	8 8 18 3 9 05	В. См		E. $\frac{1}{2}$ S. S.E. by S. S.E. by S.	Ĭ	$\begin{bmatrix} -1 & 4 \\ - & 4 \end{bmatrix}$	$\begin{vmatrix} 7 + 5 \\ 8 + 5 \end{vmatrix}$	$\begin{vmatrix} 2 & 2 & 3 & 3 \\ 2 & +2 & 1 & 40 \\ 2 & +2 & 0 & 36 \\ 2 & +19 & 31 \end{vmatrix}$	
31 p.m	-61 08 $-61 1$	8 9 05 5 9 30	CL	$\begin{vmatrix} +19 & 43 \\ +20 & 31 \end{vmatrix}$	s.e. by s.	61 3	$\begin{bmatrix} - & 4 \\ -1 & 0 \end{bmatrix}$	$\begin{vmatrix} 8 + 5 \\ 1 + 5 \end{vmatrix}$	$\begin{vmatrix} 2   + 19 & 47 \\ 2   + 20 & 22 \end{vmatrix}$	9 Unsteady,
	-61 2	$egin{array}{c ccc} 0 & 10 & 07 \\ 0 & 10 & 07 \end{array}$	M. CL	$\begin{vmatrix} +21 & 08 \\ +21 & 16 \\ +20 & 28 \end{vmatrix}$	S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.		_ 3 _ 3	$\begin{vmatrix} 1 + 5 \\ 1 + 5 \end{vmatrix}$	$\begin{vmatrix} 2 & +20 & 39 \\ 2 & +21 & 37 \\ 2 & +20 & 49 \end{vmatrix}$	
		0 10 07 0 10 07		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	J			$\begin{vmatrix} 2 & +19 & 44 \\ 2 & +19 & 42 \end{vmatrix}$	

				l			Correct	ions	<u> </u>		<del> </del>
		_	ver.					1			
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attrac-	Index.	Corrected De	eclination.	Remarks.
			0				tion.	II.			
1845.		١ ،	~	. ,	<u>'</u>	. 0	0 /	,		۰,	
Feb. 1 а.м. 1 г.м.	$-61 55 \\ -62 06$		СL. См.		s.e. by s.		- 48 - 48	+52	$\begin{vmatrix} +22 & 19 \\ +23 & 44 \end{vmatrix}$		
1 F.M.	-62 06	12 45	В.	$ +23 \ 40 \  +22 \ 21$	s.e. by s. s.e. by s.	-63 17			$  ^{+23}_{+22}   ^{11}_{25} \rangle$	+22 07	Very unsteady.
	-6206	12 55	Cr.	+20 12	S.E.	Į			+20 00	4.	
2 A.M. 2 F.M.			В. М.	$+2255 \\ +2519$	E.N.E. S.E. \frac{1}{2} E.				$\begin{vmatrix} +21 & 47 \\ +25 & 01 \end{vmatrix}$		
~ 1	-61 54		M.	+26 34	S.E. $\frac{1}{2}$ E.				+26 16		
	-61 55		T.	+23 04	S.E. ½ E.	<b>}</b> −63 28			$+22 \ 46$	+23 11	Unsteady.
	-61 54 $-61 54$		CL.	$\begin{array}{rrrr} +21 & 28 \\ +21 & 36 \end{array}$	s.e. by e. s.e. ½ e.		-1 18 $-1 10$		$\begin{vmatrix} +21 & 02 \\ +21 & 18 \end{vmatrix}$		· ·
	-6154	16 57	В.	+20 12	S.E. $\frac{1}{2}$ E.	Ì	-1 10	+52	+19 54		
3 4 37	-61 54 $-61 49$		Bn. T.	+27 44	S.E. \(\frac{1}{2}\) E.	K			$\begin{bmatrix} +27 & 26 \\ +27 & 04 \end{bmatrix}$	:	
O A.M.	-61 49		Bn.	$+27 56 \\ +25 32$	E.S.E. S.E. by E. ½ E.				$\begin{bmatrix} +27 & 04 \\ +24 & 48 \end{bmatrix}$		1
	-61 50	19 15	См.	+27 32	s.e. by E. $\frac{1}{2}$ E.		-1 36	+52	+26 48		
	-61 50 $-61 50$	19 06	В. М.	+27 19  +27 41	E.S.E. E.S.E.		_ 1 44		$\begin{vmatrix} +26 & 27 \\ +26 & 49 \end{vmatrix}$	_	
	-61 50		M.	+27 43	E.S.E.	>-64 20	-144	+52	+2651	+26 34	A less delicate point was used for the
	-61 50		M.	+27 15	E. by s.	l į			+26 04		suspension of the compass-card,
	$-61 50 \\ -61 50$	19 13 19 13	CL.	$\begin{vmatrix} +27 & 56 \\ +27 & 59 \end{vmatrix}$	E.S.E. E.S.E.		-1 44 $-1 44$	$+52 \\ +52$	$\begin{vmatrix} +27 & 04 \\ +27 & 07 \end{vmatrix}$		which made it much steadier.
	-61 50	19 13	Bn.	+27 32	E.S.E.	J	-144	+52	$+26 \ 40$		
3 р.м.			M.	+26 52	n.e. by n.	]	-1 34	+52	+26 10		
	-61 50 $-61 50$		CL.	1 ' '	$\begin{array}{c} \text{N.w.} \frac{1}{2} \text{ w.} \\ \text{w. by N.} \end{array}$		$\begin{vmatrix} + & 21 \\ +1 & 00 \end{vmatrix}$	+52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
	-61 50	19 14	CL.		w. by s.		+1 10	+52	+25 26		·
	-61 50 $-61 50$		CL.	$+23 \ 31$	W.S.W.		+1 07	+52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
,	-61 50		В.	$\begin{array}{r} +24 & 37 \\ +25 & 37 \end{array}$	N.W. by W.		$+ 29 \\ + 12$	+52	$+26 \ 41$		
	-6150	19 14	Cr.	+2452	N.W.	0	+ 12	+52	+25 56		
	-61 50 $-61 50$	19 14	CL. M.	$\begin{array}{r} +24 & 00 \\ +24 & 06 \end{array}$	w. by N. w.	-64 20	$+1 00 \\ +1 13$	$+52 \\ +52$	$\begin{vmatrix} +25 & 52 \\ +26 & 11 \end{vmatrix}$	+26 16	Card steady. Being a calm the decli-
	-61 50		M.	+23 51	w.		+1 13	+52	+25 56		nations were ob- served on different
	-61 50		Cr.	$ +25 \ 46 $	w.s.w.		+1 07	+52	+27 45		points of the com- pass to obtain the effect of the ship's
	1	19 14 19 14	CL.	$\begin{array}{r} +23 & 53 \\ +28 & 55 \end{array}$	s.w.				$\begin{bmatrix} +25 & 33 \\ +29 & 12 \end{bmatrix}$	·	iron. The com-
	<b>-61</b> 50	19 14	M.	+25 55	S. $\frac{1}{2}$ E.		- 11	+52	+26 36		wards placed in a copper-fastened
	-61 50 $-61 50$	19 14	M. M.	+24 45*	In the boat.			+52	$\begin{bmatrix} +25 & 37 \\ +27 & 36 \end{bmatrix}$		boat and the de- clination observed
4 А.М.		20 55		+27 03  +25 36	s. by E. s. ½ E.	Κ	_ 11	+52	+26 17		at a distance from the ship.
	-6200	20 55	M.	+2609	S. $\frac{1}{2}$ E.		11	+52	+26 50		
4 P.M.	$-62 00 \\ -62 05$	20 37	CL. M.		S. \frac{1}{2} E.				$ +27 \ 40 \   +29 \ 10$		
TI.M.	-62 07		M.		S.S.E. ½ E. S.S.E.	-64~40	_ 35	+52	+27 31 >	+28 05	Compass steady.
	-62 10	21 03	CL.	+28 15	S.S E.		_ 35	+52	+28 32		
	$ \begin{array}{rrr} -62 & 10 \\ -62 & 10 \end{array} $		BN.	+28 16  +30 14	S.S.E. S.S.E.		_ 35 _ 35	+52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
	-62 10	21 03	В.	+27 26	S.S.E.	J	35	+52	$+27 \ 43$		
5 А.М.	-63 14		M.	+29 01	s. by E.	Ŋ	- 19	+52	+29 34		
	-63 18 $-63 18$	21 10	CL.	+28   51	s. by E. s. ½ E.		11	+52 + 52	$\begin{vmatrix} +29 & 24 \\ +27 & 49 \end{vmatrix}$	. 00 =0	
	-63 18	21 10	Bn.	+28 47	S. $\frac{1}{2}$ E.	$-65 \ 35$	_ 11	+52	+29 28	+28.56	Steady.
Брм	-63 18 $-63 19$		Т. М.	$+28 08 \\ +28 14$	S. \frac{1}{2} E.		_ 11 _ 35	$+52 \\ +59$	$\begin{vmatrix} +28 & 49 \\ +28 & 31 \end{vmatrix}$		*
J F.M.	-00 19	~ 1 I U	1/1.	T ~5 14	S.S.E.	٧		102	F 200 61		

<sup>\*</sup> This observation is not much to be depended on, as the compass was very unsteady and difficult to observe.

			ن ا				Correct	ions.		
Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. Feb. 6 а.м.	-64 18	24 05	B.	+28   41 +28   29	S.S.E. S.S.E.	<u> </u>	- 42	+52	$\begin{array}{c c} +28 & 51 \\ +28 & 39 \end{array}$	
6 р.м.	-64 18 -64 20 -64 25 -64 35	24 02 24 10	M. M. CL.	$     \begin{array}{r}       +29 & 44 \\       +29 & 57 \\       +28 & 43 \\       +31 & 43     \end{array} $	s.s.e. s.s.e. s.s.e. ½ e. s.e. by s. ½ s.	\ -66 39	- 42 - 48	$+52 \\ +52$	$\begin{vmatrix} +29 & 54 \\ +30 & 07 \\ +28 & 47 \\ +31 & 45 \end{vmatrix} +30 & 24$	Card steady.
7 А.м.	-64 38 $-64 38$ $-64 25$	26 35 26 35 26 28	CL. Bn. M. M.	+31 22 +32 39 +31 06	S.S.E. S.S.E. S.S.E. ½ E.		- 42 - 42 - 48	$+52 \\ +52 \\ +52$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
/ A.M.	-65 25 $-65$ 16 $-65$ 16	27 45 27 45 27 45	B, CL, CL,	+32 02  +32 46  +30 41  +31 16	s.e. by s. s.s.e. s.s.e. ½ e. s.s.e. ½ e.		<ul> <li>42</li> <li>52</li> <li>52</li> </ul>	$+52 \\ +52 \\ +52$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
7 р.м.	$ \begin{array}{rrr} -66 & 02 \\ -66 & 02 \\ -66 & 02 \end{array} $	29 05 29 05	B <sub>N</sub> . B. C <sub>L</sub> . M.	+31 51 +31 12 +30 11 +30 25	S.S.E. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	-67 28	- 18 - 18	$+52 \\ +52$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Compass steady.
9 г.м.	-66 02 $-66 02$ $-66 02$	29 05 29 05 29 05 37 25	B. Bn. Cl.	+31 08 +31 00 +31 49 +36 04	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E. S.E. by E.	<u> </u>	- 18 - 18 - 18	$+52 \\ +52 \\ +52$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	:
10 а.м.	-66 26 $-66 26$ $-66 43$	37 25 37 25 38 32	B <sub>N</sub> . M. B.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.e. by e. s.e. by e. s. by w. ½ w.		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$+52 \\ +52 \\ +52$	+34 52 > +35 39 +36 18 > +38 44 > +	Steady.
10 р.м.	$ \begin{array}{rrr} -67 & 03 \\ -67 & 03 \\ -67 & 03 \end{array} $		Bn. Cl. Cl.	+35 26 $+34 23$ $+35 10$ $+39 35$	S.S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W. N. by W.	-69 22	$   \begin{array}{cccc}     + & 52 \\     + & 52 \\     - & 36   \end{array} $	$+52 \\ +52 \\ +52$	$ \begin{array}{c c} +37 & 00 \\ +36 & 07 \\ +36 & 54 \\ +39 & 51 \end{array} $	Steady.
11 А.м.	$ \begin{array}{rrr} -67 & 34 \\ -67 & 34 \end{array} $	39 41 39 41 39 41 39 41	CL.	$   \begin{array}{c cccc}     +40 & 06 \\     +40 & 11 \\     +39 & 26 \\     +36 & 03   \end{array} $	E. by s. E. by s. s.w. by s.	-69 38	$ \begin{array}{cccc} -2 & 30 \\ -2 & 30 \end{array} $	$+52 \\ +52$	$+38 \ 127$ $+38 \ 33$ $+37 \ 48$ $+37 \ 55$ $> +38 \ 13$	Card steady.
10	$     \begin{array}{rrr}     -67 & 34 \\     -67 & 34 \\     -67 & 38     \end{array} $	39 41 39 41 39 41 39 23	CL. B.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	S. N.N.E. S. ½ E.		$ \begin{array}{cccc}  & 02 \\  & 1 & 40 \\  & & 15 \end{array} $	$+52 \\ +52 \\ +52$	$   \begin{array}{c}     +38 & 31 \\     +38 & 09 \\     +38 & 26 \\     +36 & 50   \end{array} $	·
	$ \begin{array}{rrr} -66 & 38 \\ -66 & 47 \\ -67 & 06 \end{array} $	39 23 39 20 40 03	CL. M. CL.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. by E. S.S.E. S.S.E. N.E. <sup>1</sup> / <sub>2</sub> E.	\right	$ \begin{array}{rrr}  & 45 \\  & 45 \\  & 2 & 20 \end{array} $	$+47 \\ +47 \\ +52$	$\begin{array}{c c} +39 & 06 \\ +35 & 58 \\ +36 & 20 \end{array}$	Card A. unsteady.
	$     \begin{array}{rrr}     -67 & 06 \\     -67 & 06 \\     -67 & 06 \\     -67 & 06     \end{array} $	40 03 40 03 40 03	T. Bn.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. by E. N.E. by E. N.E. by E. N.E.by E. $\frac{1}{2}$ E.	-69 35	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$+52 \\ +52 \\ +52$	$\begin{array}{c c} +36 & 29 \\ +36 & 45 \end{array}$	Card J. steady.
	$ \begin{array}{rrrr} -67 & 01 \\ -67 & 01 \\ -64 & 52 \\ -64 & 52 \end{array} $	40 30 40 30 38 35	В. Сь. М.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.N.E. 1/2 E. s. by E. N.N.E.		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$+52 \\ +52 \\ +52$	$     \begin{array}{c}       +35 & 10 \\       +39 & 13 \\       +36 & 41 \\       +40 & 51    \end{array}     $	Very unsteady.
		38 37 38 37 38 37	CL. T. Bn.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. e.s.e. s.e. by e.	-68  47	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$+52 \\ +52 \\ +52$	$\begin{array}{c c} +35 & 08 \\ +34 & 55 \\ +35 & 37 \end{array} + 36 & 38$	Compass unsteady.
1 / P.M.	$ \begin{array}{rrrr} -64 & 52 \\ -64 & 52 \\ -64 & 52 \end{array} $	40 12 40 12 40 12	B <sub>N</sub> . M. CL.	+37 00  +35 28  +37 41  +38 20	S.S.E. S.S.E. S.S.E. S.S.E.	-68 31	<ul> <li>44</li> <li>44</li> <li>44</li> </ul>	$+52 \\ +52 \\ +52$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Steady.
	$-64 52 \\ -64 52$		Сь.	+37 54  +34 54	s.e. by s.		$ \begin{array}{c cccc} -1 & 06 \\ -1 & 06 \end{array} $	$+52 \\ +52$	$ \begin{array}{c c} +37 & 40 \\ +34 & 40 \end{array} $	

Date.	Lat.	Long.	Observer.	Declination	Ship's head.	Inclination.	Correct Ship's	1	Corrected Declination	Remarks.
		_	ops	observed.	-		attrac- tion.	Index.		
1845.										
Feb. 18 a.м.	$-6\mathring{4}$ 22	40 49	CL.	+3835	s. by E. ½ E.	) ° ′	_ ° 32	+52	+3855	(
	-6422		В.	$+34 \ 41$	N. by E. $\frac{1}{2}$ E.	-6840			+34 09 $+36 39$	Very unsteady.
19 р.м.					s.e. by E. $\frac{1}{2}$ E.	Κ			$+37\ 31$	
20 1 1	-6358		B <sub>N</sub> .		E.S.E.	60 40	_2 15	1 50	$+36\ 57 > +37\ 34$	Very unsteady.
	-63 56			+39 52	E. by s.	1 - 03 <del>4</del> 3			+38 14	very unsteady.
20 A M	-63 24		В.	+40 08		K :				
20 A.M.	-63 24		,	$+40 08 \\ +41 03$	s.E. by s.				$\begin{bmatrix} +39 & 52 \\ +39 & 51 \end{bmatrix}$	
	-63.22		B <sub>N</sub> .	1 -	s.E. by E. ½ E.		0 04			
	-63 22			1 .	s.E. by E. ½ E.	<b>  ≻</b> −70 09	-204			Unsteady.
00 m ve			M.	+39 39	s.e. by E. ½ E.	l i			+38 27	
20 р.м.		45 52		+39 50	s.e. by e.		1	1	+38 48	
01	-63 19 $-63 34$		CL.		s.e. by s.	K			+39 55	
21 а.м.				+39 46	E. by s. $\frac{1}{2}$ s.				$+38\ 10$	
	-63 34				S.S.E.				+39 03	
21	-63 34		Cr.	+39 20	S.S.E.	<b> </b>			+39 23	Co. 3 -4 - 0 3-
21 г.м.	_	47 03		1 .	S.E. ½ S.	<b>&gt;-70 08</b>			1 .	Card steady.
	$-63 \ 41$		В.	+42 45	S.E.				+42 00	
	-63 38			+41 11	S.E.				+40 26	
	$-63 \ 41$			+41 50	S.E.	Ų	I .	1	+41 05	
22 г.м.		49 29	CL.		S.S.W. $\frac{1}{2}$ W.	70 00			$+36\ 43$ $+39\ 2$	Very unsteady.
	$-63 \ 43$		Μ.	$+41 \ 31$	s. by E.	J -10 00	_ 24		1 + 41 59 J	
25 А.М.			В.	+41 03	E. $\frac{1}{2}$ N.	ח	1	Į.	+39 04	
	-61 36			+41 40	Е.	11			+39 35	
	-61 36		Bn.	$+42 \ 45$	E.	<b>}</b> −70 48	_2 57	+52	$+40\ 40\ $	Card steady.
25 р.м.		53 43	М.	$+40 \ 31$	s.e. by e.	1 -10 40	(—z 00		T 39 23 [	Cara Sicary.
	-61 30	1	CL.	+43 14	s.E. by s.	[ ]			+42 53	
	-61 28	1	M.	$+42\ 30$	S.E. \(\frac{1}{2}\) E.	IJ			$+41\ 26$	
26 а.м.		56 52	В.	+4244	s.	n	+ 03	+52	+43 39 \bar{\gamma}	}
	-61 19	57 26	M.	+43 56	S.E. ½ E.		-1 57	+52	+4251	
	<b>-61</b> 19	57 30	M.	+42 00	S.E. \(\frac{1}{2}\) E.	>-71 44	_1 57	+52	+40.55 ( $+41.5$	Very unsteady.
		57 18	CL.	+42 11	S.E. ½ E.	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	-157	+52	+41 06	1
26 р.м.	-61 17	58 30	CL.	+43 29	S.E.		_1 46	+52	+42 35	
	-61 17	58 30	M.	+41 42	S.E. 1/2 E.	IJ	-157	+52	+40 37	
27 A.M.	-61 02	62 55	В.	+46 08	Е.	ĺ Ì	-321	+52	+43 39 <sup>5</sup>	
	-6102	62 55	Bn.		S.E. 1 S.	1 70.50	-140	+52	+45 14	Very unsteady.
	-6102	64 10	M.	+47 17	S.E. $\frac{1}{2}$ S.	$-72\ 53$			$+46\ 29 > +45\ 1$	very unsteady.
27 р.м.	-61 10	65 00	CL.	+45 48	S.S.E.				+45 44	
28 р.м.			M.		S.S.E.	-73 50			$+4551^{2}+455$	Steady.
March 1 А.м.			CL.	+4609	S.S.E.	ח	_1 02	+ 52	+45 59	
	-62 10			+4604	S.S.E.	11	_1 02	+ 52	+45 54	
1 P.M.	-62 10	72 25		+46 19	S.S.E. 1/2 E.		_1 19	+52	+45 52	
		72 26		+47 55	s.e. by e.	>-74 34			+46 11 > +46 0	Compass steady.
	-62 10	72 26	CL.	+46 07	S.S.E. $\frac{1}{2}$ E.	11			+45 40	-
	-62 10	72 26	CL.	+46 12	S.S.E. 1/2 E.	11.			+45 45	
	$-62\ 10$	72 26	CL.	+47 31	s.e. by s.	] ]			$+46 \ 46$	
2 а.м.	-62 36	75 42	В.	+50 57	S. ½ E.	K			$+51 \ 39$	
,- 11.1	_62 43	76 05	M.		S. ½ E.	li			+50 21	
	_62 43	76 05	1	+49 31	s. by E.				+49 55	
	$-62 \ 43$	76 05	CL.		S. S.	11	1	,	+50 10	
	_62 43	76 05	См	+49 50	s. by E.	11			+50 14	
9. р.м.	$\begin{bmatrix} -62 & 46 \\ -62 & 46 \end{bmatrix}$		M.	+49 52	S. $\frac{1}{2}$ E.	<b>├ -74</b> 58			+50 34 > +50 3	Card steady.
~ 1.1/1.	62 46	76 50	T.	+48 18	S. ½ E.	1			2 +49 00	
	_62 46	76 50	CL.		S. $\frac{3}{4}$ E.	11			+49 10	
		76 59	В.	+50 33	s. 4 L.	11	1 00		+51 33	1.
	62 54	76 59		+50 17	s.	11	1 00		+51 17	1
		76 59		+51 31	s.	11	l' 00		2 + 52 31	
		1.5	1	01	1	٢	+ 08	1 "	1	

Dete	T		ver.	Declination	Shinin hard	T li di	Correct		Company Design	T.
Date.	Lat.	Long.	Observer.	observed.	Ship's head.	Inclination.	Ship's attrac- tion.	Index.	Corrected Declination.	Remarks.
1845. March 4 л.м. 5 л.м.	$-63^{\circ}05^{\circ}$ $-61^{\circ}41^{\circ}$	80.20 84.50	Ст М.	$+5\overset{\circ}{5} \overset{\prime}{33} \\ +50 \ 48$	E. $\frac{1}{2}$ N. S.E. $\frac{1}{2}$ S.	_76 2ó			$egin{pmatrix} +52 & 17 & +52 & 17 \ +49 & 13 \ \end{pmatrix}$	Very unsteady.
J A.M.	-61 42 $-61 41$	84 50 84 50	В. Сг.	+49 37  +52 14	S.E. S.E.	#C 10	-2 36 $-2 36$	$+52 \\ +52$	$\begin{array}{c cccc} +47 & 53 \\ +50 & 30 \end{array}$	
5 р.м.	$-61 \ 41$ $-61 \ 41$ $-61 \ 41$	84 50 85 59 85 59	T. Cl. B.	+49 55  +47 11  +46 36	S.E. $\frac{1}{2}$ S. S.E. $\frac{1}{2}$ S.	<i>&gt;</i> −76 43	-2 27 $-2 27$	+52	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Unsteady.
6 л.м.	$-61  41 \\ -60  51 \\ -60  51$	85 59 87 20 87 20	М. В. Вм.	$+46 24 \\ +52 54 \\ +49 16$	S.E. $\frac{1}{2}$ S. N.E. E.	$\begin{bmatrix} \\ -77 & 04 \end{bmatrix}$	-3 38	+52	$+44  49 \ +50  08 \ +45  36 > +47  47$	Compass unsteady.
7 А.м.	-6048	88 23 90 26 91 00	CL.	$ \begin{array}{c ccccc} +49 & 25 \\ +50 & 52 \\ +50 & 04 \end{array} $	S.E. S.S.E. S. by E.		$-2\ 40\ -1\ 20$	+52	$+47 \ 37 \ +50 \ 24 \ )$	
	-61 20 $-61 20$	91 00 $91 00$	CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	S. $\frac{1}{4}$ W. S. $\frac{1}{2}$ E.		$\begin{array}{ccc} + & 34 \\ - & 20 \end{array}$	+52 +52	$+4855 \\ +4719 \\ +5000$	
7 р.м.	-6128	91 00 91 58 91 58	CL.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	s.w. by s. s.w. by s.	$-77 \ 38$	$+2\ 13 + 2\ 13$	$+52 \\ +52$	+49 53	Unsteady.
	$ \begin{array}{rrr} -61 & 28 \\ -61 & 28 \\ -61 & 30 \end{array} $	91 58 91 58 92 00		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.w. by s. ½ s. s.s.w. s.s.w.		+1 38	$+52 \\ +52 \\ +52$		Amplitude.
8 А.м.	$ \begin{array}{rrr} -61 & 27 \\ -61 & 27 \\ -61 & 27 \end{array} $	91 32 91 32 91 32	B <sub>N</sub> . B. B <sub>N</sub> .	+5257	E.S.E. E.S.E	]	$ \begin{array}{rrrr} -4 & 11 \\ -4 & 15 \\ -4 & 11 \end{array} $	+52		
8 p.m.	-61 15	92 00		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by N. E. E.N.E.	-77 57	$ \begin{array}{rrrr} -4 & 20 \\ -4 & 46 \end{array} $	$+52 \\ +52$		Card steady.
9 а.м.	-61 03 $-60 58$	91 49 92 02	T. B. Bn.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. by s. E.N.E.	] ]	-4 23 $-4 34$	$+52 \\ +52$	$     \begin{array}{r}                                     $	·
	-60 58 $-60 50$	92 04 92 10	Bn. B.	$+52 \ 42 \\ +52 \ 59$	n.e. by e. E.n.e. E.n.e.	-77 32	$-4 34 \\ -4 34$	$+52 \\ +52$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Compass unsteady.
9 р.м. 10 а.м.	$ \begin{array}{rrr} -60 & 30 \\ -60 & 22 \\ -60 & 03 \end{array} $		B. Bn.		E. E.S.E. E. by s. ½ s.		$ \begin{array}{c cccc} -4 & 11 \\ -4 & 20 \end{array} $	$+52 \\ +52$	$egin{array}{cccc} +47 & 56 \ +47 & 41 \ +44 & 41 \ \end{array}$	
10 р.м.	$ \begin{array}{ccc} -60 & 03 \\ -60 & 03 \\ -60 & 03 \end{array} $	94 01 96 30 96 30	M. CL.	$ \begin{array}{c cccc} +46 & 11 \\ +48 & 10 \\ +47 & 54 \end{array} $	E. by s. s.E. s.E.	$-77 \ 37$	-249	+52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Unsteady.
	$ \begin{array}{rrr} -60 & 01 \\ -59 & 31 \\ -59 & 31 \end{array} $	100 45	CL.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.e. by s. N.E. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E.		-4 54	+52	$     \begin{array}{r}       +37 & 08 \\       +40 & 44 \\       +42 & 09     \end{array}   $	
	$     \begin{array}{r}       59 & 31 \\       \hline       59 & 31 \\       \hline       59 & 31     \end{array} $	$100 \ 45 \ 100 \ 45$	CL. T.	$   \begin{array}{c cccccccccccccccccccccccccccccccccc$	N. ½ E. N. ½ E. N. ½ E.	$-79 \ 31$	-1 46 $-1 46$	$+52 \\ +52$		Very unsteady.
12 А.М.	-59 31 $-58 31$	$     \begin{array}{ccc}       100 & 45 \\       98 & 59     \end{array} $	CL.	$^{+45}_{+42}_{31}$	N. by E. $\frac{1}{2}$ E. N.E. by N.	$\begin{bmatrix} -78 & 50 \end{bmatrix}$	$     \begin{array}{rrr}       -2 & 38 \\       -3 & 33     \end{array} $	$+52 \\ +52$	$egin{pmatrix} +44 & 09\ +39 & 50 & +39 & 50 \end{bmatrix}$	Very unsteady.
13 р.м.	$   \begin{array}{r}     -58 & 30 \\     -58 & 30 \\     -58 & 30   \end{array} $	98 32 98 32	CL.	$\left. \begin{array}{c c} +42 & 58 \\ +43 & 51 \end{array} \right $	N.E. by E. $\frac{1}{2}$ E. E. N.E. E. $\frac{1}{2}$ S.	-78 10	$     \begin{array}{rrr}     -4 & 58 \\     -4 & 33     \end{array} $	$+52 \\ +52$	$+40\ 10$	Very unsteady.
	$     \begin{array}{r}         -56 & 56 \\         -56 & 50 \\         -55 & 50     \end{array} $	101 20	CL.	$ \begin{array}{c cccc} +40 & 48 \\ +40 & 46 \\ +36 & 52 \end{array} $	E.S.E. E.S.E. E. by N.	$\left78 \ 26 \right $	$     \begin{array}{rrr}     -4 & 02 \\     -5 & 01     \end{array} $	$+52 \\ +52$	+37 30 $+32 43$	Very unsteady.
15 р.м.	_55 40 _55 35	103 18	M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	E. $\frac{1}{2}$ S. E. by S.	\rightarrow -78 33	-4 33	+52	$\begin{array}{c c} +31 & 56 \\ +34 & 02 \end{array}$	Very unsteady.

			ï.				Correct	ions.		
Date.	Lat.	Long.	Observèr	Declination observed.	Ship's head.	Inclination.	Ship's attraction.	Index.	Corrected Declination.	Remarks.
1845. Mar. 16 A.m. 16 p.m.		108 03 103 08		$+30^{\circ} 31^{'} +32 16^{'}$	N.E. N.E. ½ E.				$egin{pmatrix} +2\mathring{7} & 3\acute{6} \\ +29 & 12 \end{bmatrix}$	
10 P.M.	$ \begin{array}{r rrrr} -54 & 42 \\ -54 & 38 \end{array} $	106 08 106 28 106 28	T. M.	$\begin{vmatrix} +32 & 06 \\ +33 & 16 \end{vmatrix}$	N.E. ½ E. E. E.	<b>-78</b> 41	-356 $-446$	$+52 \\ +52$	1 on 00	Very unsteady.
17 а.м.	$-54  36 \\ -54  05$	106 28	Bn.	$\begin{vmatrix} +34 & 13 \\ +34 & 45 \\ +29 & 19 \\ +32 & 02 \end{vmatrix}$	E. by s. E. ½ s.	$\left  igcep {1 \over 2} - 79 \ 04  ight.$	$-4  46 \\ -4  52$	$+52 \\ +52$	$[+30 \ 51]$	Very unsteady.
18 а.м.	-53 30 $-53 14$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Bn. M.	$\begin{vmatrix} +25 & 18 \\ +22 & 05 \\ +26 & 50 \end{vmatrix}$	N.N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.	\\ \-77 34	$\begin{bmatrix} -2 & 37 \\ -2 & 58 \\ -4 & 01 \end{bmatrix}$	$+52 \\ +52 \\ +52$	$egin{array}{c cccc} +23 & 33 \\ +19 & 59 \\ +23 & 41 \\ \end{array}$	Very unsteady.
I .	-53.08 $-53.08$		Cr.	$\begin{vmatrix} +26 & 25 \\ +23 & 34 \\ +20 & 00 \end{vmatrix}$	N.E. $\frac{1}{2}$ E. N. $\frac{1}{2}$ W.		$\begin{bmatrix} -3 & 47 \\ -4 & 01 \\ - & 48 \end{bmatrix}$	$+52 \\ +52$	$\begin{bmatrix} +25 & 30 \\ +20 & 25 \\ +20 & 04 \end{bmatrix}$	
19 р.м. 20 а.м.	$     \begin{array}{r rrr}     -49 & 29 \\     -49 & 29    \end{array} $	8 110 30 2 112 34 2 112 34	Bn. Bn.	$\begin{vmatrix} +18 & 23 \\ +23 & 05 \\ +21 & 06 \end{vmatrix}$	N.N.E. N.E. by N. N. by E. ½ E.	h	$\begin{bmatrix} -2 & 49 \\ -2 & 04 \end{bmatrix}$	+52 + 52	$\begin{vmatrix} +21 & 08 \\ +19 & 54 \end{vmatrix}$	Very unsteady,
20 p.m.	-49 00 $-49 00$		M. CL.		N.N.E. N.E. 12 N.	-76 17	$\begin{bmatrix} -3 & 25 \\ -3 & 10 \end{bmatrix}$	$ +52 \\ +52$	$\begin{vmatrix} +18 & 38 \\ +16 & 53 \\ +15 & 40 \\ +16 & 12 \end{vmatrix} + 17 & 09$	Compass unsteady.
N. AMERICAN PROPERTY OF THE PR	$\begin{bmatrix} -48 & 59 \\ -48 & 54 \end{bmatrix}$	$egin{array}{cccccccccccccccccccccccccccccccccccc$	T. T.	$ \begin{array}{r} +18 & 30 \\ +21 & 50 \\ +17 & 12 \\ +17 & 24 \end{array} $	N.E. $\frac{1}{2}$ N. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.		$\begin{bmatrix} -3 & 35 \\ -3 & 35 \end{bmatrix}$	+52 + 52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
		$     \begin{bmatrix}       6 \\       112 \\       54     \end{bmatrix}   $	M. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} \\ -74 & 30 \\ \\ \end{bmatrix}$	-3 35 - 45 - 45	$ +52 \\ +52$	$\begin{bmatrix} +14 & 50 \\ +12 & 02 \\ +8 & 50 \end{bmatrix}$	1
	-4456	4 116 55	M. M.	$\begin{vmatrix} +10 & 38 \\ + & 7 & 12 \\ + & 5 & 40 \end{vmatrix}$	N. by w. $\frac{1}{2}$ w. n. by w.	$\left  \left\{ -73.27 \right. \right $	- 30 - 42	+52 + 52	$\begin{bmatrix} +10 & 27 \\ +7 & 34 \\ +5 & 50 \end{bmatrix}$	Very unsteady.
BOCTRACACOMINENTES	-43 45 -43 45	2 116 59 2 116 59 2 116 59	Сь. Т.	$\begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N. 1/2 W. N. N.	$\left  \begin{array}{c} -72 & 28 \end{array} \right $	-1 00 $-1 00$	+52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Card unsteady.
25 p.m. 26 a.m 26 p.m	-40 5	911642 $411642$	M. CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. $\frac{1}{2}$ E. N. by W. N. by W.	$\left.\right _{-70}^{1}$	- 33	+52  +52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Card unsteady.
	-39 0	0 116 15	M. Cl.	$\begin{vmatrix} + & 7 & 09 \\ + & 6 & 26 \end{vmatrix}$	n. by w. n. by w. n. by w. n. by e.	68 27	— 33 — 33	$\frac{+52}{3+52}$	I C AE I	Compass steady.
28 р.м	-38 0 $-37 0$	$\begin{array}{c} 2 \\ 116 \\ 19 \\ 2 \\ 116 \\ 38 \\ 6 \\ 116 \\ 38 \\ \end{array}$	M. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N. by E. N. by E. \( \frac{1}{2} \) E N.N.E.	$\begin{array}{c} \\ \\ \\ \\ \\ \end{array}$	$\begin{bmatrix} -1 & 20 \\ -1 & 11 \end{bmatrix}$	+52	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	l Steady.
29 а.м	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	6 116 35 3 116 40 2 116 40	M. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.N.E. $\frac{1}{2}$ E. N. by E. N. by E.		$\begin{bmatrix} -1 & 33 \\ -1 & 07 \\ -1 & 07 \end{bmatrix}$	$\frac{3}{7} + 52$	$2 + 4 32 \rfloor + 4 34 \gamma$	
A PARTY TO	$\begin{bmatrix} -36 & 1 \\ -36 & 1 \\ -36 & 1 \end{bmatrix}$	3 1 1 6 4 ( 2 1 1 6 4 ( 1 1 1 6 4 (	CL. T. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	n. by E. n. by E.	$-65 \ 44$	$\begin{bmatrix} -1 & 0 \\ -1 & 0 \\ - & 5 \end{bmatrix}$	7 + 52 $7 + 52$ $3 + 52$	$\begin{bmatrix} 2 & + & 4 & 14 \\ 2 & + & 4 & 37 \\ 2 & + & 5 & 37 \end{bmatrix} + 4 59$	Steady.
29 P.M	$\begin{bmatrix} -36 & 1 \\ -36 & 0 \end{bmatrix}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E. N.E. $\frac{1}{2}$ E.		-1 56 -1 56 -1 56	$\frac{6 +52}{6 +52}$	$\begin{bmatrix} + & 4 & 57 \\ + & 5 & 44 \end{bmatrix}$	*
30 а.м	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ 9   117   41 \\ 9   117   41 \\ 4   117   41 \\ 4   117   41 $	CL.	$\begin{vmatrix} + & 6 & 54 \\ + & 4 & 52 \end{vmatrix}$	S.E. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	65 36	i — 13	$\frac{9+52}{3+52}$	+ 6 47	Compass steady.
30 р.м	-351				S. ½ E. S.	J			2 + 7 12	

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Correction Ship's attrac-		Corrected Declination.	Remarks.
			0				tion.	In	, ·	
1845. Mar. 31 A.M. April 1 A.M.				$+\mathring{7} \ 5\mathring{9} \ +9 \ 57$	N.E. ½ E. N.N.E.	$-6\overset{\circ}{5} \overset{\circ}{20} \\ -65 \overset{\circ}{00}$	$-\mathring{1} \ 5\acute{6} - 1 \ 22 - 1$	+ 52 + 52	$+ \stackrel{\circ}{6} \stackrel{55}{5} + \stackrel{\circ}{6} \stackrel{55}{5} + 9 \stackrel{27}{27} + 9 \stackrel{27}{27}$	Unsteady. Unsteady.
11 A.M. 14 A.M.	-35 02 King G Sound, A	eorge's	CL.	$\begin{vmatrix} +4 & 17 \\ +4 & 53 \\ +4 & 58 \end{vmatrix}$	Observed	on shore.	-	+ 52	$ \begin{vmatrix} +5 & 09 \\ +5 & 45 \\ +5 & 45 \end{vmatrix} $	Card J. Card J. Card A.
21 A.M. 22 A.M. 23 A.M.	$     \begin{array}{r rrr}     -35 & 10 \\     -35 & 42     \end{array} $	118 06 115 40	M. M.	$\begin{vmatrix} +3 & 48 \\ +5 & 10 \\ +3 & 05 \end{vmatrix}$	w. by s. s.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 52 + 52		Card J. unsteady. Unsteady.
23 р.м.	$-35 38 \\ -35 23$	114 50	M. M. M.	$\begin{vmatrix} +4 & 33 \\ +6 & 29 \\ +6 & 31 \end{vmatrix}$	N.N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ N. N.W. by N.	-65 11	- 09 - + 09 -	+ 52 + 52	$\begin{array}{c c} +5 & 16 \\ +7 & 30 \\ +7 & 19 \end{array}$	Unsteady.
24 A.M.	$     \begin{array}{rrr}     -34 & 20 \\     -34 & 17     \end{array} $	113 15 113 12 113 05	CL.	$\begin{vmatrix} +6 & 10 \\ +5 & 34 \\ +5 & 00 \end{vmatrix}$	n.w. by n.	<b>}−64 44</b>	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 52 + 52	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Card unsteady.
Noon. 25 A.M.	$\begin{bmatrix} -32 & 48 \\ -32 & 48 \end{bmatrix}$	111 44 111 45	М. См.	$\begin{vmatrix} +6 & 55 \\ +6 & 04 \end{vmatrix}$	n.w. by n. n.w. by n. n.w. by n.	$\begin{cases} -62 & 18 \end{cases}$	- 08 - 08	+ 52 + 52	$\begin{array}{c c} +7 & 39 \\ +6 & 48 \end{array}$	QL. I
	-32 35	111 43 111 40	CL.	$\begin{vmatrix} +5 & 20 \\ +5 & 05 \\ +5 & 53 \end{vmatrix}$	N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N. N.W. by N.		- 06 - 08	$^{+}_{+}52$	$\begin{array}{c c} +5 & 51 \\ +6 & 37 \end{array}$	Steady.
26 а.м. 26 р.м.	-30 31 $-30 26$	109 15 108 58	B <sub>N</sub> .	$\begin{vmatrix} +5 & 58 \\ +6 & 25 \\ +5 & 58 \end{vmatrix}$	n.w. by n. n.w. by n. n.w.	$\left.\right\}$ -60 30	- 12 - 02 - 02	$+52 \\ +52$	$ \begin{array}{c c} +6 & 38 \\ +7 & 05 \\ +6 & 52 \end{array} $	Unsteady.
27 л.м.	-29 20 $-29 20$	106 55	М. См.	$\begin{vmatrix} +7 & 52 \\ +6 & 04 \\ +5 & 00 \end{vmatrix}$	N.W. N.W. ½ W. N.W.	$\left. \begin{array}{c} 1 \\ -59 & 25 \end{array} \right.$	$\begin{vmatrix} + & 10 \\ + & 02 \end{vmatrix}$	$+52 \\ +52$	$     \begin{array}{c}     +8 & 46 \\     +7 & 06 \\     +5 & 54    \end{array}     +6 & 30 $	Steady.
28 A.M. 28 P.M. 29 A.M.	-27 25	106 36 106 34 105 16	CL.	$\begin{vmatrix} +8 & 27 \\ +4 & 26 \\ +3 & 56 \end{vmatrix}$	n. by w.	$\left.\right\}$ -57 22	- 50 - 40	+ 52 + 52	$ \begin{vmatrix} +8 & 29 \\ +4 & 38 \end{vmatrix} $ +6 33 $ \end{vmatrix}$ +4 41	Very unsteady.
30 л.м.	$ \begin{array}{r rrrr} -26 & 10 \\ -26 & 10 \end{array} $	105 16 105 16 102 30	CL. Bn.	$\begin{vmatrix} +5 & 52 \\ +5 & 28 \\ +3 & 58 \end{vmatrix}$	N.W. N.W. W.N.W.	-55 07	- 07 - 07	+ 52 + 52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Very unsteady.
Мау 1 л.м.	_24 05	102 26 99 26	M.	$\begin{array}{ c c c c } +4 & 42 \\ +3 & 02 \\ +3 & 00 \end{array}$	w.n.w. w. w.	$\left.\begin{array}{c} -54 & 30 \\ \hline \end{array}\right)$	$\begin{vmatrix} + & 20 \\ + & 38 \end{vmatrix}$	$+52 \\ +52$	+5 54 $+4 32$ $+4 32$	Very unsteady.
Noon.	$     \begin{array}{r}       -23 & 58 \\       -23 & 58     \end{array} $	99 22 99 13	M. M. M.	$\begin{vmatrix} +4 & 25 \\ +4 & 30 \\ +7 & 57 \end{vmatrix}$	w. w.		+ 38 - + 38 -	+ 52 + 52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Unsteady.
2 A.M.	$   \begin{bmatrix}     -24 & 01 \\     -24 & 01 \\     -24 & 01 \\     -24 & 01   \end{bmatrix} $	97 34 97 34	M. Bn.	$\begin{vmatrix} +7 & 57 \\ +7 & 50 \\ +6 & 26 \\ +6 & 47 \end{vmatrix}$	N. by E. \frac{1}{2} E.  N.N.E.  N. by E. \frac{1}{2} E.  N.N.E.	-54 11	-1 00 -	+ 52 + 52	$\begin{array}{c c} +7 & 42 \\ +6 & 20 \end{array}$ \right\right\rightarrow 7 & 08	Compass steady.
3 а.м.	$   \begin{array}{r}     -23 & 55 \\     -23 & 55 \\     -23 & 55   \end{array} $	95 58 95 58	M. M.	$\begin{vmatrix} +5 & 58 \\ +4 & 58 \\ +3 & 40 \end{vmatrix}$	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.		+ 40 + 40 +	+ 52 + 52	+7 30 +6 30	
3 р.м.	$ \begin{array}{rrrr} -24 & 00 \\ -24 & 00 \\ -23 & 55 \end{array} $	95 25 95 25	М. Сь.	$\begin{vmatrix} +4 & 41 \\ +4 & 05 \\ +4 & 42 \end{vmatrix}$	W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S.	-54 21	+ 33 + + 33 + + 40 +	⊢ 52 ⊢ 52 ⊢ 52	$\begin{array}{c c} +6 & 06 \\ +5 & 30 \\ +6 & 14 \end{array}$	Steady.
4 A.M.	~	94 08 94 10	Сь. М.	$\begin{vmatrix} +5 & 09 \\ +4 & 22 \\ +3 & 51 \end{vmatrix}$	W.N.W. W.N.W. W.N.W.	$\begin{cases} -54 & 07 \end{cases}$	+ 12 + 12 + 12 + 12 + 12 + 12 + 12 + 12	- 52 - 52	$\begin{array}{c c} +6 & 13 \\ +5 & 26 \\ +4 & 50 \end{array} +5 & 31 \end{array}$	Card J. steady. Card A. steady.
Noon. 5 A.M. 6 A.M.	$-24 17 \\ -24 05$	93 58 92 11	M. CL. M.	$\begin{array}{c} +4 & 30 \\ +6 & 05 \\ +4 & 38 \end{array}$	w.n.w. n.w. by n.	52 44	+ 12 + $-$ 23 +	- 52 - 52	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Card J. steady. Steady.
U A.M.	$ \begin{array}{rrrr} -22 & 54 \\ -22 & 54 \\ -22 & 54 \\ -22 & 50 \end{array} $	90 50 90 50	B <sub>N</sub> . C <sub>L</sub> .	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. N.W. N.W.		$-\begin{array}{ccc} - & 13 + \\ - & 13 + \end{array}$	- 52 - 52	+5 36 +5 28 +5 43	
6 р.м.	$-22 \ 39$			+5 59	n.w. by n.	-52 49			+6 28 > +5 56	Compass steady.

			l				Correct	ions.		1
Doto	Tat	Tona	Observer.	Declination	Shim's has d	Inclination		T	Commented Declination	D
Date.	Lat.	Long.	psei	observed.	Ship's head.	Inclination.	Ship's attrac-	Index.	Corrected Declination.	Remarks.
			0				tion.	In	,	
1845.	0 /	0 (		0 /		0 /	0 1		0 / 0 /	
Мау 6 р.м.		90 32	M.	+612	N.N.W.	>-52 49		+52		Compass steady.
	-22 39 $-22 39$		Bn. Cl.	$  \begin{array}{c cccccccccccccccccccccccccccccccccc$	n.w. by n. n.w. by n.		- 23	$+52 \\ +52$	$\begin{array}{c c} +5 & 09 \\ +6 & 22 \end{array}$	
Sunset.		90 32	CL.	+6 33	N.W. Dy N.		- 34	+52	$\begin{array}{c c} +6 & 22 \\ +6 & 51 \end{array}$	
7 А.М.	-21 53	89 42	Μ.	+3 30	N.W.	$\left.\right\} -52 01$	- 18	+52	+4 04	Unsteady.
	-2153		CL.	+4 09	N.W.	$\int_{0}^{\infty} -3z = 0$		+52	$+4 \ 43$	Onsteady.
8 а.м.	-20 48 $-20 47$	88 <b>0</b> 8 88 <b>0</b> 5	M. M.	$\begin{vmatrix} +3 & 42 \\ +3 & 53 \end{vmatrix}$	n.w. by w. n.w. by w.			$+52 \\ +52$	$\begin{pmatrix} +4 & 24 \\ +4 & 35 \end{pmatrix}$	
	$-20 \ 45$		CL.	+3 25	n.w. by w.	>-51 15	_ 10	+52	+4 07 > +4 45	Card steady.
	$-20 \ 45$	88 05	B <sub>N</sub> .	+4 11	n.w. by w.		_ 10	+52	+4 53	
Noon.	-20 38 $-20 37$		M. M.	+430	$W_{\bullet} \stackrel{1}{\overset{1}{2}} N_{\bullet}$	$\exists$		+52	$+5 \ 48 \ $	
9 л.м.	$-20 \ 37$ $-20 \ 37$	85 39 85 39	CL.	$  \begin{array}{c} +4 & 38 \\ +3 & 28 \end{array}  $	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$	>-51 18	+ 26 + 26	$+52 \\ +52$	$\begin{array}{c} +5 & 56 \\ +4 & 46 \\ \end{array} > +5 & 20 \end{array}$	Steady.
Noon	$-20 \ 37$		M.	+4 00	$W \cdot \frac{1}{2} N \cdot$	<b>5 10</b>		+52	$+5$ 18 $\int$	- county v
10 а.м.	-20 25	82 45	M.	+4 12	$W_{\bullet} \frac{1}{2} N_{\bullet}$	<b>)</b>	+ 26	+52	+5 30	
·	-20 25 $-20 25$	3	M. Bn.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$W_{\bullet} \stackrel{1}{\overset{1}{2}} N_{\bullet}$	51 00		+52	+5 35	Vors unstand
			CL.	$+3 00 \\ +3 26$	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$	-51 22	1	$+52 \\ +52$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Very unsteady.
	-20 25	82 30	Т.	+408	$W_{\bullet} \stackrel{1}{\stackrel{1}{2}} N_{\bullet}$	]	+ 26	+52	+5 26	
11 А.М.			M.	+2 56	$W. \frac{1}{4} N.$	)		+ 52	+4 12	
ŀ	$     \begin{array}{rrr}     -20 & 36 \\     -20 & 36     \end{array} $		M. Bn.	$\begin{array}{c c} +2 & 31 \\ +2 & 27 \end{array}$	W. 4 N.		1	$+52 \\ +52$	$\begin{array}{c c} +3 & 47 \\ +3 & 43 \end{array}$	
	$-20 \ 36$		CL.	+3 12	W. 4 N. W. 1 N.	<b>├</b> -51 48		+52		Compass unsteady.
11 р.м.	<b>—20 36</b> ]	79 00	M.	+4 48	$W. \frac{1}{4} N.$		+ 24	+52	+6 04	
	$     \begin{array}{rrr}     -20 & 36 \\     -20 & 36     \end{array} $		T.	+4 34	$W \cdot \frac{1}{4} N \cdot$		1	+52	+5 50	
12 а.м.	$     \begin{bmatrix}       -20 & 36 \\       -20 & 44     \end{bmatrix} $		M.	$\begin{array}{c c} +3 & 43 \\ +5 & 38 \end{array}$	W. $\frac{1}{4}$ N.	$\langle \ \  $		$+52 \\ +52$	$\begin{array}{c} +4 & 59 \ +5 & 40 \end{array}$	
			CL.	+628	N.			+52	+630	
.  -		78 34	M.	+506	N.N.W.		0-1	+ 52	+5 20	
-	$-20 \ 44$ $-20 \ 44$	78 34   78 34	CL.	$\begin{array}{c c} +6 & 32 \\ +5 & 27 \end{array}$	N.N.W.			+52   +52	$\begin{array}{c c} +6 & 46 \\ +5 & 57 \end{array}$	
	$-20^{\circ}$		CL.	$+5 \frac{27}{12}$	N.W.		i	+52	$\begin{array}{c c} +5 & 37 \\ +5 & 42 \end{array}$	
	-20 44	78 34	M.	+3 23	W.N.W.		1	+52	+4 19	
.  -		78 34	CL.	+5 36	w.n.w.			+52	$+6 \ 32$	
		78 34   78 34	M. CL.	$\begin{array}{c c} +2 & 23 \\ +4 & 09 \end{array}$	w. w.			$+52 \\ +52$	$\begin{array}{c c} +3 & 35 \\ +5 & 21 \end{array}$	
	$-20 \ 44$	- 1	M.	+258	w.s.w.	-52 02		+52	+4 05 > +5 29	To obtain corrections for the ship's
	-20 44	- 1	CL.	+4 22	w.s.w.		+ 15	+52	+5 29	attraction. A calm, heavy swell,
	$-20 \ 44$ $-20 \ 44$		M. CL.	$\begin{array}{c c} +4 & 20 \\ +4 & 26 \end{array}$	s.w.		+ 06	$+52 \\ +52$	$\begin{array}{c c} +5 & 18 \\ +5 & 24 \end{array}$	compass unsteady.
	$-20 \ 44$		M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.w. s.s.w.			+52	$\begin{array}{c c} +5 & 24 \\ +5 & 37 \end{array}$	
	-20 44	78 34	CL.	+4 48	s.s.w.		- 01	+52	+5 39	
.	-20 44	78 34	M.	+4 42	s.		- 08	+52	+5 26	
		78 34 78 34	CL. M.	$\begin{array}{c c} +4 & 29 \\ +5 & 41 \end{array}$	S.			+52   +52	$\begin{array}{c c} +5 & 13 \\ +5 & 20 \end{array}$	
[	$-20 \ 44$	78 34	CL.	+6 00	E.N.E.			+52	$\begin{array}{c c} +5 & 20 \\ +5 & 39 \end{array}$	
	-20 44	78 34	M.	+6 21	N.N.E.	j .	- 57	+52	+6.16	
13 а.м.			CL.	+4 11	w.	7	+ 20	+52	+5 23	
	-20 39 $-20 39$	77 45	T. M.	$\begin{array}{c c} +4 & 29 \\ +3 & 49 \end{array}$	w. w.	-51 59		$+52 \\ +52$	$+5 \ 41 + 5 \ 01$ $+5 \ 22$	Steady.
14 A.M.	-20 28	76 23	M.	+3 + 43 + 43	$\mathbf{w} \cdot \frac{1}{2} \mathbf{N} \cdot$	٦ ١	+ 16	+52	+5 51	
	-20 28	76 23	B <sub>N</sub> .	+4 25	$W \cdot \frac{1}{2} N \cdot$	-52 20	+ 16	+52	+5 33 > +6 01	Very unsteady.
15 а.м.	$-20 28 \\ -20 45$	76 23	CL.	+5 31	W. $\frac{1}{2}$ N.	50 05	+ 16	+52	$+6 \ 39$	
16 A.M.	$-20  45 \\ -20  27$	73 20 70 49	M. M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$W \cdot \frac{1}{2} N \cdot W \cdot \frac{1}{2} N \cdot$	-52 25	+ 16	$+52 \\ +52$	$+5 54 +5 54 +7 20 \ +6 35$	Unsteady.
	$-20 \ 27$		CL.	$+4 \ 43$	$W \cdot \frac{1}{2} N \cdot$	$\left. \left. \right\} -52 \ 35 \right $	+ 16	+52	$\begin{array}{c} +7 & 20 \\ +5 & 51 \end{array} \} +6 & 35$	Card unsteady.
<u> </u>	· · · · · · · · · · · · · · · · · · ·					-	(			CHE MITTERIOR SCRIPT COMPANY TO PROPERTY PROPERTY AND ADDRESS OF THE PROPERTY

.i				·			Correct	tions.		
Date.	Lat.	Long.	Observer.	Declination	Ship's head.	Inclination.	Ship's	Ι.	Corrected Declination.	Remarks.
2400	nav.	Long.	Obse	observed.	omp s nouce	incimation.	attrac-	Index.	Corrected Decimation.	Tomar Ks.
							tion.	1		
1845.	9 /	aº	~	. 2 .6			/		8 - 1 > 0 /	
Мау 17 л.м.		1 - 1	CL.		w.	-53 01	+20	+ 52		Card unsteady.
18 а.м.		69 35 68 30	CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\mathbf{w}$ . $\mathbf{w}$ . $\frac{1}{4}$ s.	1	$+20 \\ +20$	$ +52 \\ +52$	T 0 0/ )	
10 A.M.		68 22	M.	+624	w. by s.		+18	+52		1
P.M.		68 04	M.	+ 7 35	N.N.W.	<b>}−53</b> 06	-37	+52		Compass steady.
~		68 04	B <sub>N</sub> .	+ 8 59	N.N.W.		-37	+52	1	
Sunset.		68 00	M.	+ 7 45	N. by $w.\frac{1}{2}w$ .	J	-47	+52	1 2	
19 А.М.	1	$\begin{vmatrix} 67 & 54 \\ 67 & 54 \end{vmatrix}$	M. CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. $\frac{1}{2}$ N.	-53 24	$-19 \\ -23$	$ +52 \\ +52$		lard steady.
		67 54	Т.	+ 511	N.W. $\frac{1}{2}$ N.	-33 24	-23	+ 52		oura steady?
20 л.м.	l .		CL.	+624	w. by N.	52 40	$+15^{\circ}$	+52		Steady
l	l .	67 29	B <sub>N</sub> .	+636	w. by N.	$-53 \ 49$	+15	+52	1 1 20 1	occur.
21 а.м.		66 26	CL. Bn.	1 ' -	w. by n.	E2 56	+15	+52		
1		66 26	M.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	w. by n. w. by n.	-53 56	+15 + 15	$ +52 \\ +52$		
22 A.M.	$-20 \ 41$	63 16	Μ.	+ 7 17	w. by N.		+15	+52	1 0 047	
Sunset.		62 44	М.	+ 7 23	w. by N.	$\left.\right\}$ -53 53	+15	+52		
23 A.M.		59 42	CL.	+ 8 40	w. by n.	7	+15		+ 9 47	
		59 42 59 42	Bn. M.	$\begin{vmatrix} + & 8 & 12 \\ + & 9 & 00 \end{vmatrix}$	w. by n. w. by n.	-54 09	+15 + 15	$+52 \\ +52$	$\begin{vmatrix} + & 9 & 19 \\ + & 10 & 07 \end{vmatrix}$ + 9 44	
24 а.м.			M.	$+\ 8\ 15$	$W \cdot \frac{1}{2} N \cdot$	J -53 56		+52		Very unsteady.
27 A.M.		57 31	M.	+ 8 31	On shore.			+52	+ 9 23 }	Port Louis, Mauri-
		57 31	M.	+ 9 13	) On shore.				+10 05	tius.
29 A.M.	i	55 31	CL. M.	-	W.	-54 00	+26		$\left  \begin{array}{ccc} +10 & 31 \\ +11 & 50 \end{array} \right  +11 & 15 \end{array}$	Card steady.
30 а.м.	$\begin{bmatrix} -20 & 50 \\ -21 & 30 \end{bmatrix}$	55 33 53 10	M.	$\begin{vmatrix} +10 & 47 \\ +12 & 09 \end{vmatrix}$	$w. \frac{1}{2} N.$ s.w.byw. $\frac{1}{2}$ w.	3	+20 + 19		$\begin{vmatrix} +11 & 59 \\ +13 & 20 \end{vmatrix}$	
P.M.		52 58	CL.		s.w. by w.	11	+16		1 19 50 1	
	_22 02	52 58	В.	+12 34	s.w. by w.	$-54 \ 45$	+10	+52	$\begin{vmatrix} +13 & 32 \\ +13 & 42 \end{vmatrix} + 13 & 44 \end{vmatrix}$	
01		52 58	M.	1 .	s.w. by w.	K	+16	+52	+14 02	
31 р.м.	$-23  44 \\ -23  44$	1 .	CL.	1 .	s.w.byw. <del>1</del> w. s.w.byw. <del>1</del> w.		+19 + 19		$\begin{vmatrix} +13 & 28 \\ +14 & 59 \\ +14 & 22 \end{vmatrix}$	Card unsteady.
	)	51 48	M.	+13 28	s.w.by $w.\frac{1}{2}w$		+19		+14 39	
June 1 A.M.	1	1	CL.	+14 16	w.s.w.	$\left  \frac{1}{2} \right  = 57 \ 19$	+27	+52	+15 35 \ +15 00	(Imatoo du
l		49 40	M.	+13 24	w.s.w.	3 -37 19	1 +21		T14 40 ]	Insteady.
2 A.M.	$\begin{bmatrix} -26 & 30 \\ -26 & 30 \end{bmatrix}$	49 20 49 20	M. CL.	$ +15 \ 38  +15 \ 25$	N.W.	$  \    \    \    \    \    \    \    \$	$\begin{bmatrix} -01 \\ -01 \end{bmatrix}$		$\begin{vmatrix} +16 & 29 \\ +16 & 16 \end{vmatrix} + 16 & 23 \end{vmatrix}$	
1	$-26 \ 30$		T.	$+15 25 \\ +15 32$	N.W.	7-30 30	01		$\begin{vmatrix} +16 & 10 \\ +16 & 23 \end{vmatrix}$	
4 A.M.	1 .	1 -	CL.	+19 50	w. by s.	li l	+48		+21 30)	
	27 10	46 09	CL.	+19 01	w. by s.		+48	+52	+20 41	
1	-27 07	46 14	M.	+17 56	w. by s.	$-58 \ 38$			$ +19 \ 36 > +20 \ 25 $	Very unsteady.
4 P.M. Sunset.		45 59 45 39	CL.	$ +19 \ 18  +17 \ 38$	w. by s.		+48    +51		+20 58     +19 21	•
5 A.M.			CL.	+17 36 + 19 40	w.	K	$+31 \\ +31$		+21 037	
	_28 19	43 11	M.	+21 14	w.	-58 31	+31	+52	$ +22 \ 37 > +21 \ 19 ^{\circ}$	Card very unsteady.
	_28 20	43 00	CL.	+18 55	w.	Ŋ	+31		+20 18	
6 а.м.		42 07			N.W. by W.		+12		+21 02	
}		42 10 42 11	M.	$\begin{vmatrix} +19 & 47 \\ +21 & 48 \end{vmatrix}$	N.w. by w.	<b>├</b> —59 01	$  \begin{array}{c} +12 \\ +12 \end{array}$	$+52 \\ +52$	$\begin{vmatrix} +20 & 51 \\ +22 & 52 \end{vmatrix}$ +21 57	Very unsteady.
1		42 00	M.	+22 00	N.w. by w.	]]	+12		$\begin{bmatrix} +23 & 02 \\ +23 & 04 \end{bmatrix}$	
7 A.M.	_28 32	40 32	M.	+21 48	w. by n.	Ď.	+22	+52	+23 02	
1	28 38	40 20	M.		w. by N.		+22		$+22 \ 43$	
7 8 14	1	40 32		$\begin{vmatrix} +21 & 04 \\ +21 & 17 \end{vmatrix}$	w. by n.	-58 54	$+22 \\ +22$		$\begin{vmatrix} +22 & 18 \\ +22 & 31 \end{vmatrix}$	Unsteady.
7 P.M.		39 52		$ +21 \ 04 $	w. by N.		+22	+52	$\begin{bmatrix} +22 & 31 \\ +22 & 18 \end{bmatrix}$	
1					1			1		

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Ship's attraction.		Remarks.
1845. June 8 A.M. 8 P.M.	-28 53 -28 56 -28 56 -28 58	37 55 37 56 37 56 37 49	M. M. Cl. T. M.	+21 41 +22 17 +21 49 +22 00 +21 44 +23 19	W. W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S. W. W. $\frac{1}{2}$ S.	-59 11	$egin{array}{cccccccccccccccccccccccccccccccccccc$	52 + 23 05 52 + 23 41 52 + 23 12 52 + 23 19 52 + 23 08 52 + 24 42	
Sunset. 9 A.M. 11 A.M. 11 P.M.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	37 37 36 04 35 46 33 45	CL. M. CL. M. CL.	+22 48 +25 36 +24 38 +26 28 +24 42 +27 05	W. ½ S. W. ½ S. W. ½ S. W. ½ S. N.W. by W. W. ½ N.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right\} - 57 59$	+ 31 + + 30 + + 30 + - 07 + + 24 +	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Very unsteady.
12 A.M. 13 A.M.	$     \begin{array}{rrrr}     -30 & 30 \\     -30 & 30 \\     -30 & 35 \\     \hline     \end{array} $	33 41 33 41 33 41 33 13 31 39	M. Bn. Cl. M. M. M.	+26 59 +27 43 +29 36 +23 58 +25 15 +25 22	N.E. s.E. $\frac{1}{2}$ E. W. by N. W. by s. $\frac{1}{2}$ s. W. by s. $\frac{1}{2}$ s.	$ \begin{vmatrix} -56 & 37 \\ 5 & -57 & 19 \end{vmatrix} $	$\begin{vmatrix} -1 & 10 \\ - & 40 \\ - & 46 \\ + & 19 \\ + & 25 \end{vmatrix}$	52 + 26   41 $52 + 27   55 $ $52 + 29   42$	Very unsteady.
13 р.м.		31 30 31 28 31 39 31 34 2 31 28	M. M. Bn. CL. CL. M.	+25 13 +25 25 +27 16 +25 46 +24 39 +25 06	w. by s. ½ s. w. by s. ½ s. w. by s. ½ s. w. by s. w. by s. w. by s. w. by s. s.w.byw.½ w. s.w.byw.½ w.		$\begin{vmatrix} + & 25 \\ + & 25 \\ + & 26 \\ + & 25 \\ + & 21 \\ + & 21 \end{vmatrix}$	52 + 26 30  52 + 26 42	Card steady.
14 A.M.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	31 23 29 51 3 29 45 3 29 45 0 29 55	CL. M. CL. T. CL.	$\begin{array}{r} +25 & 26 \\ +28 & 06 \end{array}$	s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.w. $\frac{1}{2}$ s.w. $\frac{1}{2}$ s.w. $\frac{1}{2}$ s.w.	ال.	$\begin{vmatrix} + & 21 \\ + & 22 \\ + & 30 \\ + & 31 \end{vmatrix}$	52 + 26 39 $52 + 29 20$ $52 + 28 24$	4 Card unsteady.
15 Noon	-34 36 -34 46 -34 46 -34 46	5 27 12 5 27 02 0 27 10 0 27 10 5 27 00	T. M. CL. Bn. CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} W. \ \frac{1}{2} \ S. \\ W. \ \frac{1}{2} \ N. \\ W. \ \text{N.w.byw.} \ \frac{1}{2} W. \end{array}$	-57 06	$\begin{vmatrix} + & 30 \\ + & 26 \\ + & 26 \\ + & 26 \\ + & 26 \end{vmatrix}$	52 + 27 45 52 + 27 26 52 + 29 16 52 + 29 39 52 + 28 10 52 + 29 44	1
" P•M	-34 51 $-34$ 51 $-35$ 36 $-35$ 46	25 58 1 25 58	M. CL. M. Bn. CL.	$\begin{vmatrix} +27 & 54 \\ +27 & 54 \\ +27 & 11 \end{vmatrix}$	N.w. by w.  N.w. by w.  w. \frac{1}{2} \text{ S.}  w. \frac{1}{2} \text{ S.}  w. by N.  w. by N.	  -56 08	$egin{array}{c c} 00 + & 00 + \\ 00 + & 27 + \\ + & 27 + \\ 3 + & 17 + \\ \end{array}$	52 + 28 46 52 + 28 46 52 + 28 30 52 + 28 45 52 + 29 15 52 + 29 23	6 Card unsteady.
18 А.м	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$egin{array}{cccccccccccccccccccccccccccccccccccc$	CL. M. M. CL.	$     \begin{array}{r}       +31 & 16 \\       +28 & 38 \\       +28 & 21 \\       +26 & 41     \end{array} $	N. $\frac{1}{2}$ E. N.W. $\frac{1}{2}$ W. W.N.W. W. by S. S.W. $\frac{3}{4}$ S. S.W. $\frac{3}{4}$ S.	$ \begin{vmatrix}     -55 & 25 \\     -55 & 08 \\     -54 & 50 \end{vmatrix} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6
20 А.М	-34 56 $-34 56$		CL.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.W. N.W.byW.½W N.W.½ W.	-54 00	$\begin{vmatrix} - & 19 \\ 00 \end{vmatrix} +$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	7

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Correct Ship's attraction.	Index.	Corrected Declination.	Remarks.
	servator of anchor in Simon's Bay.	A Cape of Good Hope.	CL.	+28 52 +28 23 +28 23 +27 40 +27 28 +27 14 +27 40 +28 36 +29 30	Correction	the Index as for Cards true Decli+29 07.	- 37 - 19 + 04 + 26 + 21 + 11 + 02 - 07 - 20 - 39 -1 01 -1 23 -1 19 -1 09	+52 $+52$	+29 21 +30 02 +29 47 +29 38 +29 51 +29 29 +29 34 +29 18 +29 18	To obtain the corrections for the ship's iron.  Card J. error ~52'.  Card A. error -47'.

Observations of the Inclination made on board Her Majesty's hired Bark "Pagoda," from the 10th of January to the 21st of July 1845, with Needle A (Fox C. 9). Face East.

Observer Lieut. T. E. L. MOORE, R.N. One hour after Noon.

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attrac- tion.	Index.	Corrected Inclination.	Remarks.
1845. Jan. 10.	34 46	1 <b>7 46</b>	Direct. Needle N. Needle S. Mag. N. Mag. N.S.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by n.	$\left.\right _{+63}$	- 26	-53 34	Fresh breeze, a head swell.
11.	- 35 29	15 09	Mag. S. Direct. Direct. Needle N. Needle S. Mag. N.S.	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by n. w. by n. n.w. by w. n.w. by w. n.w. by w. n.w. by w.		-26	51 27	A little motion.
12.	-35 17	14 00	Mag. N. Mag. S. Direct. Needle N. Needle S. Mag. N.S. Mag. N.	-52 15 -52 09 -51 45 -52 17 -51 20 -51 56 -51 29	N.W. by W. N.W. by W. W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S. W. $\frac{1}{2}$ S.		-26	51 16	A little motion.
13.	-35 24	13 23	Mag. S. Direct. Direct. Needle N. Needle S. Mag. N.S. Mag. N.	$\begin{array}{rrrr} -51 & 26 \\ -51 & 31 \\ -51 & 38 \\ -51 & 31 \\ -50 & 41 \\ -51 & 42 \\ -51 & 18 \end{array}$	$\begin{array}{c} \text{W.} \frac{1}{2} \text{ S.} \\ \text{W.} \frac{1}{2} \text{ S.} \\ \text{S.W.} \frac{1}{2} \text{ S.} \end{array}$	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right. + 27$	-26	-51 19	A little motion.
15.	-38 42	14 27	Mag. S. Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S.	-53 47 -52 36 -53 38 -53 19	s.w. $\frac{1}{2}$ s. s. by w. $\frac{1}{2}$ w. s. by w. $\frac{1}{2}$ w.	+18	<b>-26</b>	-53 31	A head' swell, table unsteady.
16.	-39 10	14 38	Direct. Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S.	$\begin{array}{rrrrr} -53 & 33 \\ -54 & 03 \\ -54 & 24 \\ -53 & 30 \\ -54 & 07 \\ -54 & 05 \end{array}$	s. by w. ½ w. s. w.byw.½ w. s.w.byw.½ w. s.w.byw.½ w. s.w.by w.½ w. s.w.by w.½ w. s.w.by w.½ w. s.w.by w.½ w.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right\} + 12$	-26	54 12	Table very unsteady.
17.	-40 41	14 16	Direct. Direct. Needle N. Needle S. Mag. N.S.	$     \begin{array}{r}       -33 & 36 \\       -53 & 36 \\       -55 & 17 \\       -55 & 27 \\       -54 & 47 \\       -55 & 22     \end{array} $	s.w.by w.½ w. s.w.by w.½ w. w.s.w. w.s.w. w.s.w.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right\}$	-26	<b>—54</b> 59	A heavy head swell, much motion.
21.	50 21	10 31	Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S.	-55 39 -55 32 -55 15 -55 49 -55 25 -55 31	s.w. s.w. s.w. s.w.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right\} + 24$	-26	55 34	Moderate breezes, a little motion.

								Correc	tions.		
Date.	Lat.		Lone	~	Method	Observed	Ship's head.	Ship's		Comments I I will be at a second	D
Date.	Lat.		Long	<b>g.</b>	employed.	Inclination		attrac-	Index.	Corrected Inclination.	Remarks.
								tion.			
1845.	0	,	0.			0 1				0 /	
Jan. 23.	$-\mathring{50}$	48	1 0°	18	Direct.	-57 23	s.w.byw. <u>1</u> w.	J			
					Needle N. Needle S.	-57 45 57 07	s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.				
					Mag. N.S.	-57   07   07   07   07		> +34	- 26	-57 19	A little motion.
					Mag. N.	-57 28	s.w.byw. $\frac{1}{2}$ w.	, , , , ,		0, 13	A fittle motion.
		- (			Mag. S.	-5719	s.w.byw. $\frac{1}{2}$ w.				
24.	51 4		9	9 <b>6</b>	Direct. Direct.		s.w.byw.½w.	5 1			
24.	31 4	24	9	30	Needle N.	-57 24 $-57 42$	s.w. by w. s.w. by w.	} +30	-26	-57 28	Moderate breeze,
24.	-51 5	56	9	30	Direct.	-57  41	s.w.byw.½w.	1			table steady.
			-		Mag. N.S.	-5746	s.w.byw. $\frac{1}{2}$ w.	>+28	-26	-5742	A head swell, much
2		.		00	Direct.		s.w.byw. $\frac{1}{2}$ w.	7			motion 44 P.M.
25.	53 %	51	7	32	Direct. Needle N.	-57 20 -57 51	s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.				
					Needle S.		s.w.byw. <del>2</del> w.				
					Mag. N.S.	-57.24	s.w.byw. w.	>+28	-26	-57 24	Ship passing through
					Mag. N.		s.w.byw. ½w.				streams of loose ice.
		- 1			Mag. S. Direct.		s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.			*	
26.	54 (	02	6	02	Direct.	-57 $56$	w. by N.	5 I			
					Needle N.	-5749	w. by N.				
					Needle S.	-5702	w. by N.		- 0		
					Mag. N.S. Mag. N.	-57 55 $-57 05$	w. by N.	>+61	-26	<b>-56 58</b>	Table steady, small pieces of loose ice
					Mag. S.	$-57   05 \\ -57   18$	w. by n. w. by n.			·	about the ship.
					Direct.	-5743	w. by N.				
27.	-55 ]	18	5	<b>55</b>	Direct.	-5730	S.S.W. ½ W.	<u>ا</u> ا			
		1			Needle N. Direct.	-58 23 $-57 54$	s.s.w. ½ w.	<b>&gt;</b> +10	26	-58 12	Ship pitching hea- vily, fresh breezes.
31.	-61	14	9	07	Direct.	-61 13	S.S.W. ½ W. S.S.E.	۲ ۱			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
		-	Ū	••	Needle N.	$-61 \ 41$	S.S.E.				
					Needle S.	$-60 \ 41$	S.S.E.		- 0		
					Mag. N.S. Mag. N.	-61 04 $-60 58$		>+05	-26	-61 43	Table steady, heavy snow.
					Mag. S.	-61 26	S.S.E.				
					Direct.	-61 23			,		
Feb. 1.	62 (	06	12	52	Direct.	-6256	s.e. by s.	η. Ι			
		1			Needle N. Needle S.	$-62 \ 41$ $-62 \ 36$	s.e. by s.	> 0	26	-63 17	Much motion, table
					Direct.	$-62 \ 30$ $-63 \ 12$					very unsteady, heavy snow.
2.	-61	56	16	36	Direct.	-6359	S.E. $\frac{1}{2}$ E.	ň l			
					Needle N.	-62 25	S.E. $\frac{1}{2}$ E.				
		1			Needle S. Needle N.S.	$     \begin{array}{r r}     -63 & 37 \\     -63 & 53     \end{array} $		+13	06	-63 55	Heavy snow, a head
					Mag. N.	-64 02		10	20	- 0.5 33	sea, ship pitching
					Mag. S.	-63 51	8.E. 1/2 E.				violently, water clear from ice.
	<b>6-</b>	-,	••		Direct.	-64 09		J	_		
3.	-61	50	19	14	Direct.	-65 09 $-64 49$		+25			
					Direct.	-65 00		+92  +47	-26	-64 44	Calm.
1					Direct.	-6459	w.s.w.	+25			
	00	.		40:	Direct.	-64 44	1	+03	J		
4.	-63	UU	20	40	Direct. Needle N.	-64 13 $-64 12$					
					Needle S.	-63 39	s.w.		- 00	CA OF	
					Needle N.S.	-64 06	s.w.	+03	—2b	-64 25	Unsteady.
					Mag. N.	-6359					
					Mag. S.	-64 06	s.w.	<u> </u>			

						Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	0 /	0.1.		0 1		,	,	0 /	
Feb. 5.	$-63\ 19$	21 48	Direct.	$-6\mathring{5}$ 17	S.S.E.	רו רו			
			Needle N.	-64 39	S.S.E.				
			Needle S. Needle N.S.	-64 29	S.S.E.	<b> </b> }−15	- 26	-65 35	House and from
			Mag. N.	$\begin{vmatrix} -64 & 39 \\ -64 & 46 \end{vmatrix}$	S.S.E. S.S.E.	7-15	20	-09 99	Heavy swell from S.E., light breez
			Mag. S.	-64 52	S.S.E.				table steady.
			Direct.	$-65 \ 25$	S.S.E.				[
6.	-64 25	24 18	Direct.	-66 17	S.S.E. 1/2 E.	j l		1.	
			Needle N.	-66 16	S.S.E. 1/2 E.				
			Needle S.	-65 28	S.S.E. $\frac{1}{2}$ E.	<b>&gt;-14</b>	-26	$-66 \ 41$	Table steady.
			Needle N.S.		S.S.E. ½ E.				j
	Cr 90	00.40	Direct.	-66 07	S.S.E. 1 E.	Y			į.
7.	-65 39	28 48	Direct. Needle N.		s. by E. ½ E. s. by E. ½ E.				
			Needle S.		s. by E. $\frac{1}{2}$ E. s. by E. $\frac{1}{2}$ E.				
			Needle N.S.		s. by E. $\frac{1}{2}$ E.		-26	-67 56	Table steady.
			Mag. N.		s. by E. $\frac{1}{2}$ E.				
			Mag. S.		s. by E. $\frac{1}{2}$ E.				
8.	-66 27	30 45	Direct.	-68 28	s.E. by E.	ו ו			
			Needle N.	-6809	s.e. by e.				
			Needle S.	-6749	s.e. by e.	1	06	60 91	
	}		Needle N.S. Mag. N.	$-68 04 \\ -68 08$	s.e. by e.	$\rangle + 05$	26	$-68 \ 31$	Fresh breeze, table steady.
			Mag. N.	-68 06	s.e. by e.				
-			Direct.	-68 26	s.E. by E.				
9.	$-66 \ 36$	36 50	Direct.	-6911	s.e. by e.	K			
			Needle N.	-69 13	s.e. by e.				
			Needle S.	$-68 \ 40$	s.e. by e.				
			Needle N.S.		s.e. by e.	>+05	-26	-69 22	Light breeze, very steady.
			Mag. N.	-6859	s.e. by e.			<b>-</b> ₹1.	
			Mag. S. Direct.	-69 02 $-69 20$	s.e. by e.				
10.	-67 10	38 51	Direct.	$-70 \ 12$	s. by w.	K 1			
10.	0, 10	00 01	Needle N.	-70 53	s. by w.				
			Needle S.	-70 02	s. by w.				
			Needle N.S.		s. by w.	<b>├</b> —32	-26	<b>-71 07</b>	Steady.
			Mag. N.	-70 00	s. by w.				
			Mag. S.	-70 12	s. by w.				
	67 20	40 28	Direct.	-70 05 $-70 33$	s. by w.	Ĭ I			
11.	-67 39	40 20	Needle N.	-70 35 $-70 26$	N.E.	\rangle + 89	-26	-69 27	Strong breeze, sail
12.	-67 18	40 22	Direct.	$-69 \ 36$	S. $\frac{1}{2}$ E.	K			ing along a pack of ice, unsteady
1 2.	0, 10		Needle N.	$-69 \ 43$	S. $\frac{1}{2}$ E.				
			Needle S.	-68 58	S. $\frac{1}{2}$ E.				
			Needle N.S.		S. ½ E.	>-32	-26	-70 20	Fresh breeze, tabl unsteady.
	ļ.		Mag. N.	-69 18	$S_{\bullet} \frac{1}{2} E_{\bullet}$				
			Mag. S.	-69 03	S. ½ E.				
13.	-66 55	40 16	Direct.	-69 28 $-70 12$	S. \(\frac{1}{2}\) E.	Κ. Ι		19	
10.	-00 00	70 10	Needle N.	$-70^{-12}$ $-70^{-28}$	E.N.E. E.N.E.				
			Needle S.	-69 54	E.N.E.				
	4		Needle N.S.	-70 08	E.N.E.	+67	-26	-69 30	A swell from the eastward, table
	]		Mag. N.	-70 14	E.N.E.				unsteady.
			Mag. S.	-7006	E.N.E.				
	1		Direct.	-70 13	E.N.E.	IJ			

*						Corre	ctions,		
Date.	Lat.	Long.	Method employed.	Observed. Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.		0. 4					,	0 / 0 /	
Feb. 14.	-6624	40 01	Direct.	-7038	n.e. by n.				
		* 1	Needle N.	-70 07	N.E. by N.	>+89	-26	-69 15	Very squally, with thick weather,
			Needle S. Direct.	$\begin{vmatrix} -70 & 10 \\ -70 & 17 \end{vmatrix}$	n.e. by n.				thick weather, table unsteady.
16.	-64 62	38 37	Direct.	-68 03	s. by E.	K			
			Needle N.	-68 13	s. by E.				
			Needle S.	-67 20	s. by E.	-30	-26	-68 53	A heavy swell, un-
			Needle N.S.		s. by E.			00 00	steady.
	,		Mag. N. Mag. S.	$\begin{vmatrix} -67 & 52 \\ -68 & 06 \end{vmatrix}$	s. by E.				
17.	-64 43	40 12	Direct.	-69 58	s. by E.	K			
			Needle N.	-70 02	N.				
			Needle S.	-69 22	N.		_	_	
			Needle N.S.		N.	>+76	-26	-68 18	Calm, a heavy sea, not steady.
			Mag. N.	-68 25	N.				not sicacy.
	,		Mag. S. Direct.	-68 30 $-68 50$	N. N.				
19.	-64 05	41 09	Direct.	$-70 \ 13$	E. by s.	K	oc	<b>50.00</b>	
		_	Needle N.	-69 52	E. by s.	} +27	-26	<b>-70 02</b>	Observed the inner circle to have
20.	-63 19	45 52	Direct.	-7029	s.e. by <b>E.</b> ½ E.	ŀή			moved, table very unsteady.
			Needle N.	-6951	s.e. by $e.\frac{1}{2}e.$	+10	-26	-70 147	A heavy swell.
			Needle S. Needle N.S.		s.e. by e. ½ e. s.e. by e. ½ e.				
	-63 22	45 58	Direct.	-69 54	S.E.	Κ ΄		>-70 15	
	00	10 00	Needle N.	-69 53	S.E.	1	o.c	70.35	
			Needle S.	-69 06	S.E.	>-08	-26	<b>-70 15</b>	Strong breezes, with a heavy sea run-
-	00.00		Needle N.S.		S.E.	IJ			ning.
21.	$-63 \ 36$	46 46	Direct.	-69 38	S.E.	П			
			Needle N. Needle S.	$     \begin{array}{r rrr}     -69 & 39 \\     -69 & 03     \end{array} $	S.E.	-08	-26	<b>−70 05</b> γ	Table unsteady, eight icebergs in
			Needle N.S.		S.E.			1	sight.
	-63 36	46 50	Direct.	-70 01	S.E.	К.		>-70 13	
			Needle N.	-7002	S.E.				
			Needle S.	-69 34	S.E.	-10	-26	-70 21	
			Needle N.S. Mag. N.	$ \begin{array}{r rrrr} -69 & 32 \\ -69 & 37 \end{array} $	S.E.	>-10	-20	-70 213	Much motion.
			Mag. S.	-69 32	S.E.		1		
			Direct.	-70 00	S.E.			B+	
25.	-61 34	53 49	Direct.	-7044	S.E. ½ E.	ň.			
			Needle N.	-70 22	S.E. 1/2 E.				
			Needle S. Needle N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E. $\frac{1}{2}$ E.	-05	-26	<b>-70</b> 49	Table 1 A
			Mag. N.	-70 08	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1	-20	70 19	Iceblink to the southward, fresh
			Mag. S.	<b>-70 08</b>	S.E. $\frac{1}{2}$ E.				breezes, table unsteady.
	_		Direct.	-7042	S.E. 1/2 E.				
26.	-61 19	57 33	Direct.	-71 03	S.E. ½ E.	ň ·			
,			Needle N.	-71 24	S.E. ½ E.	<b> </b>	-26	-71 26	No ice in sight,
			Needle S. Needle N.S.	$\begin{vmatrix} -70 & 26 \\ -70 & 40 \end{vmatrix}$	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.				unsteady.
	-61 22	57 41	Direct.	-70   40 $-71   01$	S.E. 2 E.	K			
		• ==	Needle N.	-71 22	S.E.	11			
			Needle S.	-70 30	S.E.	_13	-26	-71 27	Fresh breeze, table
			Needle N.S.		S.E.	1	~~	1. ~1	steady.
			Mag. N.	-70 29	S.E.				
			Mag. S.	$-70 \ 40$	S.E.	<u>U</u>			

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	0 /	0 /					,	0 / 0 /	A PARTIE AND A STATE OF THE PARTIES AND ADDRESS
Feb. 27.	-6116	64 20	Direct.	$-71^{\circ}20$	S.S.E. ½ E.	200	00		
			Needle N. Needle S.	$\begin{vmatrix} -71 & 48 \\ -71 & 10 \end{vmatrix}$	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	>-26	-26	<b>-72</b> 18	Very unsteady.
28.	-61 49	71 30	Direct.	-71 10 -72 44	S.S.E.	Υ :			
			Needle N.	-7249	S.S.E.				
			Needle S. Needle N.S.	$     \begin{array}{r rrr}     -72 & 36 \\     -72 & 43     \end{array} $	S.S.E.	>-33	-26	-73 36	Table steady.
			Mag. N.	-72   43 $-72   34$	S.S.E. S.S.E.				
			Mag. S.	-72 18	S.S.E.	ا ا		>-73 38	
	-61 49	71 30	Direct.	-7245	S.S.E.				
			Needle N. Needle S.	$-73 01 \\ -72 12$	S.S.E. S.S.E.	>-36	-26	<b>-73 40</b>	Steady.
			Needle N.S.		S.S.E.	)			
Mar. 1.	-62 10	72 25	Direct.	$-73 \ 37$	s.e. by s.	ا (			
			Needle N. Needle S.	$-73 54 \\ -73 25$	s.e. by s.				
			Needle N.S.		s.E. by s.	>-26	-26	<b>-74</b> 33	Calm, table steady.
			Mag. N.	-73 39	s.e. by s.				
2.	-62 47	76 14	Mag. S.	$-73 \ 45$	s.E. by s.	$\forall$			
z.	-02 4/	76 14	Direct. Needle N.		s. by E. ½ E. s. by E. ½ E.				
			Needle S.	-73 39	s. by E. $\frac{1}{2}$ E.	-40	-26	-74 557	
			Needle N.S.	$-73 \ 45$	s. by E. $\frac{1}{9}$ E.	7-40	20	-/+ JJ	
			Mag. N. Mag. S.		s. by E. ½ E. s. by E. ½ E.			75.05	Standulunana tahla
	-6249	76 16	Direct.	-74 11	s. by E. 2 E. S.	√		>-75 US	Steady breeze, table steady.
`			Needle N.	-74 21	s.		- 0		
			Needle S. Needle N.S.	$-73  43 \\ -73  58$	s.	<b>}−45</b>	<b>-26</b>	<b>一75 15</b> ノ	
			Direct.	-74 10	s. s.				
3.	-64 20	79 38	Direct.	-75 02	s. by w. ½ w.	j l			
			Needle N.		s. by w. ½ w.	-40	o.c	<b>-75 57</b>	Squalls of snow,
			Needle S. Needle N.S.	-74 39 $-74 41$	s. by w. ½ w. s. by w. ½ w.	>-40	-26	-15 57	fresh breeze, un- steady.
ľ			Direct.		s. by w. $\frac{1}{2}$ w.				stoney.
5.	-6142	85 07	Direct.	-76 13	S.E. $\frac{1}{2}$ E.	j			
l		- 4	Needle N. Needle S.	-76 40 $-76 18$	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	>-17	-26	<b>-76</b> 58	Fable very unsteady,
[			Needle N.S.	<b>-75 59</b>	S.E. $\frac{1}{2}$ E.		~0	, 000	a strong breeze, aurora visible.
	Co. 10		Direct.	-76 06	S.E. $\frac{1}{2}$ E.	ا لِ			
6.	$-60 \ 48$	88 33	Direct. Needle N.	$ \begin{array}{c c} -76 & 21 \\ -76 & 41 \end{array} $	S.E.				
[			Needle S.	-76 06	S.F. S.E.				
			Needle N.S.	<b>-75 46</b>	S.E.	>-23	-26	-77 04 Y	Very unsteady.
			Mag. N. Mag. S.	$ \begin{array}{c cccc} -75 & 56 \\ -76 & 16 \end{array} $	S.E.				
į			Direct.	-76 26	S.E. S.E.	1 1		` '	
7.	-61 23	91 15	Direct.	-76 26	s.s.w.	<b>i</b> 1			
l			Needle N.	-77 02	s.s.w.	1 1			
			Needle S. Needle N.S.	-76 12 $-76 28$	s.s.w.	-46	-26	<b>-77 41</b>	Aurora visible.
			Mag. N.	<b>-76 13</b>	s.s.w.				
ĺ			Mag. S.	$-76 \ 35$	s.s.w.			,	
8.	-61 07	92 10	Direct.	-76 26 $-78 11$	s.s.w. E. by s.	ا +13	_26	-78 247	
	31 01	<i>32,</i> 10	Needle N.	<b>-77</b> 39	E.S.E.	ا ` ا	~~		Aurora visible; table
			Needle S.	<b>-76</b> 55	E.S.E.	00	-26	<b>-77</b> 29	unsteady; snow.
			Needle N.S. Direct.	-76 39   -76 59	E.S.E. E.S.E.				
		,	Direct.	-10 03	230130240	, 1			· .

·						Corre	ctions.		· ·
Date.	Lat.	Long.	Method. employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.		0 /		9 /			,		
Mar. 9.	-60 30	92 34	Direct.	-7712  -7731	E.S.E.	-01	-26	<b>−77</b> 37	
			Needle N. Needle S.	$\begin{vmatrix} -77 & 31 \\ -76 & 49 \end{vmatrix}$	s.e. by e.			<b>├</b> ─77 33	Very unsteady, aurora visible.
			Needle N.S.		s.e. by E.	<b> </b> \>-10	-26	-77 28J	Wallett Visioner
			Direct.	$-76 \ 41$	s.e. by E.				
10.	-60 03	96 03	Direct.	-77 10	s.e. by e.	<b>ו</b>			
			Needle N.	-77 25	s.e. by e.	>-10	-26	<b>-77</b> 38	Table unsteady,
			Needle S. Direct.	$\begin{vmatrix} -76 & 45 \\ -77 & 01 \end{vmatrix}$	s.e. by E.				aurora still visible.
11	-59 45	99 50	Direct.	$\begin{bmatrix} -77 & 01 \\ -79 & 30 \end{bmatrix}$	s.e. by e. E. ½ N.	K			1
**	-09 40	JJ 00	Needle N.	$-79 \ 13$	$E. \frac{1}{2} N.$				
			Needle S.	-79 29	E. $\frac{1}{2}$ N.			,	
			Needle N.S.		E. $\frac{1}{2}$ N.	>+32	-26	<b>-79 23</b>	A heavy sea, very unsteady.
1			Mag. N.	$-79 \ 45$	$E \cdot \frac{1}{2} N \cdot$				
			Mag. S. Direct.	$\begin{vmatrix} -79 & 43 \\ -79 & 35 \end{vmatrix}$	E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.			·	
13-	-57 46	99 17	Direct.	$-78 \ 30$	E.N.E.	K			
	0, 10	00 - 1	Needle N.	-78 04	E.N.E.	56	96	-77 43	ба.м. The aurora
			Needle S.	<b>-78 00</b>	E.N.E.	7+30	-20	-// 43	seen faintly, very
	-0 -0	101 00	Direct.	-78 20	E.N.E.	IJ			unsteady.
14.	-56 56	101 36	Direct.	-78 04	E. by s.				
			Needle N. Needle S.	-78 21 $-77 33$	е. by s. е. by s.	1 13	26	-78 11	A.M. Aurora visi-
			Needle N.S.		E. by s.	11	~0	70.11	ble, unsteady; squally, with snow.
. [			Direct.	-7758	E. by s.				Squary, with show.
15.	-55 40	103 18	Direct.	-78 30	E.N.E.	Ď			
			Needle N.	-78 53	E.N.E.			<b>-78 09</b>	
ŀ			Needle S. Needle N.S.	$-78 \ 31$	E.N.E.	>+00	-20	<b>-78 09</b>	Unsteady.
			Direct.	$-78 \ 30$	E.N.E.				
16.	-5438	106 15	Direct.	$-79 \ 32$	E.	K	`		
. [			Needle N.	-79 29	<b>E</b> •				
			Needle S.	-78 48	<b>E</b> •	>+25	-26	<b>-79 13</b>	Heavy squalls, un- steady.
			Needle N.S. Direct.	$ \begin{array}{c c} -78 & 55 \\ -79 & 13 \end{array} $	E. E.				
17.	-54 10	108 15	Direct.	-79 13 $-79 17$	E. by s.	$  \langle   \rangle  $			
	-01 10	200 10	Needle N.	$-79 \ 31$	E. by s.				
			Needle S.	-78 38	E. by s.	>+13	-26	-79 19	A strong gale, very unsteady.
			Needle N.S.	- 1	E. by s.	(			unsteady.
	70.00	110 35	Direct.	-79 10	E. by s.	IJ I			
18.	-53 00	110 33	Direct. Needle N.	-78 38   -78 51	N.E.				
			Needle S.	$-78 \ 39$	N.E.				
			Needle N.S.	-78 50	N.E.	> <sub>+80</sub>	-26	<b>-77</b> 39	Unsteady, a heavy
. 1			Mag. N.	<b>-78 25</b>	N.E.	+80	-20	-11 39	swell from the
			Mag. S.	-78 04	N.E.			•	westward, strong breeze.
10	51 00	111 00	Direct.	$ \begin{array}{c c} -78 & 26 \\ -78 & 30 \end{array} $	N.E.	J <sub>+80</sub>	-26	<b>-77</b> 36	Too unsteady to
19. 20.	$-51 00 \\ -48 57$	111 29 112 56	Direct.	-78 30 $-77 14$	N.E. N.E. ½ N.	7	-20	11 00	continue the
. ~ ~ .			Needle N.	-77 25	N.E. $\frac{1}{2}$ N.				observation.
			Needle S.	<b>-77 01</b>	N.E. $\frac{1}{2}$ N.	>+84	-26	-76 04	Very unsteady.
			Needle N.S.	-76 55	N.E. $\frac{1}{2}$ N.	7 7 84	-20	10 01	ory unsucauy.
			Mag. N.	-7651	N.E. $\frac{1}{2}$ N.				
.		•	Mag. S.	$-76 \ 45$	N.E. $\frac{1}{2}$ N.	J	1		;

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. Mar. 22.	-47 <sup>°</sup> 21	115 <b>1</b> 5	Direct.	$-7^{\circ}_{6}$ 42	N.W. $\frac{1}{2}$ N.	<u>,</u>	,	0 /	1
		110 10	Needle N.	$-76 \ 31$	N.W. $\frac{1}{2}$ N.				
			Needle S. Needle N.S.	$\begin{vmatrix} -76 & 11 \\ -76 & 28 \end{vmatrix}$	N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N.	\ >+85	-26	-75 32	Light breeze, table
			Mag. N. Mag. S.	$\begin{vmatrix} -76 & 38 \\ -76 & 29 \end{vmatrix}$	N.W. $\frac{1}{2}$ N. N.W. $\frac{1}{2}$ N.				steady, thick fog.
24.	<b>-45</b> 08	116 50	Direct.	-76 38 $-74 31$	N.W. $\frac{1}{2}$ N. N. by E.	Y			
~4.	-49 00	. 110 30	Needle N.	-74 12	N. by E.	) >+79	-26	-73 27	A heavy sea, ship
			Needle S. Direct.	$\begin{vmatrix} -74 & 02 \\ -74 & 37 \end{vmatrix}$	N. by E.		20		pitching heavily, very unsteady.
25.	-43 22	116 49	Direct. Needle N.	$\begin{vmatrix} -73 & 25 \\ -73 & 10 \end{vmatrix}$	N. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E.				
	,		Needle S.	-7256	$N_{\bullet} = \frac{1}{2} E_{\bullet}$	\\ \>+76	-26	<b>-72 10</b>	A heavy westerly
			Needle N.S. Mag. N.	$\begin{vmatrix} -73 & 18 \\ -72 & 26 \end{vmatrix}$	N. $\frac{1}{2}$ E. N. $\frac{1}{2}$ E.		,		swell, unsteady.
26.	-41 00	116 42	Mag. S. Direct.	$\begin{vmatrix} -72 & 46 \\ -72 & 09 \end{vmatrix}$	N. $\frac{1}{2}$ E. N. by W.	$\exists$			
			Needle N.	-71 50 $-71 55$	n. by w.				
			Needle S. Needle N.S.	-7244	N. by w.	<b> </b> +80	-26	-71 14	A heavy westerly
	,		Mag. N. Mag. S.	$\begin{bmatrix} -72 & 00 \\ -72 & 12 \end{bmatrix}$	n. by w.				swell.
27.	-38 40	116 15	Direct. Direct.	$\begin{vmatrix} -72 & 09 \\ -69 & 08 \end{vmatrix}$	N. by w.	į			
~,.	00 10	110 10	Needle N.	-69 08	n. by E.		- 0	<b>C</b> 2 24	
			Needle S. Needle N.S.	-68 38 $-68 59$	N. by E.	<b>&gt;+81</b>	-26	-68 04	Table steady.
28.	-37 00	116 57	Direct.	$ \begin{array}{r rrrr} -69 & 03 \\ -67 & 24 \end{array} $	n. by E.	}			
	<b>.</b>		Needle N.	-67 37	N. by E.				
			Needle S. Needle N.S.	-67 14	N. by E. $\frac{1}{2}$ E. N. by E. $\frac{1}{2}$ E.	7+00	-26	-66 21	Table steady, cloudy:
	ei		Mag. N. Mag. S.	$\begin{bmatrix} -67 & 08 \\ -67 & 18 \end{bmatrix}$	N. by E. $\frac{1}{2}$ E. N. by E. $\frac{1}{2}$ E.				
29.	-36 11	116 48	Direct. Needle N.	-66 53 $-67 11$	N.N.E.	)			
NO.	,		Needle S.	-66 51	N.N.E.	+84	-26	<b>—66 00</b>	Unsteady.
30.	-35 07	117 28	Needle N.S. Direct.	-66 57 $-66 15$	N.N.E.	1			
			Needle N. Needle S.	-66 25 $-66 50$	N.N.E.	>+84	-26	-65 24	Unsteady.
April 7.	-35 02	117.56	Needle N.S. Direct.	-65 59 $-64 42$	N.N.E.	J			
apin /.	-00 02	117.50	Needle N.	-64 39				* X ;	
<b>10</b>			Needle S. Needle N.S.		}		-26	-64 55	At the tents, King George's Sound.
C C C C C C C C C C C C C C C C C C C			Mag. N. Mag. S.	$\begin{vmatrix} -64 & 18 \\ -64 & 29 \end{vmatrix}$					
11.	-35 02	117 56	Direct.	-65 22	Ĭ				At the tents, King George's Sound. The readings of nee-
			Needle N. Needle S.	$\begin{vmatrix} -65 & 04 \\ -64 & 48 \end{vmatrix}$		1	+18	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	dle A. being very discordant put in needle B., the
	-		Needle N.S. Mag. N.	-65 13 $-65 11$			120		change having been made be-
			Mag. S.	$ -65 \ 15$	J				tween the 7th and 10th of April*.

	-					Corre	ctions.		:
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. Apr. 1 <i>2</i> .	35 <b>0</b> 2	117 56	Direct. Needle N. Needle S. Needle N.S. Mag. N.	-65 21	}		+18	-65 07	At the tents, King George's Sound.*
19.	-35 02	117 56	Mag. S. Direct. Needle N. Needle S. Direct.	$     \begin{array}{r}       -65 & 23 \\       -65 & 15 \\       -64 & 55 \\       -64 & 32 \\       -65 & 15     \end{array} $	s. s. s.	- 21	+18	<b>—65 02</b>	
20.	-35 06	117 55	Direct.	-66 29 $-65 58$	s.e. by e.	$+12 \\ -18$	$^{+18}_{+18}$	$\begin{bmatrix} -65 & 59 \\ -65 & 58 \end{bmatrix}$ 65 59	Unsteady.
23.	-35 30	114 35	Direct. Needle N. Needle S. Needle N.S. Direct.	$   \begin{array}{r}     -66 & 33 \\     -67 & 30 \\     -66 & 30 \\     -66 & 35 \\     -66 & 30   \end{array} $	N.W. N.W. N.W. N.W.	brace + 92		<b>-64</b> 54	Very unsteady.
25.	-32 24	111 26	Direct. Needle N. Needle S. Needle N.S. Mag. N. Mag. S.	$\begin{array}{rrrr} -64 & 03 \\ -64 & 22 \\ -63 & 31 \\ -63 & 58 \\ -64 & 43 \\ -64 & 06 \end{array}$	n.w. by n.	+88	+18	<b>-62 22</b>	Moderate breeze, table steady.
27.	-29 16	106 49	Direct. Direct. Needle N. Needle S. Needle N.S.	-64   13 $-60   10$ $-60   56$ $-60   16$ $-60   30$	N.W. by N. W.N.W. W.N.W. W.N.W.	$\left. \begin{array}{c} 1 \\ +72 \end{array} \right $	+18	<b>—59 30</b>	Very unsteady.
28.	-27 35	106 32	Direct. Direct. Needle N. Needle S. Needle N.S. Mag. N.	-60 53 -58 47 -58 46 -58 51 -58 24 -58 53	w.n.w. w. by n.	$\left.\right\}$ + 61	+18	57 26	A heavy swell, un- steady.
29.	<b>-25</b> 46	104 55	Mag. S. Direct. Direct. Needle N. Needle S. Direct.	_58 53 _58 43 _56 54 _56 54 _56 41 _56 54	w. by n. w. by n. n.w. n.w. n.w.	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right. + 88 \left[ \begin{array}{c} \\ \\ \end{array} \right]$	+18	<b>-55 05</b>	Very unsteady.
May 1.	-23 58	99 06	Direct. Needle N. Needle S.	$ \begin{array}{c cccc} -55 & 48 \\ -55 & 30 \\ -55 & 22 \end{array} $	n.w. n.w. n.w.	+87	+18	-53 46	Unsteady.
2.	-24 01	97 25	Needle N.S. Direct. Needle N. Needle S. Needle N.S.	-55 28 -55 37 -55 58 -55 01 -55 32	N.W. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right\} + 56 \left  \begin{array}{c} \\ \\ \end{array} \right $	+18	54 18	Unsteady.

<sup>\*</sup> Captain Fitzrov having left a memorandum at King George's Sound stating that he had found local magnetic disturbance at King George's Sound, the Inclination was observed on the opposite side of the bay, on the same day as at the tents: needle B gave as follows (no correction being here applied for Index in either case):—

Face west..........  $-65^{\circ}$  13 Face east ........... -65 10

At the tents.

Face west......  $-6\mathring{5}$   $1\acute{6}$  Face east ...... -65 30

On the opposite side of the bay.

Mean..... -65 23

The distance between the two stations was between three and four miles.

Mean..... -65 11.5

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	-9. 1/3	02 -6	D.	-2 oó			,	0 / 0 /	
May 3.	-23 50	95 56	Direct. Needle N. Needle S. Needle N.S.		$     \begin{array}{ccccccccccccccccccccccccccccccccc$	$\left  \begin{array}{c} \\ \\ \\ \end{array} \right  + 56$	+18	-54 26	Unsteady.
4.	-24 17	93 50	Direct. Direct. Needle N. Needle S.	-55 48 -55 43 -56 08 -55 08	W. ½ N. W.N.W. W.N.W.	$\left. iggr)  ight. + 72$	+18	54 07	Unsteady.
5.	<b>-24</b> 02	92 07	Needle N.S. Direct. Direct. Needle N.	-55 33 -55 35 -54 42 -54 39	W.N.W. W.N.W. N.W. N.W.	$\left.\right\rangle_{+88}$	+18	-52 44	Cross sea, with
7.	-21 44	89 38	Needle S. Direct. Needle N.	$     \begin{array}{r}       -54 & 10 \\       -53 & 33 \\       -53 & 47 \\     \end{array} $	N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W.		+18		rolling motion.  Cross sea, with
8.	-20 38	87 50	Needle S. Needle N.S. Direct. Needle N.	$     \begin{array}{r}       -53 & 03 \\       -53 & 19 \\       -52 & 48 \\       -53 & 18     \end{array} $	N.W. $\frac{1}{2}$ W. N.W. $\frac{1}{2}$ W. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.				rolling motion.
9.	-20 37	85 02	Needle S. Needle N.S. Direct. Direct.	$     \begin{array}{rrrr}     -51 & 58 \\     -53 & 00 \\     -52 & 45 \\     -52 & 37     \end{array} $	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.	$\left. \begin{array}{c} +54 \\ \end{array} \right.$	+18	-51 33	Very unsteady.
	,		Needle N. Needle S. Needle N.S. Direct.	-53 16 -52 18 -52 20 -52 20	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	>+55	+18	-51 21	Unsteady.
10.	-20 25	82 00	Direct. Needle N. Needle S.	-52 31 $-52$ 30 $-52$ 48	W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N.				
			Needle N.S. Direct. Mag. N. Mag. S.	-52 26 $-52 31$ $-52 19$ $-52 29$	W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N.	>+68	+18	-51 05	Fresh breeze, table unsteady.
11.	<b>-20</b> 36	79 10	Direct. Needle N. Needle S. Needle N.S.	-53 10 -53 03 -52 41 -53 18	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+68	+18	51 46	Steady.
12.	-20 44	78 31	Direct. Direct. Needle N. Direct.	$ \begin{array}{rrrr} -53 & 17 \\ -52 & 15 \\ -52 & 46 \\ -52 & 42 \end{array} $	W. ½ N. S. S. S.S.W.	Į		-52 00	
			Needle N. Direct. Needle N.	$     \begin{array}{r}       53 & 05 \\       -53 & 10 \\       -52 & 57     \end{array} $	s.s.w. s.w.	$\left. \begin{array}{c} +19 \\ +30 \end{array} \right.$	+18 +18	-52 19 -52 15	
			Direct. Needle N. Direct.	$     \begin{array}{r}       -53 & 11 \\       -53 & 30 \\       -53 & 06     \end{array} $	w.s.w. w.s.w.	$\left. \left. \left. \left. \right  \right. \right\} + 44 \\ \left. \left. \right  \right\} + 51 $	+18 +18	$\begin{vmatrix} -52 & 18 \\ -52 & 11 \end{vmatrix} > -52 & 00$	Light air, table
	<b>.</b>		Needle N. Direct. Needle N.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	W. W.N.W. W.N.W.	$\left. \left. \left. \left. \right   ight.  ight.$	+18	$\begin{bmatrix} -52 & 11 & -52 & 00 \\ -51 & 45 & & & & & \end{bmatrix}$	steady. The observations at N.W., N.N.W., and N. have not been included in
			Direct. Needle N. Direct. Needle N.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	N.W. N.W. N.N.W. N.N.W.	$\left. \begin{array}{c} +86 \\ +68 \end{array} \right.$	+18 +18	-50 44 -50 53	the mean.
	·		Direct. Needle N.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	N.N.W. N.	$\left.  ight\} + 72$	+18	-51 10	

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	0 /	.0. /		. ,				0 / . 0 /	
May 12.	$-20 \ 44$	78 3í	Direct. Needle N.	-5258	N.N.E.	+68	+18	$-51 \ 33$	
			Direct.	-53 04 $-53 18$	N.N.E. N.E.	1			
			Needle N.	$-53 \ 30$	N.E.	+86	+18	$-51 \ 40 > -52 \ 00$	steauv.
			Direct.	-53 15	E.N.E.	$\left \begin{array}{c} 1 \\ +72 \end{array}\right $	+18	_52 02	The observations a N.W., N.N.W. and N. have not
10	00.00	77 49	Needle N.	-53 49	E.N.E.	1 + 12	, 10	02 02	and N. have not been included in
13.	-20 39	. 77 43	Direct. Needle N.	$     \begin{array}{r rrr}     -53 & 15 \\     -53 & 29   \end{array} $	S.E. S.E.	$  \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	+18	$-52 \ 34$	the mean.
			Direct.	-53 25	E.	lf	. 10	50.15	
			Needle N.	$-53 \ 41$	E.	$\left.\right\} + 51$	+18	-52 15	
			Direct.	-53 05	N.E.	$  \} + 86$	+18	-51 42	
			Needle N. Direct.	$     \begin{array}{r rrr}     -53 & 47 \\     -52 & 42     \end{array} $	N.E. N.	}   "			A rolling motion, not very steady a
			Needle N.	$-53 \ 13$	N.	\ -72	+18	-51 28	some points.
			Direct.	-5258	N.W.	1	+18	-51 30	
			Needle N.	-53 30	N.W.	$  \} + 86$	710	_31 30	
			Direct. Needle N.	-53 27	w.	$  \   \ +51$	+18	$[-52 \ 16]$	
16.	-20 26	70 36	Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	w. by N.	К.		,	
		69 00	Needle N.	-53 49	w. by N.		-		
			Needle S.	-53 15	w. by n.	<b>  &gt;+62</b>	+18	-52 19	Unsteady.
			Needle N.S. Direct.		w. by n.				
17.	-20 34	69 24	Direct.	$\begin{bmatrix} -53 & 30 \\ -54 & 05 \end{bmatrix}$	w. by n. w. by n.	Κ.		:	
			Needle N.	-54 10	w. by N.				
			Needle S.	-5352	w. by N.	>+62	+18	-52 447	Very unsteady.
			Needle N.S. Direct.		w. by n.		-		
	-20 34	69 24	Direct.	$\begin{vmatrix} -54 & 10 \\ -54 & 41 \end{vmatrix}$	w. by n. s.w. by w.	K		>-53 01	
			Needle N.	-54 23	s.w. by w.			1	
			Needle S.	-54 00	s.w. by w.				Very unsteady.
			Needle N.S. Mag. N.	1 00 00	s.w. by w.	+37	+18	<b>−53</b> 18 J	very unsteady.
			Mag. S.	$-54  15 \\ -54  09$	s.w. by w. s.w. by w.				
			Direct.	-54 06	s.w. by w.	j			
18.		68 04	Direct.	-54 21	w. by n.	+62	+18	-53 01	Unsteady.
19.	-21 11	67 54	Direct. N.	$-55\ 10$	w. by n.		1		
			S.	$\begin{vmatrix} -56 & 07 \\ -54 & 54 \end{vmatrix}$	w. by n. w. by n.	162	+18	_53 46	Steady.
			N.S.	-55 09			'	100 20	•
		25 00	Mag. N.	-55 10	w. by n.	IJ			
20.	-21 12	67 29	Direct. Needle N.	-55 23	w. by N.				
			Needle S.	$\begin{vmatrix} -55 & 46 \\ -54 & 56 \end{vmatrix}$	w. by n. w. by n.	+62	+18	_53 59	Table unsteady.
			Needle N.S.	-55 11	w. by N.				
		20 70	Direct.	-5519	w. by n.	IJ			
21.	-21 01	66 50	Direct. Needle N.	-55 19	w. by n.				
			Needle S.	-55  35  -54  40	w. by n. w. by n.				
			Needle N.S.	-55 11	w. by N.	+62	+18	-53 49	Unsteady.
			Mag. N.	-5517	w. by n.	11			
			Mag. S. Direct.	-54 40 55 17	w. by N.				
22.	-20 40	62 58	Direct.	$\begin{vmatrix} -55 & 17 \\ -55 & 13 \end{vmatrix}$	w. by n. w. by n.	K			:
~~•			Needle N.	-55 32	w. by N.				
		ľ	Needle S.	-5459	w. by N.	+62	+18	-53 53	Table steady.
			Needle N.S. Needle N.S.		w. by N.				
			Needle N.S.	-55 14 $-55$ 12	w. by n. w. by n.				
			1	""	Sy III.	٢			

						Corre	ctions.	-	
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. May 27.	-20°09	5 <b>%</b> 31	Direct. Needle N.	$-5\overset{\circ}{3} \overset{\circ}{53} \\ -54 \overset{\circ}{27}$		,	•	0 / 0 /	
			Needle S. Needle N.S. Mag. N.	-5329	}	•••••	+18	-53 38	On shore at Mauri- tius.
2.2	07 70		Mag. S.	-5352	IJ.			:	
30.	-21 50	53 25	Direct. Needle N.	$-5550 \\ -5620$	s.w. by w.				·
			Needle S.	-55 05	s.w. by w.	$\rangle + 32$	+18	-54 51	Unsteady.
	-0 -0		Needle N.S.	-55 30	s.w. by w.	IJ.			
June 3.	-26 26	48 20	Direct.	-60 20	N.w. by w.	1 1	* .		
	* 1		Needle N. Needle S.	$-60  ext{ } 40 \\ -59  ext{ } 57$	N.w. by w.	>+80	+18	-58 46	Unsteady.
			Needle N.S.		N.w. by w.				
4.	-27 14	45 50	Direct.	-60 02	n.w. by w.	ľ			
			Needle N.		N.w. by w.	<b> </b> +80	+18	-58 32	Very unsteady.
			Needle S. Needle N.S.	$-59 18 \\ -60 32$	N.w. by w.				
5.	-28 02	42 40	Direct.	$-59 \ 48$	N.w. by w.	フ <sub>+80</sub>	+18	-58 10	Very unsteady.
8.		37 45	Direct.	-60 02	w.	רו		1 1 1 1 1 1 1	
			Needle N.		w.			7	
			Needle S. Needle N.S.	-5951	w. w.	>+50	+18	-59 14	Steady.
			Mag. N.	-60 08	w.				
			Mag. S.	-60 02	w.				
.11.	-30 27	33 41	Direct.	-58 12	w.n.w.	} +72	+18	-56 37	Very unsteady, a
13.	-31 06	31 26	Needle N. Direct.	-58 03 $-58 50$	w.N.w. w. by s. $\frac{1}{2}$ s.	1 1			heavy sea.
10.	0. 00	01 20	Needle N.		w. by s. $\frac{1}{2}$ s.				
			Needle S.	-57 33	w. by s. $\frac{1}{2}$ s.	>+38	+18	-57 24	Very unsteady.
			Mag. N.S.	-60 12	w. by s. $\frac{1}{2}$ s.				
17.	-35 40	21 40	Direct.	-58 55 $-56 56$	w. by s. $\frac{1}{2}$ s. w. by n.	K			
- · · ·	00 10	21 10	Needle N.	-57 00	w. by n.	60	+18	-55 31	
			Mag. N.S.	-56 39	w. by n.	>+02	+10	-55 51	V.
00	Ciman's D	0	Direct.	-56 49	w. by n.	Ŋ			
23.		bay, Cape of pe, for local	Direct. Needle N.	-53 29 $-54 55$	s. s.	+27	+18	-53 45	
		action.	Direct.	$-53 \ 43$	S.E.		110	_53 37	
		-	Needle N.	-5459	S.E.	$\left \right\} + 26$	T 10	-55 5/	
			Direct.	<b>-54</b> 38	E.	) + 51	+18	-53 32	,
			Needle N. Direct.	$-54  44 \\ -54  40$	E. N.E.	IJ			
		1.2	Needle N.	-55 01	N.E.	$  \} + 87$	+18	-53 06 > -53 24	
			Direct.	-54 31	N.	$\frac{1}{2} + 75$	+18	-53 12	
			Needle N.	-54 59	N.	[] [			
			Direct. Needle N.	$-54  45 \\ -54  54$	N.W.	} +88	+18	-53 00	
1			Direct.	-54  46	w.	K	+18	_53 39	
			Needle N.	-54 51	w.	$\left \right\} + 51$	710	-00 08)	
24.		in the Dock-	Direct.	-53 53 -54 94					·
	yaru, III S	imon's Bay.	Needle N. Needle S.	-54 24 $-53 12$	}		+18	-53 37	
			Mag. N.S.	-54 09	J				
L		<u> </u>		L	<u> </u>	<u> </u>		I .	

				·		Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. June 30. July 2.	-33 56	18 29 18 29	Direct. Needle N. Needle S. Mag. N.S. Mag. N. Mag. S. Direct. Needle S. Mag. N.S. Mag. N.S. Mag. N. Mag. S. Direct. Needle N. Needle S. Mag. N.S. Mag. N.S. Mag. N.S. Needle S. Mag. N.S. Mag. N.S. Mag. N.S.		} }		+18	$\begin{bmatrix} -53 & 22 \\ -53 & 27 \\ -53 & 37 \end{bmatrix}$	Observed at the Magnetic Observatory, Cape of Good Hope.

Observations of the Inclination made on board Her Majesty's hired Bark "Pagoda," with Needle 1 (Fox No. 1). Face West. Time usually two hours before Noon.

Observer, Lieut. H. CLERK, Royal Artillery.

						Correc	etions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1844. Nov.10.	tory, Good		Direct. N.	$-5\overset{\circ}{3}  5\overset{\circ}{6} \\ -53  25$	Observed on shore.		+08	-53 31	Needle A. used as de- flector, adjusted at
21.	-33 56	18 29	S. Direct. N. S.	$     \begin{array}{r rrr}     -53 & 37 \\     -53 & 53 \\     -53 & 25 \\     -53 & 37   \end{array} $	Observed on shore.		+08	-53 31	40° from the apparent dip.
Dec.19.	-34 12	18 26	Direct. N. S.		Observed on shore.		+08	-53 50	Observed in the dock-yard at Si- mon's Bay.
Jan. 9.		g out of Bay.	Direct. N. S. Direct.	$ \begin{vmatrix} -54 & 03 \\ -54 & 25 \\ -54 & 48 \end{vmatrix} $	s.e. by s. $\frac{1}{2}$ s. s.e. by s. $\frac{1}{2}$ s. s.e. by s. $\frac{1}{2}$ s. w. $\frac{1}{2}$ s.	$\left. \begin{array}{c} +22 \\ 1 \end{array} \right.$		$\left\{ -53 \ 48 \right\} -53 \ 34$	A strong south-east wind, table very unsteady 2 r.m.
10.	-34 44	17 50	N. S. Direct. N. S.	$     \begin{array}{r}       -53 & 58 \\       -54 & 10 \\       -54 & 18 \\       -53 & 48 \\       \hline       48 & 54 & 08     \end{array} $	$\begin{array}{c} w. \frac{1}{2} s. \\ w. \frac{1}{2} s. \\ w. by n. \\ w. by n. \end{array}$	+51	+08	-53 20 J -52 56	Table very unsteady.  Table unsteady.
13.			Direct. N. S.	$ \begin{vmatrix} -54 & 08 \\ -52 & 33 \\ -52 & 03 \\ -52 & 25 \end{vmatrix} $	s.w. by w. s.w. by w. s.w. by w.	$\left. \begin{array}{c} \\ \\ \end{array} \right\} + 37$	+08	-51 35	Table steady. Up to the 13th of
	-37 25		Direct. N. S. N.S.	$ \begin{array}{r rrrr} -52 & 48 \\ -51 & 54 \\ -52 & 05 \\ -52 & 08 \end{array} $	s.w. by w. s.w. by w. s.w. by w. s.w. by w.	+17	+13	-51 44	January the deflec- tors were at 40° from dip; on and after the 14th they were at the dip, so that the same observa- tions gave dip and
	-38 37		Direct. N. S. N.S.	$ \begin{vmatrix} -54 & 58 \\ -53 & 48 \\ -54 & 03 \\ -53 & 58 \end{vmatrix} $	N.w. by w. N.w. by w. N.w. by w. N.w. by w.	+79	+13	-52 39	intensity. Very unsteady.
16.	-39 10	14 41	Direct. N. S. N.S.		s.w.byw.½w. s.w.byw.½w. s.w.byw.½w. s.w.byw.½w.	7+33	+13	-54 14	Table steady.
17.	-40 21	14 29	Direct. N. S. N.S.	$ \begin{array}{r rrrr} -56 & 18 \\ -55 & 40 \\ -55 & 52 \\ -56 & 00 \end{array} $	s.w. by w. s.w. by w. s.w. by w. s.w. by w.	$\left  \begin{array}{c} \\ \\ \end{array} \right  + 35$	+13	-55 10	Much motion.
18.	42 50	13 00	Direct. N. S. N.S.	$ \begin{vmatrix} -56 & 38 \\ -55 & 40 \\ -55 & 48 \\ -55 & 50 \end{vmatrix} $	s.s.w. s.s.w.	$\left  \begin{array}{c} \\ \\ \end{array} \right  + 12$	+13	-55 34	Much motion.
19	_44 50	13 19	Direct. N. S.	$ \begin{vmatrix} -57 & 18 \\ -56 & 25 \\ -56 & 35 \end{vmatrix} $	s.s.w. s.w. by s. s.w. by s.	+15	+13	_56 14	Much motion.
21	_47 40	12 25	N.S. Direct. N.	$ \begin{array}{r rrrr} -56 & 30 \\ -56 & 43 \\ -56 & 50 \end{array} $	s.w. by s. s. by E. s. by E.	$\left.\right\} + 06$	+11	-56 29	A calm, very unsteady.

						Correc	tions.	1	:
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. Jan. 22.	$-4\mathring{8} \ 3\mathring{5}$	10° 51	Direct.	$-5\r{7}$ 2 $\r{3}$	s.w. by s.	\ \	. ,	0 / 0 /	
Jan. 22.	-45 55	10 01	N.	-57 17	s.w. by s.	>+15	+13	_56 44	Table steady.
			S. N.S.	$\begin{vmatrix} -57 & 03 \\ -57 & 05 \end{vmatrix}$	s.w. by s.		,		Table steady.
23.	-50 30	10 25	Direct.	$     \begin{array}{r rrr}     -57 & 33 \\     -57 & 33     \end{array} $	S.W. $\frac{1}{2}$ S. S.W. $\frac{1}{2}$ S.	וֹ וֹ			
			S.	-5745	s.w. ½ s.	> +15	+13	-57 02	Table steady.
24.	<b>-51</b> 48	9 33	N.S. Direct.	$\begin{bmatrix} -57 & 10 \\ -58 & 13 \end{bmatrix}$	$\begin{array}{c c} s.w. \frac{1}{2} s. \\ s.w. by w. \end{array}$	$  \cdot  $			
			N. S.	-57 55	s.w. by w.	×+25	+13	-57 13	1 г.м. table steady.
		· · · · · · · · · · · · · · · · · · ·	N.S.	$\begin{vmatrix} -57 & 37 \\ -57 & 40 \end{vmatrix}$	s.w. by w. s.w. by w.				
25.	-52 53	7 53	Direct. N.	$\begin{vmatrix} -58 & 13 \\ -57 & 20 \end{vmatrix}$	s.w. by w. s.w. by w.				
			S.	-57 40	s.w. by w.	$\left  \begin{array}{c} +25 \end{array} \right $	+13	-57 03	Table rather un- steady.
26.	-53 52	6 07	N.S. Direct.	-57 30 $-58 23$	s.w by w. w. by s.	K			
			N. S.	$     \begin{array}{r rrr}     -57 & 55 \\     -57 & 40     \end{array} $	w. by s. w. by s.	+46	+13	-57 01	Table very steady.
			N.S.	-58 03	w. by s.	J			
27.	<b>-55</b> 08	5 50	Direct.	$-58 38 \\ -57 28$	S.S.W. $\frac{1}{2}$ W. S.S.W. $\frac{1}{2}$ W.		. 10	" oc	
			S. N.S.	-57 25	s.s.w. $\frac{1}{2}$ w.	>+16	+13	-57 26	Table very un- steady.
30.	-60 43	4 00	Direct.	$\begin{vmatrix} -58 & 10 \\ -61 & 23 \end{vmatrix}$	S.S.W. ½ W.	$\left.\right\}$ -08	+24	-61 067	
			N.S. Direct.	$\begin{vmatrix} -61 & 20 \\ -61 & 03 \end{vmatrix}$	s. s.e. by E.	{			
			N.S.	-60 58	s.E. by E.	$\left  \left. \right  + 22 \right $	+24	-60  14 > -59  58	Table unsteady.
	**:		Direct. N.S.	$\begin{bmatrix} -60 & 08 \\ -60 & 40 \end{bmatrix}$	N. N.	$\left.\right\} + 85$	+24	_58 35 J	
31.	-61 05	9 03	Direct.	$\begin{vmatrix} -61 & 32 \\ -61 & 35 \end{vmatrix}$	s.e. by s.				
			s.	-61 13	s.E. by s.	> 00	+13	-61 01	Table steady.
Feb. 2.	-61 54	16 23	N.S. Direct.	$\begin{vmatrix} -60 & 35 \\ -64 & 18 \end{vmatrix}$	s.e. by s. E.s.e.	Κ Ι			
			N. S.	$\begin{bmatrix} -63 & 30 \\ -63 & 30 \end{bmatrix}$	E.S.E.	+30	+13	-63 00	Table unsteady.
	2		N.S.	-63.33	E.S.E.				-
3.	-61 50	19 13	Direct.	$\begin{vmatrix} -65 & 13 \\ -64 & 18 \end{vmatrix}$	E.S.E.		: 10	Co rr	
			S. N.S.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	E.S.E.	+25	+19	-63 55	Table very steady.
4.	-62 00	20 25	Direct.	-65 33	S.S.E.	Ĭ			
			N. S.	$ \begin{array}{r rrrr} -64 & 43 \\ -64 & 35 \end{array} $	S.S.E. S.S.E.	-15	+13	-64 55	Table very steady.
6	-64 20	24 05	N.S. Direct.	$\begin{vmatrix} -64 & 40 \\ -67 & 03 \end{vmatrix}$	S.S.E.	Ĭ			
0.	-04 20	24 00	N.	-66 13	S.S.E. S.S.E.	_18	+13	_66 37	Table very steady.
			S. N.S.	$\begin{vmatrix} -66 & 20 \\ -66 & 30 \end{vmatrix}$	S.S.E.		1.10		zanie very steady.
7.	-65 34	28 30	Direct.	-6718	S.S.E. ½ E.	Ĭ.			
			N. S.	$\begin{vmatrix} -67 & 00 \\ -66 & 40 \end{vmatrix}$	S.S.E. $\frac{1}{2}$ E. S.S.E. $\frac{1}{2}$ E.	>-16	+13	-66 59	Table very steady.
Q.	-66 30	36 46	N.S. Direct.	$\begin{vmatrix} -66 & 45 \\ -69 & 13 \end{vmatrix}$	S.S.E. $\frac{1}{2}$ E.	1			
	30 00	55 10	N.	-69 10	E.	   > + 40	+13	-68 16	Table very steady.
		•	S. N.S.	$\begin{bmatrix} -69 & 03 \\ -69 & 08 \end{bmatrix}$	E. E.				

						Correc	tions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attrac- tion.	Index.	Corrected Inclination.	Remarks.
1845.	. g . /						· 3	0 / 0 /	
Feb. 10.	-66 $43$	38 49	Direct. N.	$\begin{vmatrix} -69 & 28 \\ -69 & 08 \end{vmatrix}$	S.S.W.				
			S.	-69 03	S.S.W.	<b>  }−26</b>	+13	-69 22	Table very steady.
	_		N.S.	-6858	s.s.w.				
11.	-67 35	39 31	Direct.	-71 28	N.E.	ام . ما	. 10	Co. 40	
			N. S.	$\begin{vmatrix} -71 & 43 \\ -71 & 23 \end{vmatrix}$	N.E.	<b>&gt;+89</b>	+13	-69 49	Table very steady 8 r.m.
12.	-66 45	39 23	Direct.	$-70^{\circ}08$	S.S.E.	K. 1	•	٠.	:
		-	N.	-70 10	S.S.E.	>-30	+13	<b>-70</b> 12	Table very unsteady.
			S.	-6945	S.S.E.		Ţ10	70 12	l and the state of
13.	<b>-67 00</b>	40 07	N.S. Direct.	$\begin{bmatrix} -69 & 35 \\ -70 & 43 \end{bmatrix}$	S.S.E. E.N.E.	K I			
10.	0, 00	10 0,	N.	-71 10	E.N.E.	CC		Co. 00	
			S.	-71 28	E.N.E.	>+66	+13	-69 39	Table steady.
1.0	C 4 × 2	00.05	N.S.	$-70 \ 30$	E.N.E.	J		CC 07 #3	
16.	-6452	38 37	Direct. Direct.	-68 32	N.N.E.	-85	+32	$-66\ 35*$ $68\ 40$	Table very unsteady,
			N.	-68 53 $-68 08$	S. $\frac{3}{4}$ E. S. $\frac{3}{4}$ E.	-26	+13	-68 40	ship pitching much.
			S.	-68 20	S. \(\frac{3}{4}\) E.	J ~ "	, 20		mucn.
17.	-6452	40 12	Direct.	-7008	n. by w.	n. I			
			N.	-7032	n. by w.	>+80	+13	-68 44	Table very unsteady,
			S. N.S.	$\begin{vmatrix} -70 & 25 \\ -70 & 02 \end{vmatrix}$	n. by w.		3		heavy swell.
18.	-6422	40 49	Direct.	$-68 \ 13$	s. by E.	ή I			
			N.	-68 25	s. by E.	>-29	+13	-68 40	Table very unsteady.
7.0	0.0		S.	$-68 \ 35$	s. by E.	7	,	,	
19.	$-63 \ 49$	42 00	Direct.	$-70 \ 33$	E. by s.				
		:	N. S.	$\begin{bmatrix} -70 & 03 \\ -70 & 20 \end{bmatrix}$	E. by s. E. by s.	>+28	+13	-69 36	Table very unsteady
			N.S.	$-70^{\circ}20^{\circ}$	E. by s.				6 р.м.
20.	-63 22	45 35	Direct.		s.e. by E. ½ E.	<b>)</b>			
			S.	-70 25	s.e. by e. ½ e.	>+13	+21	<b>-70 03</b>	Table very unsteady.
21.	-63 36	46 41	N.S. Direct.	$\begin{bmatrix} -70 & 33 \\ -70 & 03 \end{bmatrix}$	s.e. by e. ½ e. s.s.e.	$\prec$ 1			
~1.	-00 00	40 41	N.	-70 03 $-70 18$	S.S.E.			<b>F</b> 0.00	
			S.	$-69 \ 35$	S.S.E.	>-28	+13	-70 02	Table unsteady.
2.1	00		N.S.	$-69\ 10$	S.S.E.	]			
24.	$-62 \ 36$	51 40	Direct. N.S.	$-69  48 \\ -69  40$	Е.	+41	+ 24	<b>−</b> 68 39ე	Taken at 10 A.M.,
			Direct.	-70 28	E. E.	۲ . ا		>69 13	table very un- steady, ship
.			N.	$-70 \ 13$	E.	>+41	+13	$-69 \ 46$	pitching violently. Taken at 5 р.м.
	2		S.	-71 20	Е.	J			
25.	-61 25	53 38	Direct.	-71 28	E.S.E.	)			
			N. S.	$-71 18 \\ -71 00$	E.S.E. E.S.E.	>+12	+13	-7046	Table unsteady.
			N.S.	$-71 00 \\ -70 58$	E.S.E.				
26.	-61 17	57 28	Direct.	$-72 \ 13$	S.E. ½ E.	ή l			
			N.	-7243	S.E. $\frac{1}{2}$ E.	>-11	+13	<b>-72 01</b>	Table unsteady.
			S.	-7148	S.E. ½ E.		20	• • • • • • • • • • • • • • • • • • • •	
27.	<b>-61 00</b>	64 03	N.S. Direct.	$-71 28 \\ -73 28$	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ S.	$\prec$ .1			
~	- 00		N.	$-73 \ 15$	S.E. $\frac{1}{2}$ S.		119	72 07	mahla ay 1
	, 1		S.	-73 38	S.E. $\frac{1}{2}$ S.	>-21	+13	-73 27	Table steady.
00	61 96	70 40	N.S.	-7255	S.E. $\frac{1}{2}$ S.	$\langle \ \  $	,		
28.	$-61 \ 36$	70 46	Direct. N.	$-73  ext{ } 43 \\ -73  ext{ } 55$	S.S.E. S.S.E.				
		. }	S.	$-73 \ 35$ $-73 \ 35$	S.S.E.	>-38	+13	<b>-74</b> 02	Table unsteady, heavy swell.
		1	N.S.	-73 15	S.S.E.	j			
	·!								

<sup>\*</sup> Error, probably in the degree noted; result not included in the mean.

Γ							Correc	tions.		
١	Date.	Lat.	Long.	Method	Observed	Ship's	Ship's		Corrected Inclination.	Remarks.
	Date.	1140.	Long.	employed.	Inclination.	head.	attrac-	Index.	Corrected Incimation.	remarks.
							tion.		:	
	1845.	-62° 10°	72° 25	Dinget	$-7\mathring{4} \ 1\mathring{3}$		<b>\</b> 4	,	0 1 0 1	
l	Mar. I.	-02 10	12 25	Direct. N.	-74 13 $-74 23$	S.S.E. S.S.E.			,	
١	-			S.	-74 20	S.S.E.	>-38	+13	<b>-74</b> 35	Table steady.
١	2,	-62 40	76 09	N.S. Direct.	$-73 \ 43$	S.S.E.	$\forall$			
١	2.	-0z 40	70 09	N.	$\begin{vmatrix} -74 & 28 \\ -74 & 13 \end{vmatrix}$	s. s.	4.0	. 10	<b>7.</b> 50	Table very steady.
				S.	-74 23	s.	-46	+13	<b>-74</b> 50	Table very steady.
ļ	3.	-64 20	79 38	N.S. Direct.	-74 03	s. by w. ½ w.	$\langle \  $			
İ	•/•	-04 20	19 50	N.		s. by w. $\frac{1}{2}$ w.	49	. 10	76 94	Wakla sanataa da
I				S.	-76 27		-43	+13	-76 34	Table unsteady.
l	5	<b>-61 38</b>	84 40	N.S. Direct.	$\begin{bmatrix} -75 & 10 \\ -76 & 13 \end{bmatrix}$	s. by w. $\frac{1}{2}$ w. s.E.	$\forall$			·
l	0.	-01 3	04 10	N.	-76 10	S.E.	00	110	76 07	
1				S.	-7638	S.E.	-23	+13	<b>-76 27</b>	Table unsteady.
I	6.	_60 4g	80 12	N.S. Direct.	$\begin{vmatrix} -76 & 08 \\ -77 & 23 \end{vmatrix}$	S.E. N.E. ½ N.	K			
l	0.	-00 42	00 12	N.	-7708	$N \cdot E \cdot \frac{1}{2} N \cdot$	\ \>+82	+13	<b>-75 43</b>	Table unsteady.
l				S.	-77 23	$N.E. \frac{1}{2} N.$	7+02	+10	-75 45	
١	7.	<b>-61 20</b>	91 09	N.S. Direct.	$\begin{vmatrix} -77 & 18 \\ -76 & 28 \end{vmatrix}$	N.E. $\frac{1}{2}$ N. s. by E.	K		:	
١	•	01 20		N.	-77 20	s. by E.	$\begin{vmatrix} -49 \end{vmatrix}$	+13	-77 237	Table very unsteady,
l				S. N.S.	$\begin{vmatrix} -77 & 18 \\ -76 & 02 \end{vmatrix}$	1		10	77 20	taken at 10 A.M.
1		-61 26	91 20	Direct.	-70 02 $-77 18$	s.w. by s.	K		77 35	Taken at 5 P.M. in consequence of the
١				N.	-77 28	s.w. by s.	$\begin{vmatrix} -35 \end{vmatrix}$	+13	<b>-77 46</b>	h.m. observations being unsatisfac-
۱				S. N.S.	$\begin{bmatrix} -77 & 50 \\ -77 & 00 \end{bmatrix}$			'	'' ''	tory. The aurora was very brilliant all the previous
1	8.	-61 14	92 03	Direct.	-79 03		K			and succeeding
١				N.	$ -79 \ 43$	1	+26	+13	<b>-78 26</b>	Table steady.
١				S. N.S.	$\begin{vmatrix} -79 & 05 \\ -78 & 30 \end{vmatrix}$	1		'	•••	Table steady, light N.W. swell.
ı	9.	-60 3	92 25	Direct.	-78 13	1	K			
l				N.	-78 25		+26	+13	<b>-77 30</b>	Table unsteady.
l				S. N.S.	-78 15 -77 42					
ı	10.	_60 O	95 36	Direct.	-76 27	S.E. $\frac{1}{2}$ S.	Κ			
١				N. S.	$\begin{vmatrix} -77 & 30 \\ -77 & 35 \end{vmatrix}$		$\left  -37 \right $	+13	<b>-77</b> 35	Table very unsteady.
١	- 11.	-595	2 99 30		$\begin{vmatrix} -77 & 35 \\ -80 & 03 \end{vmatrix}$		K			*
۱				N.	-80 23	$E \cdot \frac{1}{2} S \cdot$	+15	+13	-79 217	Table very unsteady,
۱				S. N.S.	-79 25 $-79 23$			'		taken at 10 A.M.
. [		-59 5	99 39		$-80 \ 28$		K		79 36	Table steady, taken at 6 P.M.
				N.	-81 05	E. $\frac{1}{2}$ N.	+30	+13	$-79 \ 51$	
-				S. N.S.	$\begin{vmatrix} -80 & 50 \\ -79 & 53 \end{vmatrix}$					
	13	$-57 \ 3$	5 99 28	Direct.	-79  18	E. by s.	H +11	+14	-78 36	Table very unsteady, taken at 6 P.M.
-				N.S.	-7903		Ţ			
	14	_56 5	3 101 24	Direct.	-78 33 $-79 38$				70.40	
ı				S	-79 22	E. by s.	+12	+13	<b>-78 40</b>	Table very unsteady.
I	1 8	_55 5	2 103 06	N.S. Direct.	-78  48  -79  18		K			
	. 10	-00 5	100 00	N.	-80 28		1 20	1 19	-78 56	Toble versus tos
				S.	-80~03	E. by N.	+39	+13	70.00	Table very unsteady.
				N.S.	<b>-79 23</b>	E. by N.	<u> </u>			

	·					Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.	0 4	8 - 4	D: 1	<b>-</b> ° 20		,	,	0 1 0 1	
Mar. 16.	$-5\mathring{4} \ 4\mathring{8}$	105 04	Direct. N.	$ \begin{array}{c cccc} -79 & 33 \\ -80 & 03 \end{array} $	N.E.				
			S.	-79 25	N.E.	<b>&gt;</b> +78	+13	<b>-78 09</b>	Table very unsteady.
·			N.S.	-79 38	N.E.	J			
17.	-54 17	108 05	Direct.	-78 23	S.E.	$\left.\right\}_{-30}$	. 10	70.160	
			N. S.	$\begin{vmatrix} -79 & 38 \\ -78 & 55 \end{vmatrix}$	S.E.	>-30	+13	$ -79 \ 16$	
			Direct.	$-78 \ 38$	E.	3		>-78 49	Table very unsteady, ship pitching vio-
			N.	-7858	<b>E.</b>	+24	+13	-78 21	lently.
			S.	-7918	Е.	Į			
18.	-53 00	110 08	Direct.	<b>-79 28</b>	N.N.E. $\frac{1}{2}$ E.				
			N. S.	-7855 $-7848$	N.N.E. $\frac{1}{2}$ E. N.N.E. $\frac{1}{2}$ E.	>+82	+13	<b>-77</b> 28	Table very unsteady.
			N.S.	-79 00	N.N.E. $\frac{1}{2}$ E.			•	`
19.	-51 20	111 23	Direct.	-78 08	N.N.E. 1 E.	1 I		*	
			S.	<b>-78 48</b>	N.N.E. $\frac{1}{2}$ E.	>+85	+21	-76 41	Table very unsteady,
00	40.07	111 45	N.S.	-78 25	N.N.E. 1/2 E.	$\forall$		-	heavy swell.
20.	<b>-49 01</b>	111 47	Direct. N.	$\begin{vmatrix} -77 & 38 \\ -78 & 38 \end{vmatrix}$	n.e. by n.				
			s.	-78 30	n.e. by n.	>+82	+13	-76 30	Table unsteady, very heavy swell.
			N.S.	-77 33	n.e. by n.	J			nouty swell.
22.	-47 21	115 15	Direct.	<b>-76 43</b>	E.N.E.	ן ו	-		
		1	N.	-77 13	E.N.E.	>+58	+13	$-75 \ 31$	Table steady, light
			S. N.S.	$\begin{vmatrix} -77 & 03 \\ -75 & 48 \end{vmatrix}$	E.N.E.		•		swell.
95	-43 20	116 52	Direct.	-73   48 $-73   23$	E.N.E. N. ½ E.	Υ .			
~0.	-10 ~0	110 0%	N.	$-75 \ 45$	N. $\frac{1}{3}$ E.		. 10	#O 4F	
	. [		S.	-74 48	$N \cdot \frac{\overline{1}}{2} E \cdot$	>+76	+15	-72 45	Table very unsteady, heavy swell from W.
			N.S.	-7258	$N \cdot \frac{1}{2} E \cdot$	J			· ·
26.	<b>-41</b> 18	116 09	Direct.	-71 33	N. by w.				
	1		N. S.	$\begin{vmatrix} -71 & 33 \\ -72 & 15 \end{vmatrix}$	N. by w. N. by w.	>+80	+13	<b>-70</b> 11	Table unsteady,light swell.
	1		N.S.	$-71 \ 33$	N. by w.				swell.
27.	-38.52	116 15	Direct.	-70 23	n. by w.	ή l			
	.		N.	$-70 \ 45$	N. by w.	>+80	+13	-68 49	Table steady.
	1		S. N.S.	-70 50	N. by w.		•		,
28.	-37 03	116 57	Direct.	$     \begin{array}{r rrr}     -69 & 28 \\     -68 & 33     \end{array} $	n. by w. n. by e.	$\forall$ 1			
20.	-0, 00	110 07	N.	-6848	N. by E.		+13	-66 46	m 11
	1		S.	-68 13	n. by E.	>+83	+10	-00 40	Table very steady, nearly calm.
	-0		N.S.	-67 53	n. by E.	7			
29.	-36 12	-116 50	Direct.	$\begin{bmatrix} -67 & 30 \\ 67 & 12 \end{bmatrix}$	N.N.E.				
1			N. S.	-67 13 $-66 55$	N.N.E. N.N.E.	>+84	+13	-65 28	Table unsteady.
			N.S.	$-66 \ 43$	N.N.E.		ļ		
30.	-35 18	117 07	Direct.	-67 28	N.E. 1/2 E.	<b>i</b>			
		_	N.	-6800	N.E. $\frac{1}{2}$ E.	×+86	+13	-65 48	Table unsteady.
	1		S. N.S.	$\begin{vmatrix} -67 & 48 \\ -66 & 30 \end{vmatrix}$	N.E. $\frac{1}{2}$ E.				
April 7.	-35 02	117 56	Direct.	-65 28	N.E. ½ E.	,		11.	4
I	King G		N.	$-65 \ 36$	Observed	1	112	-65 117	
	Sou		S.	$-65 \ 30$	on shore.	} ·····	+13	-05 11	
	<i>v</i> · ~	,	N.S.	-65 03	٦	, .		>-65 11	The observations
11.	King G Sou	eorge's	Direct.	-65 28 $-65 28$	Observed				were made at the same place that was
	ວບນ	nu.	N. S.	$-65 \ 31$	on shore.	ا	+13	-65 11	used by Captains FLINDERS and
			N.S.	-65 09	J		1 5 •5		FITZROY.

						Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845. April <b>19</b> .	At anch	or in the	Direct. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	s.s.w. s.s.w.	} _16	+24	_64 46 <u>]</u>	
			Direct. N.S.	$ \begin{array}{r rrrr} -65 & 49 \\ -65 & 25 \end{array} $	s.w. s.w.	+01	+24	-65 12	
			Direct. N.S.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	w.s.w. w.s.w.	$\left.\right\} + 23$	+24	-64 57	
		ion.	Direct. N.S. Direct.	$   \begin{array}{r}     -66 & 02 \\     -65 & 39 \\     -66 & 23   \end{array} $	W. W. W.N.W.	+46		-64 41	
		ttract	N.S. Direct.	$-66 \ 03$ $-66 \ 35$	W.N.W. N.W.	$\left.\right\} + 70$	+24	-64 39	
		To obtain corrections for the ship's attraction.	N.S. Direct.	-66 16 $-66 50$	N.W. N.N.W.		$+24 \\ +24$	-64 30 $-64 52$	
		the sh	N.S. Direct. N.S.	-66 29 $-66$ 29 $-66$ 14	N.N.W. N.	$\begin{cases} +84 \\ +84 \end{cases}$	+24	-64 34	
		ls for	Direct. N.S.	-66 48 $-66$ 26	N. N.N.E. N.N.E.	$\left.\right\} + 83$	+24	-64 50 $-64 51$	The table was very steady during these observations.
		ection	Direct. N.S.	$-66  ext{ } 35 \\ -66  ext{ } 09$	N.E.	$\left.\right\} + 92$	+24	-64 26	:
		1 corr	Direct. N.S.	$ \begin{array}{rrr} -66 & 27 \\ -66 & 00 \\ -66 & 37 \end{array} $	E.N.E. E.N.E.	+70	+24	<b>-64 40</b>	
		obtai	Direct. N.S. Direct.	-66 21 $-66 16$	E. E. E.S.E.	} +46	+24	<b>-65</b> 19	ů.
		$\Gamma_0$	N.S. Direct.	-65 40 $-65 52$	E.S.E. S.E.	$\left.\begin{array}{c} +23 \\ +01 \end{array}\right $	$+24 \\ +24$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	-		N.S. Direct.	-65 19 $-65 13$	S.E. S.S.E.	$\begin{cases} -16 \end{cases}$	+24	-64 58	
			N.S. Direct. N.S.	-64 58 $-65$ 11 $-64$ 46	S.S.E. S. S.	$\left. \begin{array}{c} -21 \end{array} \right $	+24	-64 57	
23.	<b>—35</b> 36	114 44	Direct.	-6653 $-6745$	N.W.	$\left.\begin{array}{c} \\ \\ \\ \end{array}\right. + 92$	+13	<b>-65 28</b>	Table unsteady.
24	04.10	110.01	S. N.S.	$-67  ext{ } 40$ $-66  ext{ } 33$	N.W.	\[ \frac{\pi \ 3\z}{\pi} \]	7.10	-0 <b>0</b> 20	Table unsteady.
24.	<b>-34</b> 16	113 01	Direct. N. S.	$-66   33 \\ -66   28 \\ -66   25$	n.w. by n. n.w. by n. n.w. by n.	+88	+13	-64 44	Table unsteady.
25.	<b>—32 32</b>	111 36	N.S. Direct.	$-66 \ 15$ $-63 \ 48$	n.w. by n.	$\left\{ \ \ \right $			
			N. S.	-64 25 $-63 55$	n.w. by n.	+88	+13	<b>-62 14</b>	Table unsteady.
27.	-29 20	106 55	N.S. Direct. N.	$     \begin{array}{rrr}     -63 & 33 \\     -60 & 58 \\     -61 & 05     \end{array} $	N.W. by N. W.N.W.		,		
			S. N.S.	$ \begin{array}{c cccc} -60 & 20 \\ -60 & 33 \end{array} $	W.N.W. W.N.W.	\rightarrow +72	+13	<b>-59 19</b>	Table steady.
28.	-27 47	106 36	Direct. N.	$-58 28 \\ -58 10$	ท. by พ. ½ พ. ท. by พ. ½ พ.	+76	+13	<b>-57</b> 17	Table very unsteady,
90	<b>-26 00</b>	105 11	S. N.S. Direct.	$ \begin{array}{c cccc} -58 & 25 \\ -60 & 00 \\ -56 & 38 \end{array} $	N. by w. ½ w. N. by w. ½ w. N.w.	$\left\{ \right.$			heavy swell.
29.	-20 00	100 11	N. S.	-56 48 $-57$ 08	N.W. N.W.	+88	+13	-55 09	Table very unsteady, very heavy swell.
			N.S.	-56 45	N.W.	J			org month

224 01 97 30 Direct55 03 w. h55 20 w. h							Correc	ctions.	5 ;	
1845	_		<b>.</b>	Method	Observed	G1. 1 1	01:1		0	
May 124 00 99 23   Direct.	Date.	Lat.	Long.			Ship's head.	attrac-	Index.	Corrected Inclination.	Remarks.
May 124 00 99 23   Direct.	1845.							,		
224 01 97 30   S.   -56 13   w.   N.S.   -55 4 43   w.   -55 20   w.   N.S.   -55 28   w.   N.S.   -55 30   w.   N.S.   -55 4 28   N.W.   N.S.   -54 48   N.W.   N.S.   -52 44   N.W.   N.S.   -52 44   N.W.   N.S.   -52 44   N.W.   N.S.   -52 44   N.W.   N.S.   -52 30   N.W.   by w.   N.S.   -52 30   N.W.	May 1.	-24 00	99 23		-5518	w.	h 'l	,		
224 01 97 30   N.S.   -55 43   w.   N.S.   -55 28   w.   N.S.   -55 28   w.   N.S.   -55 13   w.   N.S.   -55 13   w.   N.S.   -55 13   w.   N.S.   -55 38   w.   N.S.   -54 48   N.W.   N.S.   -52 28   N.W.   by W.   N.S.   -52 38   W.   2 N.   N.S.   -52 38   W.   2 N.   N.S.   -52 38   W.   2 N.   N.S.   -52 28   N.W.   by W.   N.S.   -52 38   W.   2 N.   N.S.   -52 38   W.   2 N.   N.S.   -52 38   W.   2 N.   N.S.   -52 28   W.   2 N.   N.S.   -52 38   W.   2 N.   N.S.   -52 40   W.		1				w.	51	<b>±13</b>	54 99	
224 01 97 30 Direct55 03 w. S55 28 w. S55 30 w. S. S54 28 N. W. S. S54 13 N. W. S. S52 30 N. W. S. N.		1		S.		w.	( + 31	710		considerable mo-
N.   -55 20   W.   S.   -55 20   W.   S.   -55 28   W.   W.   M.   S.   -55 28   W.   W.   M.   M.   S.   -55 38   W.   M.   M.   M.   M.   M.   M.   M.	Į					1	IJ			tion.
S.	2.	-24 01	97 30			1				
324 00 96 06   N.S.   -54 35   N.W.   N.S.   -55 36 N.W.   N.S.   -55 36 N.W.   N.S.   -55 38 N.W.   N.S.   -55 38 N.W.   N.S.   -54 48 N.W.   N.S.   -52 58 N.W.   N.S.   -52 58 N.W.   N.S.   -52 58 N.W.   N.S.   -52 13 N.W.   Direct.   -52 23 N.W.   Direct.   -52 24 N.W.   Direct.	1		,			ľ	>+51	+13	-54 03 T	Cable steady.
324 00 96 06 Direct55 18   N. \frac{1}{N} \ N. \ S55 30   N. \frac{1}{N} \ N. S54 28   N. N. \ N. S54 40   N. W. \ N. S54 40   N. W. \ N. S54 48   N. W. \ N. S54 88   N. W. \ N. S54 88   N. W. \ N. S54 89   N. W. \ N. S54 80   N. W. \ N. S52 13   N. W. \ N. S52 13   N. W. \ N. S52 13   N. W. \ N. S52 30   N. W. \ N. S52 35   N. W. \ N. S52 36   N. W. \ N. S52 37   N. W. \ N. S52 40   N. W. \ N. S53 30   N.	1					1				
N.   -55   13   W.     N.   N.   N.   N.   N.   N.	3	_24 00	96 06			!	K			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.	-24 00	30 00		1					
N.S.   -55   38   N.W.   N.W	1				1 .		\ \rangle + 56	+13	-54 16	l'able steady.
N.   -54 40   N.w.	1		1		-55 38					
S.	6.	-2247	91 00		-54 28	N.W.	ń I			
721 50 89 44 Direct53 28 N.w. N. N. S54 18 N.w. N. S54 08 N.w. N. S54 08 N.w. N. S54 18 N.w. N. S54 08 N.w. N. S54 08 N.w. by w. N. S52 28 N.w. by w. N. S52 13 N.w. by w. N. S52 15 N.w. by w. N. S. N.					-	i	1 487	+13	-52 49	Cable very unsteady.
721 50 89 44 Direct.			2		1	1	1	1,20	1 00 10	heavy swell from W.
8. $-20$ 46 87 59 $\begin{bmatrix} N. & -53 & 53 & N.w. \\ S. & -54 & 08 & N.w. \\ N.S. & -54 & 13 & N.w. \\ N.S. & -52 & 28 & N.w. by w. \\ N.S. & -52 & 58 & N.w. by w. \\ N.S. & -52 & 58 & N.w. by w. \\ N.S. & -52 & 33 & N.w. by w. \\ N. & -52 & 33 & N.w. by w. \\ N. & -52 & 33 & N.w. by w. \\ N. & -52 & 33 & N.w. by w. \\ N. & -52 & 33 & N.w. by w. \\ N. & -52 & 33 & N.w. by w. \\ N. & -52 & 35 & N.w. by w. \\ N. & -52 & 45 & N.w. by w. \\ N.$		21.50	00.44			ľ	IJ.			
S.	7.	-21 50	89 44			1				
820 46 87 59   N.S.   -54 13   N.W.   -52 28   N.W. by W.   N.   -53 03   N.W. by W.   N.   -52 13   N.W. by W.   N.   -52 33   N.W. by W.   N.   N.   -52 35   N.W. by W.   N.   N.   N.   -52 35   N.   N.   N.   N.   N.   N.   N.   N						í	> +86	+13	$ -52 \ 17$	Table very unsteady,
820 46 87 59   Direct.   -52 28   N.w. by w.   N.   -53 03   N.w. by w.   N.S.   -52 13   N.w. by w.   N.S.   -52 13   N.w. by w.   N.S.   -52 33   N.w. by w.   N.S.   -52 33   N.w. by w.   N.S.   -52 35   N.W. by w.   N.S.   -52 40   N.S.   -52 40   N.   N.S.   -52 40   N.S.   N.S.   -53 35						(				neavy w. swell.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8.	-20 46	87 59			P.	K			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		70						. 10	F1 0C	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							>+82	+13	-51 00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				N.S.	-52 13		-		50 57	n 11
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							ň i		1 1 . 1	server Mr. Bur-
9. $-20$ 38 85 26 $\begin{vmatrix} N.S. & -52 & 15 & N.W. & by W. \\ Direct. & -52 & 15 & N.W. & by W. \\ -52 & 35 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 35 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 38 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 38 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 38 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 38 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 38 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 33 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 33 & W. & \frac{1}{2} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -52 & 49 & W. & \frac{1}{4} & N. \\ N.S. & -53 & 30 & W. & \frac$							1 482	+13	1 50 49 1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							1	1 20		l'able steady.
10. $-20\ 26$ 82 22  N. S. $-52\ 35$ N.S. $-52\ 38$ N.S. $-52\ 38$ N.S. $-52\ 38$ N.S. $-52\ 38$ N.S. $-52\ 58$ N.S. $-52\ 49$ N.S. $-53\ 30$ N.W. $-50\ 30$ N.S. $-50\ 30$		20 20	05.06				IJ			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.	-20 38	85 20			1 =				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	'		4				$  \rangle + 56$	+13		Fable very unsteady
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						1 7				heavy swell.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.	-20 26	82 22			, =	K			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				N.			1 56	. 19	51 400	Pahla ware urataade
Direct. $-52$ 49 $-52$ 47 $-52$ 47 $-51$ 39 $-5$				s.	-5258	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	> + 30	+13	-51 40	ane very unsteauy
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					1	W. $\frac{1}{2}$ N.	IJ	1	_51 30	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						1 2	n		( 01 03	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-					( ±	+53	+13	-51 37	Fable very unsteady.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						1 2		•	1 - 1	
$ \begin{vmatrix} N. & -52 & 45 & W. \frac{1}{4} & N. \\ S. & -53 & 05 & W. \frac{1}{4} & N. \\ N.S. & -53 & 30 & W. \frac{1}{4} & N. \\ N.S. & -52 & 38 & W. \frac{1}{4} & N. \\ N. & -52 & 40 & W. \frac{1}{4} & N. \\ S. & -53 & 08 & W. \frac{1}{4} & N. \\ N.S. & -52 & 53 & W. \frac{1}{4} & N. \\ N.S. & -52 & 53 & W. \frac{1}{4} & N. \\ N.S. & -53 & 55 & W. \\ Direct. & N.S. & -53 & 23 & W.N.W. \\ N.S. & -53 & 23 & W.N.W. \\ N.S. & -53 & 30 & N.W. \\ N.S. & -53 & 23 & N.W. \\ N.S. & -53 & 24 & N.W. \\ N.S. & -53 & 25 & N.N.W. \\ N.S. & -53 & N.M.W. \\ N.S. & -53 & N.M.$	11	_ ou sc	70 00		1	1 2	K			4.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.	20 50	.5 ~~							* * * * * * * * * * * * * * * * * * * *
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			8			, <u>"</u>	$ \rangle$ + 53	+13	-51 55	Fable very unsteady. Observer Mr. Bur-
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						1 7				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					-52 38	1 1	K			**************************************
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			*			$W. \frac{1}{4} N.$	1 4 53	+13	-51 44	Fable unsteady.
$ \begin{vmatrix} 12. & -20 & 44 \end{vmatrix} \begin{vmatrix} 78 & 31 \end{vmatrix} \begin{vmatrix} \text{Direct.} & -54 & 08 & & & & & & \\ N.S. & -53 & 55 & & & & & \\ Direct. & N.S. & -53 & 23 & & & & \\ N.S. & -53 & 23 & & & & & \\ N.S. & -53 & 30 & & & & \\ N.S. & -52 & 53 & & & & \\ N.W. & N.W. & & & \\ N.W. & N.W. & & \\ N.W. & N.W. & & \\ N.W. & N.W. & & \\ -68 & +24 & -51 & 20 \end{vmatrix} $	·					1 ₹	1	10		
$\left\{\begin{array}{c ccccccccccccccccccccccccccccccccccc$		20	#O 07		)	_	Ŋ			
$\left\{\begin{array}{c ccccccccccccccccccccccccccccccccccc$	12.	-20 44	78 31			1	$\left  \right  + 51$	+24	-52 47	
$\left\{\begin{array}{c ccccc} N.S. & -53 & 23 & W.N.W. \\ Direct. & -53 & 23 & N.W. \\ N.S. & -53 & 30 & N.W. \\ Direct. & -52 & 53 & N.N.W. \\ \end{array}\right\} + 86 + 24 \begin{vmatrix} -51 & 35 \\ +24 & -51 & 37 \\ +68 & +24 & -51 & 20 \\ \end{array}$								l		
$\left \begin{array}{c ccccc} \text{Direct.} & -53 & 23 & \text{N.w.} \\ \text{N.S.} & -53 & 30 & \text{N.w.} \\ \text{Direct.} & -52 & 53 & \text{N.w.} \\ \text{N.N.w.} & \\ \end{array}\right _{N.N.W.} + 86 + 24 -51 & 37 -10 = 10$						1	$  \} + 72$	+24	-51 55	
$\left\{\begin{array}{c c} \text{N.S.} & -53 \cdot 30 & \text{N.W.} \\ \text{Direct.} & -52 \cdot 53 & \text{N.N.W.} \end{array}\right\} + 80 + 24 - 51 \cdot 20$						ì	1		5, 07	
Direct. $-52\ 53$ N.N.W. $\begin{bmatrix} +68 \\ +24 \\ -51\ 20 \end{bmatrix}$							1 + 86	+24	-51 37	
1 + 08 + 24 - 01 = 0						1	1	104	51 00	
				N.S.	-5250	N.N.W.	1 + 08	1	1 1 1	*
Direct. $\begin{vmatrix} -52 & 43 \end{vmatrix}$ N. $\begin{vmatrix} 7 & +70 \end{vmatrix} + 32 \begin{vmatrix} -51 & 01 \\ -52 & 03 \end{vmatrix}$				Direct.	$ -52 \ 43$	N.	+70	+32	$ -51 \ 01 \ \rangle -52 \ 03$	

	-					Correc	ctions.		
	. 1		Method	Observed					
Date.	Lat.	Long.	employed.	Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1845.									
May 12.	-20 44	78 31	Direct.	$-53^{\circ}48^{'}$	N.N.E.	7 60	104	0 / 0 /	_
		•	N.S.	-53 03	N.N.E.	+68	+24	-51 54 > -52 03	
		*	Direct.	-5248	s.	$\}+15$	+24	-52 01	
	1		N.S.	-52 33	s.	1 10	, 72	- 0% U1	
			Direct. N.S.	-5348	s.s.w.	} +19	+24	-52 46	ra in the
			Direct.	$\begin{bmatrix} -53 & 10 \\ -53 & 43 \end{bmatrix}$	s.s.w.	3			
			N.S.	-53   03	S.W.	} +30	+24	-52 29	
			Direct.	-5348	w.s.w.	1	+24	FO 95	To obtain correc-
			N.S.	$-53 \ 38$	w.s.w.	+44	+24	$[-52 \ 35]$	tions for the
13.	-20 39	77 43	Direct.	-53 48	w.	$\frac{1}{2} + 51$	+24	-52 42)	tion. Calm,table very unsteady,
			N.S.	-54 05	w.	1		, <u>-,</u> ,	considerable rolling motion.
			Direct. N.S.	$-53 28 \\ -53 13$	N.W.	<b>\}</b> +86	+24	-51 30	, and the state of
			Direct.	-52 58	N.W.	,			
			N.S.	-52  45	N.	+70	+24	-51 18	
			Direct.	-53 23	N.E.	$\frac{1}{5} + 86$	+24	$\begin{vmatrix} -51 & 24 \end{vmatrix} -51 & 59$	,
			N.S.	-53 05	N.E.	[ ]	1 ~ 1	-01 XI	
	1		Direct.	-53 53	Е.	$\left  \right  + 51$	+24	-52 27	
			N.S. Direct.	-53 30 $-53 48$	E. S.E.	Ĭ			,
			N.S.	-53   08	S.E.	} +30	+24	$[-52 \ 34]$	
14.	-20 29	76 22	Direct.	-53 08	$W \cdot \frac{1}{2} N \cdot$	К 1			
			N.	-53 00	$W \cdot \frac{1}{2} N \cdot$	>+56	+13	-52 137	Table very unsteady.
			S.	$-53 \ 35$	$W \cdot \frac{1}{2} N \cdot$	7+00	710	-02 10	able very unsteady.
			N.S.	-53 43	W. 1 N.	IJ.		>-52 20	
			Direct. N.	$-53  38 \\ -53  48$	W. $\frac{1}{2}$ N. W. $\frac{1}{2}$ N.				
			S.	-53 50	$W \cdot \frac{1}{2} N \cdot$	$\rangle + 56$	+13	-52 27	Table very unsteady. Observer Mr.
			N.S.	-53 08	$W \cdot \frac{1}{2} N \cdot$				Burdon, R.N.
16.	-20 28	70 46	Direct.	-54 08	$w. \frac{1}{4} N.$	ñ			
	:		N.	-53 48	$W \cdot \frac{1}{4} N \cdot$	+53	+13	-52 51	Table steady.
			S. N.S.	-53 53	W. 1 N.		·		Table steady.
19	-21 06	68 12	Direct.	_53 58 _54 43	$W. \frac{1}{4} N. W.s.W.$	K			
10.	-21 00	00 12	N.	$-53 \ 45$	w.s.w.	11		<b>T</b> 0 -0	
			S.	-54 05	w.s.w.	+44	+13	-53 10	Table very unsteady.
			N.S.	-53 53	w.s.w.	IJ			
19.	-21 11	67 54	Direct.	-54 28	n.w. by n.	)			
			N. S.	-54 35	n.w. by n.	>+77	+13	-52 547	Table steady, nearly
			N.S.	-54 23 $-54 08$	n.w. by n. n.w. by n.	[			calm.
			Direct.	-54   53	n.w. by n.	K		<b>}−53 02</b>	2 P.M.
			N.	-54 45	n.w. by n.	+77	112	59 10	
			S.	-54 38	n.w. by n.	>+11	+13	-53 10	Table steady. Ob- server Mr. Bur-
		C= 00	N.S.	-54 23	n.w. by n.	IJ			don, R.N.
20.	-21 12	67 29	Direct. N.	-55 03 $-54 58$	w. by N.				
1			S.	-55 08	w. by n. w. by n.	>+63	+13	$-53 \ 46$	Table steady.
1			N.S.	-54 58	w. by n.			70.00	
		**	Direct.	-54 58	w. by n.	Ĭ		<b>}−53 39</b>	
			N.	-54  45	w. by n.	$\rightarrow +63$	+13	-53 32	Table steady. Ob-
			S. N.S.	-55 00 $-54 28$	w. by N.			7.	server Mr. Bur- bon, R.N.
			11.00	-01 20	w. by n.	<u>ا</u>			

						Correc	tions.		
	<b>.</b> .		Method	Observed	Chimia haad	Chinia		Commented I I all all all	70. 1
Date.	Lat.	Long.	employed.	Inclination.	Ship's head.	Ship's attrac-	Index.	Corrected Inclination.	Remarks.
						tion.			
1045				<del></del>					
1845. May 21.	-21 02	66° 02′	Direct.	$-5\overset{\circ}{5}\ 2\overset{\prime}{8}$	w. by N.	h 1	1	0 /	
1.1uj ~1.	102 070	00 00	N.	-55 13	w. by n.	>+63	. 19	F4 09	m 11 1
	- ,		<b>S.</b>	-55 23	w. by n.	7+03	+13	-54 03	Table steady.
	20.01	<b>20.10</b>	N.S.	-55 13	w. by n.	Ŋ I		1	
23.	$-20 \ 31$	59 42	Direct. N.	$\begin{bmatrix} -55 & 28 \\ -55 & 00 \end{bmatrix}$	w. by n. w. by n.				
			S.	-55 23	w. by N.	>+63	+13	-53 59	Table very unsteady.
			N.S.	-55 07	w. by N.		·	:	
27.	<b>-20 0</b> 9	57 31	Direct.	-54 27	n "				
	Port	Louis,	N.	-54 22	Observed		+13	-54 14	Observed by Lieut.
		ritius.	S.	-54 59	on shore.	)	,		Moore, R.N.
20	-21 44		N.S. Direct.	$\begin{bmatrix} -54 & 01 \\ -55 & 33 \end{bmatrix}$	∪ w.s.w.*½ w.	h			·
30.	-21 11	00 04	N.	-55 20	w.s.w. ½ w.				
			S.	-55 28	$w.s.w. \frac{1}{2} w.$	\ \rac{+38}{}	+13	-54 38	Table very unsteady, heavy swell.
			N.S.	-55 35	w.s.w. $\frac{1}{2}$ w.	IJ			
June 2.	-26 25	49 12	Direct.	-60 33	N.w. by w.	n .			
			N. S.	-59 50	N.w. by w.	>+80	+13	-58 36	Table very unsteady,
			N.S.	$\begin{bmatrix} -60 & 05 \\ -60 & 10 \end{bmatrix}$	N.w. by w.	11			heavy swell.
4.	-27 12	46 09	Direct.	-59  48	w. by s.	K			
			N.	-5918	w. by s.	+46	+13	-58 44	Table unsteady,
			S.	-5948	w. by s.	1 7 + 40	+10	-30 44	fresh breeze.
] _	:00.04	40.00	N.S.	-5958	w. by s.	K			
5.	-28 24	43 00	Direct. N.	$\begin{bmatrix} -59 & 43 \\ -59 & 53 \end{bmatrix}$	w.				
			S.	$-60 \ 18$	w.	>+51	+13	-58 52	Table very unsteady, fresh breeze.
İ			N.S.	-59 48	w.				fresh breeze.
6.	-28 44	42 01	Direct.	-60 33	w.n.w.	Ĭ			
1			N.	-60 25	W.N.W.	+72	+13	_59 01	Table very unsteady,
			S. N.S.	$\begin{bmatrix} -60 & 23 \\ -60 & 23 \end{bmatrix}$	W.N.W.				fresh breeze,
7.	-28 35	40 24	Direct.	-59 58	W.N.W. W. $\frac{1}{2}$ N.	K			
١ "	70 00	10 21	N.	-59 56	$W \cdot \frac{1}{2} N$	1	. 10	FO F4	m-11
			s.	-60 28	$W \cdot \frac{1}{2} N$ .	+56	+13	-58 54	Table very unsteady.
			N.S.	-5950	$W \cdot \frac{1}{2} N \cdot$	Ų			
8.	-28 57	37 52	Direct. N.	-60 38 $-59 45$	w.	[]			
1	}		S.	-60 25	w. w.	>+51	+13	-59 08	Table steady, nearly a calm.
			N.S.	-60 02	w.				
12.	-30 33	33 19	Direct.	-59 03	w.n.w.	1			
	1		N.	-58 30	w.n.w.	+72	+13	-57 19	Table unsteady.
	1		S.	-58 43	W.N.W.	1	'		and uniteday.
13.	_31 06	31 34	N.S. Direct.	-58 38 $-58 33$	w.n.w.   w. by s. $\frac{1}{2}$ s	K			
13	-01 00	51 54	N.	-58 20	w. by s. $\frac{1}{2}$ s	1.1			Table steady, nearly
1			S.	-58 35	w. by s. $\frac{1}{2}$ s		+13	-57 28	a calm.
1			N.S.	-58 05					
14.	-33 01	29 36	Direct.	-58 38	w.	n			
			N. S.	-58 25 $-59 08$	W.	>+51	+13	-57 34	Table unsteady,
1			N.S.	-58 20	w. w.				fresh breeze.
15	. 34 31	27 04	Direct.	-58 23		K			
1			N.	<b>-58 08</b>	$W \cdot \frac{1}{2} N \cdot$	+56	+13	-57 06	Table very unsteady,
1	1		S.	-58 45		1	'		long heavy swell.
}			N.S.	-5745	$W.\frac{1}{2}N.$	IJ			

	- •					Correc	tions.		
			Method	Observed		Correc	tions.		
Date.	Lat.	Long.		Inclination.	Ship's head.	Ship's attrac- tion.	Index.	Corrected Inclination.	Remarks.
1835.	0 /			0 /		,	٠,	0 / 0 /	
June 16.	$-35 \ 46$	23 35	Direct.	-5738	w. by n.	)	-		
			N.	-57 23	w. by n.	>+63	+13	-56 08	Table steady, fresh
			S. N.S.	$-57 15 \\ -57 20$	w. by n. w. by n.				breeze.
17.	-35 36	21 40	Direct.	-5648	w. by n.	3			
	00 00	71 10	N.	-56 43	w. by n.		. 10	FF 10	
	,		S.	-56 40	w. by n.	\rangle +72	+13	-55 18	Table steady.
			N.S.	-56 40	w. by n.	]			
18.	-35 07	20 46	Direct.	-5618	w. by s.	)			
			N.	-55 45	w. by s.	>+46	+13	+5508	Table steady.
			S. N.S.	-56 08 $-56 18$	w. by s.		·		
23.	-34 12	18 26	Direct.	-54 17	w. by s.	K .			
20.	-01 12	10 20	N.S.	$-53 \ 45$	on shore.	}	+24	$\begin{bmatrix} -53 & 37 & -53 & 37 \end{bmatrix}$	Observed in the dockyard at
30.	-33 56	18 29	Direct.	-54 12	K	ر			Simon's Bay.
l			N.	-53 13	Observed	1	. 19	-53 32)	
ŀ			S.	-53 46	on shore.	}	+13	-00 02	Monthly mean dip by Robinson's
		ic Obser-	N.S.	-53 51	Ų	-		>-53 34	needles
July 2.		Cape of	Direct.	-54 08		1,			A 1 53 24 A 2 53 24
	Good	Hope.	N.	$-53  15 \\ -53  46$	Observed	}	+13	-53 30	Mean 53 24
	:		S. N.S.	-53  40 $-53  44$	on shore.	J			
June 23.	-34 12	18 26	Direct.	-53 59	s.	1			
bane ze.	01 .~	10 20	N.S.	-53 46	s.	\ + 09	+24	-53 20	
1			Direct.	-53 50	s.s.w.	11	04	-52 56	
			N.S.	-53 17	s.s.w.	$+ 14$	+24	-32 30	
			Direct.	-54 25	s.w.	$  \} + 26$	+24	-53 20	
			N.S.	-5354	s.w.	\\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1 72		
1		<b>့်</b>	Direct.	-55 04	w.s.w.	+41	+24	-53 50	
l	١,	Bay, Cape of Good Hope.	N.S. Direct.	$-54  46 \\ -55  18$	w.s.w.	11			
1		<u> </u>	N.S.	-55   01	w.	$  \rangle + 51$	+24	-53 54	
		00	Direct.	-55 34	w.n.w.	11		50.06	
	1	ي	N.S.	-5449	w.n.w.	$+72$	+24	-53 36	
	1	<b>t</b> o a	Direct.	55 30	N.W.	$  \} + 88$	+24	-53 28	
ľ		ape	N.S.	$-55\ 10$	N.W.	1	~-	00 %	
l		,	Direct.	-5507	N.N.W.	$  \} + 71$	+24	-53 25	
		ay	N.S. Direct.	-5452 $-5436$	N.N.W.	{		>-53 2	To obtain correc- tions for the ship's
1			N.S.	-54 14	N. N.	$  \ \rangle + 75$	+24	-52 46	attraction.
		uc	Direct.	-55 10				50.14	
1		ă 	N.S.	-54 28		$  \} + 71$	+24	-53 14	
		$\mathbf{x}$	Direct.	-55 16	N.E.	$\frac{1}{3} + 87$	+24	_53 10	
1		.=	N.S.	-54  46	N.E.	] ]	+~1	00.10	
1		At anchor in Sinon's	Direct.	-55 34		1 + 72	+24	-53 41	
		inc	N.S.	-54 59		Į			
1		Lt &	Direct. N.S.		E. E.		+24	-53 55	
1		₹, ,	Direct.	-55 05		13		70.40	
1			N.S.	$-54 \ 31$	E.S.E.	$\left \right.\right.$	+24	-53 43	
1			Direct.	-54 24	S.E.	1 + 26	+24	-53 26	
1			N.S.	-54 07	S.E.	1) -20	T 24	-00 20	
1	1		Direct.	-54 39		$\frac{1}{1} + 14$	+24	$[-53 \ 37]$	
1			N.S.	-53 50	S.S.E.	1			

Observations of the Magnetic Force made on board Her Majesty's hired Bark "Pagoda," from the 10th of January 1845 to the 20th of June 1845, with Needle A. of C. 9. one hour after Noon.

Observer, Lieut. T. E. L. MOORE, R.N.

100								Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.		Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected intensity.	Remarks.
1845.											1, 2, 1
Jan. 10.	-34 46	17 46	Def. N.	48 19	64	w. by N.	0.988	008	.000	0.980 ∫	
	,		Def. S.	49 15	64	w. by N.	0.975	008		0.967	
			Def. N.S.	67 36	64	w. by n.	0.988	008			Fresh breezes, a
			Def. N.	46 11	64	w. by n.	1.001	008	1	0.993	head swell.
			Def. S.	45 42	64	w. by N.	1.014	008		1.006	· .
11.	-35 09	15 09	Def. N.	49 23	68		0.960	+.002	1	0.961	
			Def. S.	49 22	68	n.w. by w.		+.002	1	0.974	
			Def. N.S.	68 57	68	и.w. by w.		+.002	002		
			Mag. N.	47 00	66	N.W. by W.		+.002			A little motion.
			Mag. S.	46 54   19 56	66	N.W. by W.		+.002		0.967	
			wt. 1 gr.	19 56 42 14	66	N.W. by W.		+.002		0.925*	: .
10	-35 17	14 00	wt. 2 grs. Def. N.	49 55	78	n.w. by w.		+·002 -·016	1	0.981	
12.	00 17	14 00	Def. N.	50 42	78	$w. \frac{1}{2} s.$ $w. \frac{1}{2} s.$	0.950 0.929	-·016	-·001	0.933	
			Def. N.S.	69 27	78	1 5	0.944	<b>016</b>	005		A little motion.
V .			Mag. N.	48 03	78	W. ½ S. W. ½ S.	0.930	<b>-</b> 016	1	0.913	A little motion.
			Mag. S.	47 16	78	w. ½ s. w. ½ s.	0.952	<b>-</b> 016	ı	0.935	
13.	-35 24	12 92	Mag. N.	48 59	72	$S.W. \frac{1}{2} S.$	0.971	033		0.937	
10.	00 2.	10 20	Mag. S.	50 00	72	s.w. ½ s.	0.952	033	001		14.5
			Mag. N.S.	68 30	72		0.965	033	003		
			Mag. N.	47 13	72	s.w. ½ s.	0.961	033	1	0.00#	
			Mag. S.	46 58	72		0.966	033	I	0.932 > .933	A little motion.
			wt. 1 gr.	19 17	72		0.952	033		0.920*	
			wt. 1½ gr.	30 42	76	$s.w.\frac{1}{2}s.$	0.981	033		0.949	
			wt. 2 grs.	42 46	76	$s.w. \frac{1}{3} s.$	0.968	033		0.936	
15.	-38 49	14 27	Def. N.	47 18	64	s. by w. $\frac{1}{2}$ w.		038		0.981 7	
			Def. S.	48 25	64	s. by w. $\frac{1}{2}$ w.	1.005	<b>038</b>	•000	0.967	
			Def. N.S.	66 52	64	s. by w. $\frac{1}{2}$ w.		038	<b>001</b>	0.967 > .978	Table unsteady, a
			Mag. N.	45 49	64	s. by w. $\frac{1}{2}$ w.		038	-000	0.980	head swell.
	ĺ		Mag. S.	45 21	64	s. by w. $\frac{1}{2}$ w.	1.031	038	.000	0.993	
16.	-39 10	14 38	Def. N.	48 27	70	s.w.byw. $\frac{1}{2}$ w.	0.984	<b> · 024</b>	<b></b> ·001	0∙959 گ	
	•		Def. S.	48 53	70	s.w.byw. $\frac{1}{2}$ w.		<b>024</b>	1 .	0.963	
			Def. N.S.	67 27	70	s.w.by w. $\frac{1}{2}$ w.		024	003		Table very un- steady.
*			Mag. N.	46 37	70	s.w.byw. $\frac{1}{2}$ w.		024	1	0.960	sceauy.
			Mag. S.	46 04	70	s.w.byw. $\frac{1}{2}$ w.		024	1	0.972	*
17.	$-40 \ 41$	14 16	Mag. N.	47 52	68	1	1.000	-024		0.975	
			Mag. S.	48 16	68	1	1.009	024	,		A heavy head swell, much motion.
			Mag. N.S.	66 22	68		1.020	024	002		
21.	-50 21	10 31	Mag. N.	45 42 46 14	45		1.074	032	+.001		
			Mag. S.		45			032	+.001	1.045	Madauata husanaa a
	l		Mag. N.S.	63 54 44 19	45		1.086		+ .004	1.038 >1.051	Moderate breezes, a little motion.
			Mag. N. Mag. S.	44 07	45 45		1.082 1.090	-·032	+·001 +·001	1.050	
23.	50.40	10 10	Mag. N.	44 45	43	s.w. s.w.byw. <del>1</del> w.				1.009	
23.	- 50 40	10 18	Mag. S.	44 54	43	s.w.byw. <del>2</del> w.		-024	+.001	1.007	
			Mag. N.S.	62 39	43	s.w.byw. <del>2</del> w.	1	024	+.001	1.106 >1.093	-
			Mag. N.	43 44	42	s.w.byw.½w.		024			
			Mag. S.	43 43	42	s.w.by w. ½ w.			+.001		
24.	-51 44	9 36	Mag. N.	44 15	49	s.w. by w.		024	+.001	1.105	
1	-5156		Mag. N.S.	62 19	50	s.w.byw.½w.			+.003		Nr. 1
-	01 00	1 3 55	wt. 1 gr.	17 12	50	s.w.byw. <del>2</del> w.		024			Moderate breezes, table steady.
	1	1	wt. 2 grs.	35 29	50	s.w.byw. $\frac{1}{2}$ w.		024		1.107	P.M. A head swell, much motion.
	1				1	1 3 2		1			much motion.

<sup>\*</sup> Omitted in mean.

		T								Corre	ctions.		
				-		Angle of	Tempera- ture.		٠.			G	1
Date.	Lat.		Long	s.	Methou	deflec-	ope ure	Ship's head.	sity	Ship's	Tempe-	Corrected	Remarks.
		1			employed.	tion.	len t	-	en	attrac-	rature.	Intensity.	
ľ		1		1					Intensity.	tion.	Tavuic.	,	l .
		- -		-									
1845.		,	0	,		。 ,						_ ,	i I
Jan. 25.	-53 2	1	7 3	2	Def. N.	43 49	41	s.w.byw. $\frac{1}{2}$ w.					
i		1	1	- 1	Def. S.	43 59	41	s.w.byw. $\frac{1}{2}$ w.	1.152	024	+.001		1
		1			Def. N.S.	61 56	41	s.w. byw. $\frac{1}{2}$ w.	1.147	024	+.006	1.129 >1.134	Table steady; pass- ing through
		-			Mag. N.	42 39	39	s.w.byw. $\frac{1}{2}$ w.					streams of ice.
		1			Mag. S.	42 33	39	s.w.byw. $\frac{1}{2}$ w.	1.174	024	+.002	1.152	· I
26.	-54 0	2	6 (	12	Def. N.	43 43	42		1.148		+.001		
1		1	•	_	Def. S.	44 14	42	w. by n.	1.145	1	+.001		1
	1	1		1	Def. N.S.	62 09	42	w. by N.	1.142		+.006		
	1	1		- 1	Mag. N.	43 00	40	w. by n.		012	+.002		Very steady, small
] .	)	-			Mag. S.	42 44	40	w. by N.	1.164		+.002		pieces of loose ice
1	1	1				_	40		1.096	1 .	+.002		about the ship.
1					wt. 1 gr.		40	w. by n.	1.164	1	+.002		
					wt. 2 grs.	34 23	1	w. by n.	1	1	1		
	-551		5		Def. N.	42 50	39	s.s.w. $\frac{1}{2}$ w.			+.001	1.143 1.146	Ship pitching heavily, fresh
31.	-61 1	4	9 (	07	Def. N.	39 38	37	S.S.E.	1.324		+.002		breezes.
		1			Def. S.	40 08	37	S.S.E.	1.320		+.002		
į.	1				Def. N.S.	57 04	37	S.S.E.	1.331		+.008		Table steady, heavy snow, passing
Ì	1	Ì			Mag. N.	39 45	37	S.S.E.	1.310	-042	+.003	1.271	various icebergs.
	1				Mag. S.	39 30	37	S.S.E.	1.349	-042	+.003	ر 1.310	
Feb. 1	-62 (	6	12	52	Def. N.	38 10	37	s.E. by s.	1.398	040	+.002	1.360 } 1.340	Much motion, table
1	1				Def. S.	38 58	37	s.E. by s.	1.376	040	+.002	1.338	unsteady.
2	-61 8	66	16	36	Def. N.	39 17	37	S.E. 1 E.	1.341	036	+.002	1.307	
					Def. S.	39 21	36	S.E. $\frac{1}{2}$ E.	1.357		+.002		
1	. [				Def. N.S.	56 28	36	S.E. ½ E.	1.358	1	+.009		Heavy snow, a head
1	İ	- 1			Mag. N.	39 21	36	S.E. $\frac{1}{2}$ E.	1.339		+.003		sea, ship pitching violently.
1		1			Mag. S.	39 08		S.E. $\frac{1}{2}$ E.	1.372		+.003		violently.
4	-63	<b>7</b> 0		10	Def. N.	38 17			1.391				
1 7	-03 (	ייי	zu	40		38 35		S. ½ E.	1.395			1 5	
1	1				Def. S.	1 0		S. ½ E.	1.376	1	1	1 1	
1					Def. N.S.	56 04		S. $\frac{1}{2}$ E.	1.406			1·333   1·357 >1·34	Water very clear
1					Mag. N.	38 17		S. ½ E.	1		+.002	1.	from ice, a little
1					Mag. S.	38 35		S. $\frac{1}{2}$ E.	1.405			1.356	Vibration great.
-	.				wt. 1 gr.	13 26		Ś. ½ E.	1.353	1		1.300*	A Interior Brown
1		-			wt. 2 grs.	27 58	1 -	$S_{\bullet} \frac{1}{2} E_{\bullet}$	1.402			1.349	
	-63	19	21	48	Def. N.	38 36		S.S.E.	1.376	1 -		1.332	
1	l	-			Def. S.	38 24	37	S.S.E.	1.405	1		1.361	
1		I			Def. N.S.	55 38	37	S.S.E.	1.397	1 -		1.360	
ľ	1				Mag. N.	38 27	36	S.S.E.	1.396	1			2 A heavy swell from S.E., light breezes,
1	1 .	ı			Mag. S.	38 38		S.S.E.	1.407	1 .		1.364	table steady.
1		١			wt. 1 gr.	13 51			1.313	-046	-003	1.264*	
1	1		,		wt. 2 grs.	26 57			1.45(	-046	-003	3 1·401 J	and the second
1 6	664	25	24	18		37 17			1.447	-045			
1	-		~ -		Def. S.	37 48	3 39			-045			8 Water perfectly
1	1	- 1			Def. N.S.	54 5	39				+.008		smooth, very
	765	30	00	10		36 3			1.48		+.00	1.437	steady.
1	00	υJ	20	*0		37 1		1 - 7 -			+.00		
1	1				Def. S.				1.46			3 1.423	
1					Def. N.S.	54 1.		S. Dy E. 2 E	1.40	$\frac{1}{2} - 05$			2 Table steady, water
1	1				Mag. N.	37 0			1.40	7 - 100			smooth, no ice in
- 1	1				Mag. S.	37 20						2 1.438	sight.
ſ					wt. 1 gr.	13 0			1.399			2 1.340*	,
		ŧ			wt. 2 grs.	26 2			1.47			2 1.423	
	866	27	30	45		36 2			1.49	4 -049	s  +.008	2 1.454	
I	1		1		Def. S.	36 5			1.48	1	s  +.00	2 1.443	
1	1				Def. N.S.	54 0	5 33	s.E. by E.	1.47				8 Fresh breeze, table unsteady.
1					Mag. N.	37 0	0 30	s.E. by E.	1.49			4 1.461	umounty.
1	1				Mag. S.	37 3		s.E. by E.	1.47	5 -04	5 + .00	4 1·437 J	4
I					1			1				1	- L

<sup>\*</sup> Omitted in mean.

	į.				-g			Corre	ections.		
Date.	Lat.	Long.	Method employed.	Angle of deflection.	Tempera-	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845. Feb. 9.	-66° 36	36 50	Def. N.	3Ĝ 0Ć	3°9	s.e. by e.	1.514	042	+.001	1.473)	
			Def. S.	36 43	39	s.e. by E.	1.508	042		1.467	
			Def. N.S.	53 41	36	s.E. by E.	1.505	042		1.473 >1.470	Light breeze, very
			Mag. N.	36 55	35	s.e. by E.	1.505	042		1.466	steady, water smooth.
	-		Mag. S.	36 59	34	s.E. by E.	1.509	042		1.470	
10.	-67 11	38 51	Def. N.	35 39	34	s. by w.		050		1.492	
			Def. S.	36 31	34	s. by w.	1.509	050		1.461	
1			Def. N.S.	52 45	34	s. by w.	1.549	050	+.009	1.508 >1.483	Steady, water very smooth.
			Mag. N.	36 27	34	s. by w.	1.540	050	+.003	1.493	J
11.	67 20	10 00	Mag. S.	37 02	$\frac{34}{35}$	s. by w.	1.509	-·050 -·016	+.003	1.462	0-11
12.	-67 39 $-67 18$		Def. N. Def. N.	36 10     35 30	32	N.E.	1.510 1.548	-·050	+.002	1.496 1.496	Sailing along a pack of ice, unsteady.
12.	-0/ 10	10 22	Def. N.	36 07	$\frac{32}{32}$	S. $\frac{1}{2}$ E. S. $\frac{1}{2}$ E.	1.533	<b>-</b> ⋅050	+.003	1.486	1
			Def. N.S.	53 16	32	S. ½ E.	1.520	-050	+.013		Fresh breeze, table
			Mag. N.	36 37	32	S. ½ E.	1.529	<b></b> 050	+.004	1.483	unsteady.
			Mag. S.	36 03	32	S. ½ E.	1.575	<b></b> ·050	+.004	1.529	
13.	-66.55	14 16	Def. N.	36 00	34	E.N.E.	1.519	025	+.002	1.496	
			Def. S.	36 37	34	E.N.E.	1.504	025	+.002	1.481	Ü
			Def. N.S.	53 29	33	E.N.E.	1.506	025	+.011	1.492 >1.490	Swell from E., table
	- 1		Mag. N.	36 43	33	E.N.E.	1.521		+.004	1.500	unsteady.
			Mag. S.	37 06	33	E.N.E.	1.503	025	+.004	ر 1·482	:
14.	-66 24	40 01	Def. N.	36 18	34	N.E. by N.	1.502		+.003	1.488 1.494	Table unsteady, very
	0	00.05	Def. S.	36 24	34	1	1.515		+.002	1.501	squally.
16.	-64 52	38 37	Def. N.	35 59	41	s. by E.	1.520		+.001	1.471	:
	-		Def. S.	36 56	41	s. by E.	1.487		+.001	1.438	m
			Def. N.S. Mag. N.	53 48	41 40	s. by E.	1·490 1·493		+.008		Thick weather, a heavy swell, un-
			Mag. S.	37 07 37 15	40	, ,	, - ,		+.003 $+.003$	1·446 1·445	steady.
17.	<b>-66 43</b>	40 12	Def. N.	36 34	36				+ 003	1.471	
	30 10		Def. S.	37 08	36				+.005	1.459	
		1	Def. N.S.	53 18	38	1			+.010	- 1	Calm, a heavy sea,
1		ŀ	Mag. N.	36 53	38			. 1	+.003	1.490	not steady.
			Mag. S.	37 13	37		1.495	<b></b> ·018	+.003	1.480	
19.	-64 05	41 09	Def. N.	36 35	37	E. by s.	1.486	<b></b> ·035	+.002	1.453 1.453	Very unsteady, a
20.	-63 19	45 52	Def. N.	36 12		s.e. by E. $\frac{1}{2}$ E.	- 1		+.001	1.468	swell from N.
-			Def. S.	37 10		s.e. by e. ½ e.			+.001	1.435	
1	CO. 00	45 50	Def. N.S.	53 40		S.E. by E. $\frac{1}{2}$ E.		040		1.463	A heavy swell, strong
-	-63 22	45 58	Def. N.	36 08	44			046	+:001	1.400	breeze, with a heavy sea running.
	1		Def. S.	36 33 53 22	42	S.E.	1.507	046	+ .000	1.462	neavy sea running.
21.	-63 36	46 46	Def. N.S. Def. N.	36 00	39 40	S.E.	1.510	046	1.009	1.477	
21.	-00 00	10 40	Def. S.	36 33	39	S.E.	1.507	046	T.001	1.474	
		1	Def. N.S.	53 23	39	S.E.	1.513	046		1.476	
-	-63 36	46 50	Def. N.	36 01	40		1.518			1.473	
Ì	- 3	1	Def. S.	36 37	40		1.505	-046		1.460 >1.470	Table unsteady, much motion.
		1	Def. N.S.	53 26	39	S.E.	1•511  -	• 046		1.474	
			Mag. N.	36 39	39	S.E.	1.525 -	-•046	+.003	1.482	1
	0.5	-	Mag. S.	37 09	39	1		- 046		1.457	
25	-61 34	53 49		35 41	42		1.537	- 044	+.001	1.494	
	1	1	Def. S.	36 13	42			- 044	+.001	1.484	
Ì	1	1		53 21	40		1.515 -	- 044	+ 009	1.480 >1.498	resh breeze, table steady.
1		·	Mag. N. Mag. S.	36 14 36 19	39 39		•558  -  •557  -	_·044  - _·044  -	+.003	1.517	· .
	1		mag. D.	50 19	UJ .	D.E 2 E.	. 007	- 014	T 009	1 010	:

				Angle of deflec- tion.		T		0			
				Angle of	Fa.		Intensity.	Corre	ctions.		1
Date.	Lat.	Long.	Method	deflec-	npe	Ship's head.	sua	Ship's	Tempe-	Corrected	Remarks.
		-	employed.	tion.	Ter		II I	attrac-	rature.	Intensity.	
								tion.			
1845.											
Feb. 26.	-61° 29	57 33	Def. N.	35 11	40°	S.E. 1/2 E.	1.566		+.001		41
			Def. S.	35 46	40	S.E. 1/2 E.	1.552	044			·
			Def. N.S.	52 55	40	S.E. ½ E.	1.541	044	+.009		
	-61 22	57 41	Def. N.	35 07	40	S.E.	1.571	046	+.001		
THE COURT			Def. S.	35 57	40	S.E.	1.540	046	+.001		Fresh breezes, table
			Def. N.S.	52 58 36 24	40 39	S.E.	1.540 1.543	-·046 -·046	+.003	1.909	steady.
			Mag. N. Mag. S.	36 22	38	S.E.	1.553	_·046	+.003		
			wt. 1 gr.	12 41	38		1.432	046	<b></b> 003	1.383*	
		ļ	wt. 2 grs.	25 29	38	S.E.	1.528	046	003		
27.	-61 10	64 20	Def. N.	34 35	39		1.602	<b>04</b> 8	+.002	1.556	
			Def. S.	34 49	39	S.S.E. 1 E.	1.610	<b>04</b> 8	+.002	1.564 } 1.560	Very unsteady.
28.	-6149	71 30	Def. N.	33 47	38	S.S.E.	1.651	049	+.002	1.604 )	
			Def. S.	34 15	38	S.S.E.					Very unsteady.
			Def. N.S.	51 17	37	S.S.E.	1.635	049	+:010		
			Mag. N.	34 35	37	S.S.E.	1.680	049	+.003		Table steady.
	C		Mag. S.	35 15	35	S.S.E.	1.637	049	+.003	- 00-	Table steauy.
	-6149	71 32	Def. N.	33 26	35	1	1.675 $1.632$	049 049	+.002	1.628	
Ĩ			Def. S. Def. N.S.	34 27 51 05	35 35	1	1.646	049	$^{+.002}_{+.011}$	1.600	
Mar. 1.	_69 10	70 05	Def. N.S.	33 14	46	s.s.e. s.e. by s.	1.687		+.002		
iviai. 1.	-02 10	12 23	Def. S.	33 31	46	s.e. by s.	1.692	047	+.002	1.647	
			Def. N.S.	50 33	46	s.E. by s.	1.680	047	+.006	1.639	
			Mag. N.	34 24	46		1.695	047	+.002	1.650 >1.642	Calm, table steady.
			Mag. S.	34 49	46		1.673	047	+.002	1.628	
			wt. 1 gr.	10 37	46		1.706	047	002	1.657*	.
			wt. 2 grs.	22 49	46		1.695	047	002		
2.	-62 47	76 14	Def. N.	33 15	42	s.e. by E. ½ E.	1.687	047		1.641	
Ì			Def. S.	33 30	42	s.e. by e. $\frac{1}{2}$ e.	1.693	041	+.001	1.653	
			Def. N.S.	50 26	42	s.e. by E. ½ E.	1.086	041	+.008	1.653	
MENON CO.			Mag. N.	34 15 34 40	42 42	s.e. by E. \frac{1}{2} E.	1.605	041 041	+.003	1.647	
			Mag. S. wt. 1 gr.	11 02	42	s.e. by $e.\frac{1}{2}e.$ s.e. by $e.\frac{1}{2}e.$	1.643		+ 003	1.599*	Steady breeze, table
			wt. 2 grs.	22 31	42	s.E. by E. $\frac{1}{2}$ E.		041	003	1 033" 1	steady.
	-62 40	76 16	Def. N.	32 46	42	S.E. Dy E. 2 E.	1.717	056	+.002		
	0.2	1.0 10	Def. S.	33 30	42	s.	1.693	056	+.002	1.639	
		1	Def. N.S.	50 24	42	s.	1.688	056	+.008	1.640	
3.	-64 20	79 38	Def. N.	32 32	34	s. by $w.\frac{1}{2}w$ .		054	+.003	1.681 7	
R. C. C. C. C. C. C. C. C. C. C. C. C. C.			Def. S.	32 58	32	s. by $w.\frac{1}{2}w$ .	1.728	054	+.003	1.677 >1.678	Fresh breeze, un-
			Def. N.S.	49 56	31	s. by $w \cdot \frac{1}{2} w$ .		054	+ .014	1·677 J	steady, thick, with squalls of snow.
5.	-61 49	85 07	Def. N.	31 35	36	S.E. ½ E.	1.795	-049	+.003	1.748 }	
2.0			Def. S.	32 09	37	S.E. 1 E.	1.783	049	+.002	1.736 >1.730	Unsteady; aurora visible.
	60.40	00.00	Def. N.S.	49 35	37	S.E. $\frac{1}{2}$ E.	1.742	-·049	+.012	1.700	
6.	-00 48	88 33	Def. N. Def. S.	$\begin{vmatrix} 31 & 34 \\ 32 & 27 \end{vmatrix}$	39	S.E.	1.796 1.762	-·051 -·051	$+002 \\ +002$	1.713	
			Def. N.S.	49 32	38	S.E.	1.746		+.011	1.706 1.747	Very unsteady, with
Programme and the second			Mag. N.	32 38	37	S.E.	1.833		+.004	1.786	thick weather.
			Mag. S.	33 01	37	S.E.		051	+.004	1.783	
7.	-61 23	91 15	Def. N.	31 46	41	s.s.w.	1.783		+.002	1.732	
1			Def. S.	32 14	42	s.s.w.	1.779	1 -	+.002	1.728	
			Def. N.S.	49 00	42	s.s.w.	1.785	053	+.009	1.741 >1.749	Unsteady.
	ļ ·		Mag. N.	32 54	42	s.s.w.	1.811	053	+.003	1.761	1
			Mag. S.	32 57	42	s.s.w.	1.834	-053	+.003	1.784	
1	i	1	1				1	1			<u> </u>

<sup>\*</sup> Omitted in mean.

			1	Angle of	ra-		ity.	Corre	ctions.		
Date.	Lat.	Long.	Method employed.	deflec- tion.	Tempera- ture.	Ship's head.	Intensity.	Ship's attrac- tion.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.	-61° 07	9ž 1ó	Def. N.	31 13	4î	7 G 7	1.004	.046	1.000	1.700	
Mar. 8.	61 .07	92 10			1	E.S.E.	1.700		+.002	1.780	
			Def. S.	32 04	40	E.S.E.	1.790	046	+.002		Unsteady, with snow.
	Co 00	00.01	Def. N.S.	49 04	38	E.S.E.	1.782	046	+.011		
9.	<b>60 30</b>	92 34	Def. N.	31 19	40	s.E. by E.	1.817	048	+.002		
			Def. S.	32 09	41	s.e. by e.	1.784	048	+.002		Very unsteady.
1	00.00	00.00	Def. N.S.	49 08	41	s.e. by e.	1.780	-·048	+.010	1 700 1	
10.	-60 03	96 03	Def. N.	31 08	39	E.S.E.	1.832	:046	+.002	1.788 $1.770$	Aurora visible,
			Def. S.	31 56	38	E.S.E.	1.796	046	+.002		table steady.
11.	-5945	99 50	Def. N.	29 54	35	E. $\frac{1}{2}$ N.	1.919	041	+.002	1.880	
			Def. S.	30 31	34	E. $\frac{1}{2}$ N.	1.908	041	+.002	1.809	
			Def. N.S.	48 58	34	E. $\frac{1}{2}$ N.	1.788	041	+.013	1.700 >1.830	A heavy sea, very unsteady.
			Mag. N.	32 21	34	E. $\frac{1}{2}$ N.	1.855	041	+.004	1.818	
			Mag. S.	32 23	34	E. 1/2 N.	1.888	041	+.004		
13.	-5746	99 17	Def. N.	30 34	46	E.N.E.	1.870	039	+.001		Very unsteady.
			Def. S.	31 28	46	E.N.E.	1.831	039	+.001	1 1 20	
14.	-5656	101 36	Def. N.	30 31	40	E. by s.	1.876		+.002	1.831	
4			Def. S.	31 20	41	E. by s.	1.842		+.002	1.797 >1.80%	A.M. Aurora visible unsteady.
Ï			Def. N.S.	48 35	41	E. by s.	1.816		+.010	ر 1•779	unsteady.
15.	-55 40	$ 103 \ 18 $		30 30	41	E.N.E.	1.876	-039			
			Def. S.	31 10	41	E.N.E.	1.854		+.002		Squally with snow, unsteady.
			Def. N.S.	48 34	41	E.N.E.	1.817			1.788	ansionay.
16.	<b>54 3</b> 8	106 15		30 03	39	Е.	1.909	-045	+.002	1.866	
			Def. S.	31 18	38	<b>E</b> •	1.844	045		1.801 >1.817	Heavy squalls, un-
			Def. N.S.	48 34	38	E.	1.817	045	+.012	1.784	steady, snow.
17.	-54 10	108 15	Def. N.	29 59	39	E. by s.	1.913	047	+.002	1.868 ∫	
			Def. S.	31 05	40	E. by s.	1.860	047	+.002	1.815 >1.821	A strong gale, very
			Def. N.S.	48 34	40	E. by s.	1.817	047	+.011	1.781	unsteady.
18.	-53 00	110 30	Def. N.	30 28	44	N.E.	1.878	036	+.002	1.844 5	
			Def. S.	31 14	44	N.E.	1.849	036			
			Def. N.S.	48 30	43	N.E.	1.822	036	+.009	1.795 >1.825	Unsteady, a heavy
			Mag. N.	31 55	43	N.E.	1.889	-:036	+.003	1.856	swell from west- ward. strong
			Mag. S.	32 48	43	N.E.	1.850	036	+.003	1.817	breeze.
20.	-4857	112 56	Def. N.	30 52	47	N.E. 1 N.	1.849	035	+.001	1.815	
	İ		Def. S.	31 26	48	N.E. $\frac{1}{2}$ N.	1.834	035		1.800	
			Def. N.S.	48 22	48	N.E. $\frac{1}{2}$ N.	1.831	035	+.006	1.802	
			Mag. N.	32 20	49	N.E. $\frac{1}{2}$ N.	1.857	035	+.002	1.004	
	j		Mag. S.	32 58	49	N.E. $\frac{1}{2}$ N.	1.835	035	+.002	1.802 >1.821	Fresh breeze, very unsteady.
		}	wt. 1 gr.	9 59	50	N.E. $\frac{1}{2}$ N.	1.813	035		1.776*	
	1.	,	wt. 2 grs.	20 01	50	N.E. $\frac{1}{2}$ N.	1.920	035	002		
		1	wt. 3 grs.	31 32	50	$N.E. \frac{1}{2} N.$	1.859	035			1
22.	-47 21	115 15		30 38	50	$N.W. \frac{1}{2} N.$	1.866		+.001		
~~.	'		Def. S.	30 34	50	$N.W. \frac{1}{2} N.$	1.897	029	+.001	1.869	
			Def. N.S.	48 29	50	$N.W. \frac{1}{2} N.$	1.821	029	+.005		Light breeze, table
			Mag. N.	32 07	50	$N.W. \frac{1}{2} N.$	1.876	029	+.002	1.849	steady, thick fog
			Mag. S.	32 26	50	$N.W. \frac{1}{2} N.$	1.885	029	+.002	1.858	
24.	45 08	116 50	Def. N.	31 01	49	N. by E.	1.840		+.001	1.821 7	
~ 1.	-0 00		Def. S.	31 21	50	N. by E.	1.838	1	+.001		A heavy swell from westward, un-
25.	-43 22	116 40		31 06	55	$N \cdot \frac{1}{3} E \cdot$	1.833	020		1.813	steady.
~0.	1	1.3	Def. S.	31 49	55	N. 1/2 E.	1.807	1		1.787	
			Def. N.S.	48 57	55	N. ½ E.	1.789		+.002		
		1	Mag. N.	32 33	55	1 7	1.840	1	+.001	1 1	A heavy swell, um-
ì			Mag. N.	33 24	56	N. ½ E. N. ½ E.	1.793		+.001		steady.
		1		10 20	56		1.753			1.732*	
	1		wt. 1 gr.	20 30	56	N. $\frac{1}{2}$ E.	1.877		001		
	1.		wt. 2 grs.	20 00	30	N. ½ E.	1.011	-020		1.000	

<sup>\*</sup> Omitted in mean.

	4	1 1	•				•	Corre	ctions.	,	
			Method	Angle of	Tempera- ture.	61.1.1.1.1	Intensity.	~		Corrected	Daine Ver
Date.	Lat.	Long.	employed.	deflec- tion.	E E	Ship's head.	ten	Ship's attrac-	Tempe-	Intensity.	Remarks.
				mon.	Te		In	tion.	rature.	,	
1845.			A								
Mar. 26.	-41 00	116 42	Def. N.	31 40	56	n. by w.	1.790	-020	•000	1.770	
			Def. S.	31 37	56	N. by w.	1.821	020		1.801	
			Def. N.S.	49 41	56	N. by w.	1.736	020	+.002	1.718 >1.758	A heavy westerly
			Mag. N.	33 19	56	N. by w.	1.780	020	+.001		swell.
			Mag. S.	33 46	56	n. by w.	1.759	020	+.001	1.740	
27.	-38 40	116 15		32 33	62		1.731	012	i .	1.719	
			Def. S.	32 35	62		1.752	012			Table steady.
			Def. N.S.	49 55	62	1 .	1.720	012		1.707	
28.	-37 00	116 57		33 12	63	N. by E.	1.689	012		1.677	
			Def. S.	33 34	64	N. by E. $\frac{1}{2}$ E.		012		1.675	
			Def. N.S.	50 42	64	N. by E. $\frac{1}{2}$ E.		-012		1.656	
		-	Mag. N.	34 06	68	N. by E. $\frac{1}{2}$ E.		-012	001	)	Unsteady.
			Mag. S.	34 41	68	N. by E. $\frac{1}{2}$ E.		-012	001	1.009	
			wt. 1 gr.	11 08	68	N. by E. $\frac{1}{2}$ E.		-012	+.001	1.617*	
			wt. 2 grs.	22 48	68	N. by E. $\frac{1}{2}$ E.		-012		1.685	
			wt. 3 grs.	35 19	65	N. by E. $\frac{1}{2}$ E.		-012		1.671	
29.	-36 11	116 48		33 12	67	N.N.E.	1.689	-012	1	1.676	Trestande
	-		Def. S.	33 21	67 68	N.N.E.	1.702	012	-·001 -·003		Unsteady.
20	27 07	117 20	Def. N.S.	50 51	66	N.N.E.	1.661 1.708	-·012			
30.	-35 07	117 38		32 54	66	N.N.E.	1.712	-012			Unsteady.
			Def. S. Def. N.S.	33 13 50 12	66	N.N.E.	1.701	-012	-002		E Distance
A	-35 02	117 56	Def. N.S.	33 11	68	N.N.E.	1.690	- 012	-001		
April 7.	King G		Def. N.	33 32	68	11	1.690		001		
	Sound,		Def. N.S.	50 24	68		1.689		003		
	Aust		Mag. N.	34 30	68	11	1.687		001		
	21450		Mag. S.	34 34	69	Observed			001	1.600	
		1	wt. 1 gr.	10 44	69	on shore.	1.688		+.001		On the 8th needle A. was found to have
		1	1		69	011 2110101			+.001		been injured,
<b>.</b>		ì	wt. 14 or.	117 lb			11.088				1 . 11 . D
1	U		wt. $1\frac{1}{2}$ gr. wt. 2 grs.	17 16 22 56			1.688 1.688				needle B. was therefore used
	u		wt. 2 grs.	22 56	69		1.688		+.001	1.689	
	ru		wt. 2 grs. wt. $2\frac{1}{2}$ grs.	22 56 28 18	69 69				+.001	1.689 1.689	therefore used
,			wt. 2 grs.	22 56	69		1.688 1.688		+.001	1.689 1.689	therefore used
			wt. 2 grs. wt. $2\frac{1}{2}$ grs.	22 56 28 18	69 69	Needle B	1.688 1.688 1.688		+.001	1.689 1.689	therefore used
			wt. 2 grs. wt. 2½ grs. wt. 3 grs.	22 56   28 18   35 11	69 69 69	Needle B	1.688 1.688 1.688		+·001 +·001 +·001	1.689 1.689 1.689	therefore used
12.		117 56	wt. 2 grs. wt. 2½ grs. wt. 3 grs.  Def. N.	22 56 28 18 35 11	69 69 69	Needle B	1.688 1.688 1.688		+·001 +·001 +·001	1.689 1.689 1.689	therefore used
12.	King G	eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs.  Def. N. Def. S.	22 56 28 18 35 11 29 23 35 31	69 69 69 64 64	Needle B	1.688 1.688 1.688		+·001 +·001 +·000 -000	1.689 1.689 1.689	therefore used subsequently.
12.		eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs.  Def. N. Def. S. Def. N.S.	22 56 28 18 35 11 29 23 35 31 50 11	69 69 69 64 64 64		1.688 1.688 1.688 1.688		+·001 +·001 +·000 ·000 ·000	1.689 1.689 1.689 1.689 1.657 1.657	therefore used subsequently.
12.	King G	eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs.  Def. N. Def. S. Def. N.S. Mag. N.	22 56 28 18 35 11 29 23 35 31 50 11 31 37	69 69 69 64 64 64 64	Observed	1.688 1.688 1.688 1.671 1.657 1.679 1.658		+·001 +·001 +·001 +·000 ·000 ·000 ·000	1.689 1.689 1.689 1.689 1.657 1.657 1.679 1.658	therefore used subsequently.
12.	King G	eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs.  Def. N. Def. S. Def. N.S. Mag. N. Mag. S.	29 23 35 31 29 23 35 31 50 11 31 37 36 25	69 69 69 64 64 64 64 62		1.688 1.688 1.688 1.688		+·001 +·001 +·000 ·000 ·000 ·000 ·000	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653	therefore used subsequently.
12.	King G	eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs.  Def. N. Def. S. Def. N.S. Mag. N. Mag. S. wt. 1 gr.	29 23 35 31 50 11 31 37 36 25 16 13	69 69 69 64 64 64 62 62	Observed	1.688 1.688 1.688 1.688 1.657 1.657 1.658 1.653 1.693		+·001 +·001 +·001 -000 -000 -000 -000 -000	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693	therefore used subsequently.
12.	King G	eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 1 gr. wt. 1½ gr. wt. 1½ gr.	29 23 35 11 29 23 35 31 50 11 31 37 36 25 16 13 24 39	69 69 69 64 64 64 62 62 62 62	Observed	1.688 1.688 1.688 1.688 1.657 1.657 1.658 1.653 1.693 1.672		+·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 ·000 ·000	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.672       1.688	therefore used subsequently.
	King G Sou	reorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 1 gr. wt. 1½ gr. wt. 2 grs.	29 23 35 11 29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27	69 69 64 64 64 62 62 62 62	Observed on shore.	1.688 1.688 1.688 1.688 1.657 1.659 1.658 1.693 1.672 1.698		+·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 ·000 ·000	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.698       1.688	therefore used subsequently.
12.	King G Sou	eorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 1 gr. wt. 1½ gr. wt. ½ grs. Def. N.	29 23 35 11 29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03	69 69 69 64 64 64 62 62 62 62 66	Observed on shore.	1.688 1.688 1.688 1.688 1.657 1.679 1.658 1.693 1.672 1.698 1.670		+·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 ·000 ·000	1.689       1.689       1.689       1.689       1.689       1.657       1.679       1.658       1.653       1.693       1.698       1.658	therefore used subsequently.
	King G Sou	reorge's	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 1 gr. wt. 1½ gr. wt. ½ grs. Def. N. Def. S. Def. N. Def. S.	29 23 35 11 29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01	69 69 69 64 64 64 62 62 62 62 66 66	Observed on shore.	1.688 1.688 1.688 1.688 1.657 1.659 1.658 1.693 1.672 1.698 1.670 1.687		+·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 ·000 -·001 -·001	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.698       1.658       1.658       1.675       1.672       1.672       1.672       1.672       1.672       1.672       1.672       1.672       1.672       1.672	therefore used subsequently.
23.	King G Sou -35 30	eerge's and.	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 1 gr. wt. 1½ gr. wt. ½ grs. Def. N. Def. S. Def. N. Def. S. Def. N. Def. S. Def. N. S.	29 23 35 11 29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55	69 69 69 64 64 64 64 62 62 62 66 66 66	Observed on shore.  N.W. N.W. N.W.	1.688 1.688 1.688 1.688 1.657 1.657 1.658 1.693 1.672 1.698 1.670 1.687 1.696		+·001 +·001 +·001 +·001 -000 -000 -000 -000 -001 -001 -002	$ \begin{array}{c c} 1.689 \\ 1.689 \\ 1.689 \end{array} $ $ \begin{array}{c c} 1.711 \\ 1.657 \\ 1.679 \\ 1.658 \\ 1.693 \\ 1.698 \\ 1.658 \\ 1.658 \\ 1.675 \\ 1.683 \end{array} $	therefore used subsequently.
	King G Sou -35 30	reorge's	Wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs.     Def. N. Def. S. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07	69 69 69 64 64 64 62 62 62 66 66 66 66 69	Observed on shore.  N.W. N.W. N.W. N.W. N.W.	1.688 1.688 1.688 1.688 1.657 1.657 1.658 1.693 1.672 1.698 1.670 1.687 1.696 1.602		+·001 +·001 +·001 +·001 -000 -000 -000 -000 -001 001 002 001	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.693       1.693       1.658       1.658       1.658       1.658       1.658       1.658       1.658       1.590	therefore used subsequently.
23.	King G Sou -35 30	eerge's and.	Wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs.     Def. N. Def. S. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N. Def. S. Def. N. Def. S.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07 36 26	69 69 69 64 64 64 64 62 62 62 66 66 66 69 69	Observed on shore.  N.W. N.W. N.W. N.W. N.W. N.W. by N. N.W. by N.	1.688 1.688 1.688 1.688 1.657 1.658 1.653 1.693 1.672 1.696 1.687 1.696 1.602 1.603		+·001 +·001 +·001 +·001 -·000 ·000 ·000 ·000 -·001 -·001 -·002 -·001 -·001 -·001	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.693       1.658       1.658       1.658       1.675       1.683       1.590       1.591	therefore used subsequently.  Very unsteady, heavy south-west swell.
23.	King G Sou -35 30	eerge's and.	Wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs.     Def. N. Def. S. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07 36 26 51 30	69 69 69 64 64 64 62 62 62 66 66 66 69 69	Observed on shore.  N.W. N.W. N.W. N.W. N.W. by N. N.W. by N. N.W. by N.	1.688 1.688 1.688 1.688 1.657 1.658 1.653 1.693 1.672 1.696 1.680 1.696 1.602 1.603 1.599		+·001 +·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 -·001 -·001 -·001 -·004	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.698       1.658       1.658       1.658       1.658       1.591       1.584       1.573	therefore used subsequently.
23.	King G Sou -35 30	eerge's and.	Wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs.     Def. N. Def. S. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Mag. N.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07 36 26 51 30 33 14	69 69 69 64 64 64 62 62 62 66 66 66 69 69 69	Observed on shore.  N.W. N.W. N.W. N.W. N.W. by N. N.W. by N. N.W. by N. N.W. by N.	1.688 1.688 1.688 1.688 1.657 1.658 1.653 1.693 1.672 1.686 1.687 1.686 1.602 1.603 1.599 1.547		+·001 +·001 +·001 +·001 -000 -000 -000 -000 -001 001 001 001 004 004	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.698       1.658       1.658       1.658       1.672       1.591       1.591       1.584       1.535	Very unsteady, heavy south-west swell.
<b>23.</b> 25.	—35 30 —32 24	eorge's and.	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. N. Def. N. Def. N. Def. N. Def. N. Def. N. Mag. N. Mag. N. Mag. S.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07 36 26 51 30 33 14 37 23	69 69 69 64 64 64 64 62 62 66 66 66 69 69 69 69	Observed on shore.  N.W. N.W. N.W. N.W. by N. N.W. by N. N.W. by N. N.W. by N.	1.688 1.688 1.688 1.688 1.671 1.657 1.658 1.653 1.693 1.670 1.687 1.698 1.670 1.698 1.670 1.699 1.547 1.577		+·001 +·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 -·001 -·001 -·001 -·001 -·004 -·001 -·001	$ \begin{array}{c c} 1.689 \\ 1.689 \\ 1.689 \end{array} $ $ \begin{array}{c c} 1.711 \\ 1.657 \\ 1.679 \\ 1.658 \\ 1.653 \\ 1.698 \\ 1.658 \\ 1.658 \\ 1.658 \\ 1.590 \\ 1.591 \\ 1.584 \\ 1.535 \\ 1.565 \end{array} $	Very unsteady, heavy south-west swell.
23.	—35 30 —32 24	eerge's and.	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Mag. N. Mag. S. Def. N.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07 36 26 51 30 33 14 37 23 32 17	69 69 69 64 64 64 64 62 62 66 66 66 69 69 69 72	Observed on shore.  N.W. N.W. N.W. N.W. by N. N.W. by N. N.W. by N. N.W. by N. N.W. by N. N.W. by N. N.W. by N.	1.688 1.688 1.688 1.688 1.671 1.657 1.658 1.653 1.672 1.698 1.670 1.687 1.602 1.603 1.539 1.547 1.577		+·001 +·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 -·001 -·001 -·001 -·001 -·001 -·001 -·001 -·001 -·001	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.658       1.658       1.658       1.658       1.658       1.591       1.591       1.584       1.555       1.518	Very unsteady, heavy south-west swell.  Moderate breeze, table steady.
23. 25.	—35 30 —32 24	eorge's and.	wt. 2 grs. wt. 2½ grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. wt. 3 grs. Def. N.S. Mag. N. Mag. S. wt. 1 gr. wt. ½ grs. Def. N. Def. N. Def. N. Def. N. Def. N. Def. N. Def. N. Mag. N. Mag. N. Mag. S.	29 23 35 31 50 11 31 37 36 25 16 13 24 39 33 27 30 03 35 01 49 55 31 07 36 26 51 30 33 14 37 23	69 69 69 64 64 64 64 62 62 66 66 66 69 69 69 69	Observed on shore.  N.W. N.W. N.W. N.W. by N. N.W. by N. N.W. by N. N.W. by N.	1.688 1.688 1.688 1.688 1.671 1.657 1.658 1.653 1.693 1.670 1.687 1.698 1.670 1.698 1.670 1.699 1.547 1.577		+·001 +·001 +·001 +·001 -·000 ·000 ·000 ·000 ·000 -·001 -·001 -·001 -·001 -·001 -·001 -·001 -·001 -·001 -·001	1.689       1.689       1.689       1.689       1.689       1.657       1.657       1.658       1.653       1.693       1.658       1.658       1.658       1.658       1.568       1.590       1.591       1.584       1.535       1.555       1.518       1.499       1.499	therefore used subsequently.  Very unsteady, heavy south-west swell.

<sup>\*</sup> Omitted in mean.

							1				<del></del>
					-		١.	Correc	ctions.		
_		_	Method	Angle of	Tempera- ture.		Intensity.	ļ		Corrected	
Date.	Lat.	Long.	employed.	deflec-	tur tur	Ship's head.	sua	Ship's	Tempe-	Intensity.	Remarks.
				tion.	Te	,	Ħ	attrac-	rature.	intensity.	1
							-	tion.			***
1845.											
Ap. 28.	97 35	106 32	Def. N.	33 36	<b>7</b> 5	n. by w.	1.467	+.002	001	1.468	
лр. ≈о.	-21 00	100 52	Def. S.	37 36	76	n. by w.	1.532	+.002	-·001	1.533	
			Def. N.S	53 30	76	n. by w.			006		
							1.483			1.479 >1.478	Unsteady, a heavy swell.
			Mag. N.	34 36	76	n. by w.	1.459		002	1.459	J. Carron
20	25 40		Mag. S.	39 06	76	и. by w.	1.451	1	002	1.451	
29.	-25 46	104 55		33 47	68	N.W.	1.450	003	001	$\binom{1.446}{1.440}$ 1.447	Very unsteady.
	20 40		Def. S.	39 02	68	N.W.	1.453	1	001	1.449	
May 1.	-23 58	99 06		34 30	68	w.	1.414	022	001	1.391	
			Def. S.	39 54	68	w.	1.407		001	1.384 > 1.381	Unsteady.
			Def. N.S.	55 14	68	w.	1.394	022	003	1·369 J	
2.	-24 01	97 25	Def. N.	34 32	72	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.412	019	001	1.392]	
			Def. S.	40 02	72	$W \cdot \frac{1}{2} N \cdot$	1.402	019	001	1.382 > 1.381	Unsteady.
			Def. N.S.	55 15	72	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	1.394	019	005	1.370	
3.	-23 50	95 56	Def. N.	35 00	76	$W_{\bullet} = \frac{1}{2} N_{\bullet}$	1.388	019	001	1.368	1
			Def. S.	40 16	76	w. ½ N.	1.389	1	001	1.369	
			Def. N.S.	55 38	76	$W_{\cdot} \frac{1}{2} N_{\cdot}$	1.378	019	006	1.353	1
			wt. 1 gr.	19 28	76	$W \cdot \frac{1}{2} N \cdot$	1.419		+.001	$ 1.401\rangle 1.377$	Steady.
			wt. 1½ gr.	29 58	76	$W_{\cdot} \frac{1}{2} N_{\cdot}$	1.396		+.001	1.378	
			wt. 2 grs.	41 30	76	$W \cdot \frac{1}{3} N \cdot$	1.413		+.001	1.395	1
4.	-24 16	93 48		35 21	76	w.n.w.	1.371	010	001	1.360	April 1985 April 1985
	~ 1 10	30 10	Def. S.	41 05	76	w.n.w.	1.350	-010	<b></b> 001	1.339 >1.352	Unsteady.
		1	Def. N.S.	55 45	76	W.N.W.	1.369			1.358	Chsicady.
5.	-24 02	92 07	Def. N.	35 51	73		1.347	}	-·001	1.0545	
J.	& T U &	32 01	Def. N.	40 37	73	N.W.				( \.1•3h7	Cross sea, much
-	01 44	00 90				N.W.	1.373	+.008	001	1.380	rolling motion.
7.	-21 44	89 38	Def. N.	36 30	73		1.316	+.004		1.319	Table unsteady.
			Def. S.	42 13	73	N.W. $\frac{1}{2}$ W.	1.298	+.004		1.301 >1.314	Table unsicady.
	20.00		Def. N.S.	56 45	73	N.W. $\frac{1}{2}$ W.	1.322	+.004		1.321	
8.	-20 38	87 50	Def. N.	36 39	77	N.W. $\frac{1}{2}$ W.	1.309	+.004		1.312	
		1	Def. S.	42 49	77	N.W. $\frac{1}{2}$ W.	1.270	+.004		1.273 >1.298	Unsteady.
. 1			Def. N.S.	56 58	77	N.W. $\frac{1}{2}$ W.	1.312	+.004		1.310	
9.	-20 37	85 02	Def. N.	36 56	77	$W.\frac{1}{2} N.$	1.295	015		1.279	
		1	Def. S.	42 49	77	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.270	015	<b></b> 001	1.254 >1.263	Heavy swell.
		1	Def. N.S.	57 46	77	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.276	<b>015</b>	006	1.255	
10.	-20 25	82 10	Def. N.	37 46	77	$W. \frac{3}{4} N.$	1.260	<b>012</b>	001	1.247	1
			Def. S.	42 48	76	$W. \frac{3}{4} N.$	1.270	012	<b>001</b>	1.257	}
			Def. N.S.	57 46	76	$W_{\bullet} \frac{3}{4} N_{\bullet}$	1.276	012	<b>0</b> 06	1.258 >1.248	Heavy swell.
		1	Mag. N.	38 04	76	$W \cdot \frac{3}{4} N \cdot$	1.256	012		1.243	[
			Mag. S.	42 13	76	$W_{\bullet} \frac{3}{4} N_{\bullet}$	1.249	012		1.236	
11.	-20 36	79 10	Def. N.	39 00	78	$W.\frac{\frac{4}{3}}{4} N.$	1.207	012		1.194	
			Def. S.	43 29	78			012		1.226	1
[			Def. N.S.	58 28	78	4	1.247	012	007	1.228	Unsteady.
1			Mag. S.	42 44	78	$\mathbf{W} \cdot \frac{3}{4}  \mathbf{N} \cdot$	1.220	012	002	1.206	ŀ
12.	-2044	78 31	Def. N.	37 23	87	8.	1.275	040	_ 002	1.233	1
٠	~0 *1	, 0 01	Def. N.	37 12	87		1.283	<b>036</b>	-002	1.245	
			Def. N.	37 12	87		1.282	-·032	002	1.248	1
			Def. N.	38 13	87			032	002		
l			Def. N.	38 28	87		1.241	-·016		1.216	
							1.229			1.211	These observations were made to de-
l		1	Def. N.	38 27	87		1.230	007	002	1.221 1.234	termine the effec
			Def. N.	37 47	86		1.258	<b></b> ·001	002	1.252	of the ship's iron at sea.
			Def. N.	38 14	84		1.240	.000	002	1.238	at sca.
		1	Def. N.	38 11	80	- 1	1.242	+.002	001	1.243	
		.	Def. N.	38 28	78		1.229	.000	001	1.228	
-			Def. N.	38 17	78		1.236	001	001	1.234	
			Def. N.	38 00	78	E.N.E.	1.249	<b>007</b>	001	1.241	

											1
					ė			Correc	ctions.		
Date.	Lat.	Long	Method	Angle of	Tempera- ture.		Intensity.		l	Corrected	D
Daw.	Lat.	Long.	employed.	deflec- tion.	em tu	Ship's head.	ten	Ship's attrac-	Tempe-	Intensity.	Remarks.
				<b>v.</b> o	Ĕ		In	tion.	rature.	•	
			**************************************								
1845.	· /			. ,	0		_				
May 13.	-20 39	77 43	Def. N.	37 41	81	S.E.	1.262	032	001	1 - 1	L
			Def. N.	38 00	81	E.	1.249	016	<b></b> ∙001		Made to determine the effect of the
			Def. N.	37 40	81		1.264	001	001	1 51.200	-1-1-1-1-1-1-1
			Def. N.	38 24	80		1.232	+.002	001		A rolling motion
			Def. N.	38 31	79		1.228	001	001	i i	A rolling motion, not very steady at
			Def. N.	38 20	79	1	1.235	016	001	1 2	some points.
16.	-20 26	70 36	Def. N.	38 40	78		1.221	011	001		
			Def. S.	43 52	<b>78</b>	_ •	1.221	011	001		Unsteady.
	00.04	Co. O.	Def. N.S.	59 .26	<b>78</b>		1.214	011	007		
17.	-20 34	69 24	Def. N.	38 37	<b>78</b>		1.222	011	001		
			Def. S. Def. N.S.	43 59	78		1.217	011	001		
				59 09	<b>78</b>		1.222	011	007	1 222	,
	* -		Def. N. Def. S.	38 09		s.w.byw.½w.		030	001		Unsteady.
			Def. N.S.	43 17		s.w.byw. $\frac{1}{2}$ w.		-·030	-·001	1 1	
	1. 2.			58 34		s.w.byw.½w.		030	007 $002$	1 1	
			Mag. N. Mag. S.	38 23 42 07	80	s.w.byw.½w.		030	ı	1 1	
10	<b>—21 11</b>	67 54	Def. N.	38 57	80 76	s.w.byw. $\frac{1}{2}$ w.	1.209	-·030 -·001	-·002 -·001	1 -	
19.	-21 II	0/ 54	Def. S.		76	N.W.		ł.			
			Def. N.S.	44 17	76	N.W.	1.203	-·001	001 $005$	1 1	Unsteady.
ĺ				59 54 38 52	76	N.W.	1·196 1·211	001	-·003	1 - 1	
			Mag. N.		76	N.W.	1.223	-001	+.001	, , , , , , , , , , , , , , , , , , ,	
			wt. 1 gr. wt. $1\frac{1}{2}$ gr.	22 44 35 01	76	N.W.	1.215	<b>-</b> ⋅001	+.001		
			wt. $1\frac{1}{2}$ gr. wt. 2 grs.	51 35	76	N.W.	1.195	001	+.001		Steady.
20.	-21 12	67 00	Def. N.	39 02	74	w. by n.	1.205	-012	-·001		Sucary
20.	-21 12	07 29	Def. S.	44 03	77	w. by N.	1.212	-012	<b>-</b> ⋅001		Unsteady.
			Def. N.S.	59 59	77	w. by N.	1.194	012	004	1 / -	1
21.	-21 01	66 10	Def. N.	39 03	76	w. by N.	1.204	012	001	1. •	
~1.	-21 VI	00 10	Def. S.	44 29	76	w. by N.	1.195	012	001	1	
			Def. N.S.	59 40	76		1.204	-012	005		Unsteady.
			Mag. N.	39 14	76	w. by N.	1.194	012	001	i :	
			Mag. S.	43 48	76	w. by N.	1.163	012	001		
22.	-20 40	62 58	Def. N.	39 28	74	w. by n.	1.189	012	001	ł	-
			Def. S.	45 01	74	w. by N.	1.173	012	001	1.160	malla star la
ŀ			Def. N.S.	59 41	74	w. by N.	1.203	012	005	1.186	Table steady.
			Mag. N.	39 28	74	w. by n.	1.181	012	001	1.168	4 3
27.	-2009	57 31	Def. N.	40 07	77	)	1.165		001	1.164 7	
			Def. S.	45 28	77	[	1.153		001	1	
<u> </u>			Def. N.S.	60 43	77	On share	1.167		006		Steady.
			Mag. N.	39 55	77	On shore	1.158			1.157	
	;		Mag. S.	44 14	77	at Mauritius.	1.138		001		
	:		wt. 1 gr.	23 59	80	indus.	1.163		+.001		
			wt. 1½ gr.*	33 46	80		1.255			1.256* >1.156	Steady.
			wt. 2 grs.	54 42	80	ا ا	1.147		+.001		
30.	-21 50	53 25	Def. N.	39 41	81	s.w. by w.			001	1.154	77
			Def. S.	44 25	81	s.w. by w.			001		Unsteady.
_	- 6		Def. N.S.	59 59	80	s.w. by w.			008	1	
June 3.	-26 26	48 20	Def. N.	39 31	79	n.w. by w.			ł	1.181	77
			Def. S.	45 18	78	n.w. by w.			-·001	1 /	Unsteady.
	a t= - :		Def. N.S.	60 41	78	n.w. by w.			006		
4.	-27 14	45 50	Def. N.	39 44	69	w.	1.179		001	1.100	
			Def. S.	44 39	70	w.	1.188	1	001		Unsteady,
			Def. N.S.	60 38	70	w.	1.169	018	003	1.148	
<b></b>									<u></u>		

<sup>\*</sup> This observation is evidently wrong, and is omitted in the mean.

										·	
					d		٠	Corre	ctions.		
Date.	Lat.	Long.	Method	Angle of deflec-	Tempera- ture.	Ship's head.	Intensity.	Chin's	1	Corrected	Remarks.
Duic.	2200	mong.	employed.	tion.	to to	omp s neua.	ten	Ship's attrac-	Tempe-	Intensity.	
					I		I.	tion.	rature.		1
1845. June 8.	08 r7	3 <sup>°</sup> 7 55	Def. N.	40 36	$\mathring{74}$		1.14#	018	.001	1.128	
anne 2.	-zo 5/	3/ 33	Def. N.	46 11	76	w. w.	1·147 1·124	-·018	1	1.105	
			Def. N.S.	61 44	77	w. w.	1.131	-018	1	1.108 >1.111	Steady
	1		Mag. N.	40 27	77	w.	1.132	-018	001	1	i i i i i i i i i i i i i i i i i i i
			Mag. S.	44 33	77	w.	1.121	018	001	1	
11.	-30 27	33 41	Def. N.	41 32	79	w.n.w.	1.114	008	001	1.105 1.105	Very unsteady.
	-31 06		Def. N.	41 58	79	w. by s. $\frac{1}{2}$ s.	1.098	024		1.073	
			Def. S.	47 30	79	w. by s. $\frac{1}{2}$ s.	1.079	024		1.054 >1.063	3
			Def. N.S.	61 41	79	w. by s. $\frac{1}{2}$ s.	1.131*	024		1.101*	1
17.	-3540	21 40	Def. N.	43 12	62	w. by n.	1.053	013		12.040	Unsteady.
			Def. N.S.	64 49	62	w. by N.	1.038	013		1.023	onsteady.
23.	Simon's		Def. N.	43 22	68	8.	1.047	040	1	1.006	
	Cape of	Good	Def. N.	43 41	67	S.E.	1.036	032	1	1.004	
	Hope.		Def. N.	44 14	67	E.	1.117	016		1.001	
			Def. N.	44 35	67	N.E.	1.004	001		1.003	
			Def. N.	44 40	67	N.	1.001	+.002		1.003	
			Def. N.	44 46	67	N.W.	1.997	001		0.996	
			Def. N.	44 20	70	w.	1.013	-016	1	0.996	
0.4	Ciman'	. Dos	Def. N. Def. N.	43 50	70 68	s.w.	1.032	032		0.999	
24.	Simon's at the I		Def. N.	44 38 50 14	68	FaceEast,	1·004 0·990*			1.003 0.989* \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
	Yard.	DUCK	Def. N.S.	66 16	68	on shore.	1.002			1.000	<b>`</b>
30.	Tara.		Needle N.	45 01	61	K	0.989			0.989	
00.			Needle S.	49 59	62	11	0.996			0.996	<b>'</b>
			Mag. N.S.	66 20	63	On shore.	0.997			0.996	
			Mag. N.	43 45	64	1	0.989			0.989	
			Mag. S.	47 23	64		0.997			0.997	1
July 2.			Needle N.	44 33	61	ħ	1.005			1.005	
, i		,	Needle S.	49 42	62	11	1.005		. 000	1.005	1
ļ			Needle N.S.		63	11	0.998		-001	0.997	
			Mag. N.	43 15	63	On shore.	1.006		,	1.006	1
•			Mag. S.	47 20	64		0.999			0.999	
1			wt. 1 gr.	28 26	56	11	0.993			0.993 >1.000	)
			wt. $1\frac{1}{2}$ gr.	44 16	57		0.999			0.999	1
١,,	Magnet	in Oh	wt. 2 grs.	69 15	58	K	1.001			1.001	1
ļ ,1.	Magnet servator		Def. N. Def. S.	$\begin{vmatrix} 44 & 31 \\ 49 & 48 \end{vmatrix}$	75 75	11	1·006 1·002		1	1.005	
	servator of Good		Mag. N.S.	66 02	75	1.1	1.002			1·001 0·999	
	or Good	Trobe.	Mag. N.S.	43 21	76	11_	1.003			1.001	
l			Mag. S.	47 13	76	On shore.	1.002		3	1.001	1
			wt. 1 gr.	28 00	76	11	1.007		+.001		1
			wt. 1½ gr.	44 10	76	11	1.001		1+.001	1.002	•
		4	wt. 2 grs.	69 31	76	11	0.999			1.000	
	l					۲ .	000	1	1'	[	

<sup>\*</sup> Not included in mean.

Observations of the Magnetic Force made on board Her Majesty's hired Bark "Pagoda," from the 1st of December 1844 to the 2nd of July 1845. Needle 1. Fox No. 1.; Face West; time usually two hours before Noon.

Observer, Lieut. H. CLERK, R.A.

		. ,		A	1 :		*	Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo meter.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1844. Dec. 1.	—33° 56	18 29		39° 06	$6\mathring{s}$	<u> </u>	1.006		•000	ł - · · ł	
			Def. N.S.	40 38 59 23	67 68		1·001 0·981		-·001	0.980	
	3.5		wt. 2 grs.	21 29 46 54	70 71		1·009 0·995		+.001	0.996	
5.	Magnet servator			65 22 39 01	72 72	Observed on shore.			+·001 -·001	$\begin{vmatrix} 1.001 \\ 1.007 \end{vmatrix}$ 0.999	
	of Good		Def. S.	40 37 59 22	72 73		1·001 0·983	•••••	-·001 -·003		
			wt. 1 gr.	21 34	74		1.006		+.001	1.007	
			wt. 2 grs. wt. $2\frac{1}{2}$ grs.	46 33 65 19	74 74		1.001 1.001		+.001	1.002	
21.	-34 12	18 26	Def. N.	39 04 40 25	74 76	Ĭ	1.007 1.007		-·001	1.006	
•	Dock	Yard.	Def. N.S.	59 11	78	Observed	0.998		004	0.984	
	Simon'			21 04 46 30	78 78	on shore.	1.029		+.001	1.030	
1845.			wt. $2\frac{1}{2}$ grs.	65 49	78	J .	0.997		+.001	0.908	
	-34 44	17 50		39 42 40 39	70 70	w. by n. w. by n.	0.986 1.000	-·009		0.976	Table unsteady.
	0		Def. N.S.	59 11	70	w. by N.	0.988	009	002	0.977	Table unsteady.
13.	<b>-35</b> 12	13 28	Def. N. Def. S.	40 02 40 40	72 72		0·976 0·999	-·030	-·001	0.945	
				59 25 22 00	75 70	s.w. $\frac{1}{2}$ w. s.w. $\frac{1}{2}$ w.	0.980 0.987	-·040 -·040	+·001	$\begin{vmatrix} 0.937 \\ 0.948 \end{vmatrix} > 0.950$	Table steady.
			wt. 2 grs.	47 02	69	s.w. $\frac{1}{2}$ w.	0.992	040	+.001	0.953	
14.	_37 25	13 24	wt. $2\frac{1}{2}$ grs. Def. N.	57 01 38 52	68 65	s.w. $\frac{1}{2}$ w. s. by w.	0.987 1.013	-·040 -·042	+.001	0.9717	
			Def. S. Def. N.S.	40 22 58 50	65 65	s. by w.	1.009	-·042 -·042	001	0.967 >0.965	Table unsteady.
15.	-38 37	14 27	Def. N.	38 55	62	N.W. by W.	1.012	+.003	.000	1.015	
			Def. N.S.	39 55 59 25	62 66	n.w. by w.	0.980	+.003	001	0.982	Very unsteady.
16.	<b>-39</b> 10	14 41	Def. N. Def. S.	38 47 39 35	63	s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.	1.016 1.034	-·026	·000	- 00 - 1	
			Def. N.S.	58 30	63	s.w.byw.1w.	1.009	-·026	·001 •000	0.982	Table steady.
			wt. 2 grs.	21 32 45 22	65	s.w.byw. $\frac{1}{2}$ w.s.w.byw. $\frac{1}{2}$ w.	1.021	026	•000	0.995	
17.	-40 21	14 29	wt. $2\frac{1}{2}$ grs. Def. N.	64 42 38 42	67 64	s.w.byw. $\frac{1}{2}$ w.s.w. by w.		·026 ·029	.000	0·979	
·			Def. S.	39 25 58 27	65 65		1.039	029	-000 -001	1.010 >0.994	Much motion.
18.	-42 50	13 00	Def. N.	38 32	60	s.s.w.	1.025	040	•000	0.985う	
			Def. N.S.	38 35 58 07	59 58	s.s.w. s.s.w.	1·066 1·021	040	•000	0.981	Much motion.
19.	-44 50	13 19	Def. N.	38 17 39 02	48 45		1·033 1·051	-·037 -·037	+.001		Much motion.
				57 27	44	s.w. by s.	1.044	_·037	+.003	1.010	M acu motou.

			·		٨.			Correc	tions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermon meter	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.	. ,	0 /		Q /	. 0	_		_			
Jan. 21.		12 25	Def. N.	36 30	$egin{array}{c} 43 \ 48 \ \end{array}$		1.091		+.001	1.051 1.051	Very unsteady.
22.	<b>-48 35</b>	10 51	Def. N. Def. S.	36 15 37 35	48		1·101 1·104	1	+.001		Table steady.
			Def. N.S.	56 28	47	_ •	1.080		+.003		
23.	-50 30	10 25	Def. N.	35 10	43		1.140	1	+.001	1.105	
			Def. S.	36 37	43		1.141		+.001		Table steady.
<b>4</b>		0.00	Def. N.S.	55 47	43		1.105		+.003		
24.	-51 48	9 33	Def. N.	34 47 36 10	48 47	s.w. by w.	1.154		+.001	1.126	Table steady.
			Def. S. Def. N.S.	55 07	47	s.w. by w.	1·158 1·131		+.003	$\begin{vmatrix} 1.130 \\ 1.105 \end{vmatrix}$	Table steady.
25.	-52 53	7 53	Def. N.	34 57	41	s.w. by w.	1.148	1	+.001	1.120	
,,,,,	0.00		Def. S.	35 47	41	s.w. by w.	1.173		+.001		Rather unsteady.
			Def. N.S.	55 17	40	s.w. by w.	1.125		+.004	1.100	
26.	-5352	6 07	Def. N.	34 22	43	w. by s.	1.171		+.001	1.152	
			Def. S.	35 42	43	w. by s.	1.175		+.001	1.156	
			Def. N.S.	$\begin{array}{ccc} 54 & 30 \\ 18 & 12 \end{array}$	42	w. by s.	1·155 1·185		+·003 -·001	$\begin{vmatrix} 1.138 \\ 1.164 \end{vmatrix}$ 1.143	Very steady.
		1	wt. 1 gr. wt. 2 grs.	39 40	40	w. by s. w. by s.	1.138	1	_·001	1.117	
			wt. $2\frac{1}{2}$ grs.	51 50	41	w' by s.	1.155		001	1.134	
27.	-55 08	5 50	Def. N.	33 05	39	s.s.w. $\frac{1}{2}$ w.	1.221	1	+.002	1.185	
	l	1	Def. S.	35 52	38	s.s.w. $\frac{1}{2}$ w.	1.201		+.002	1.165 >1.161	Very unsteady.
	2		Def. N.S.	54 12	37	s.s.w. $\frac{1}{2}$ w.	1.167		+.005	1.134	
30.	$-60 \ 43$	4 00	Def. N.S.	51 57	35	S.	1.262				
			Def. N.S.	51 35	34	s.e. by e.	1.282				Table unsteady.
31.	-61 05	9 03	Def. N.S. Def. N.	$\begin{vmatrix} 52 & 22 \\ 30 & 57 \end{vmatrix}$	34 42	s.e. by s.	1.246		+.002	1.248	
91.	-01 00	9 03	Def. S.	31 55	42	s.E. by s.	1.339		+.002	1.297	
			Def. N.S.	51 22	41	s.E. by s.	1.294		+.005	1.055	
			wt. 1 gr.	16 02	41	s.E. by s.	1.340			1.295	Table steady.
			wt. 2 grs.	32 22	41	s.e. by s.	1.343		001	1.298	
	0- "		wt. $2\frac{1}{2}$ grs.	43 02	41	s.E. by s.	1.332		001	1.287	
Feb. 2	-61 54	16 23	Def. N.	29 57	40	E.S.E.	1.368	-032	+.003		70.11
			Def. S. Def. N.S.	30 57 50 45	39	E.S.E.	1.384 $ 1.325$		+·006 +·003		Table unsteady.
3	-61 50	19 13		30 10	41	E.S.E.	1.348		+ 000	1.299 ]	
0.	01 00	, 13 10	Def. S.	31 20	41	E.S.E.	1.366		+.002	1.336	
			Def. N.S.	50 20		E.S.E.	1.346		+.006	1.390	XX
	1		wt. 1 gr.	15 05	38	E.S.E.	1.420	1		1.380	Very steady.
			wt. 2 grs.	31 55	38	E.S.E.	1.376		1		
,	CO 04	00 25	wt. $2\frac{1}{2}$ grs.	42 57		E.S.E.	1.336	-032	+.002	1.302	
4	-62 00	20 25	Def. N. Def. S.	29 30 30 37		S.S.E.	1.388	-046	+.003	$\begin{vmatrix} 1.345 \\ 1.358 \end{vmatrix}$ 1.353	Very steady.
			Def. N.S.	49 27		S.S.E. S.S.E.	1.396	046	+.006	1.356	very steady.
6	64 20	0 24 05		28 00		S.S.E.	1.461		+.003		-
			Def. S.	29 57		S.S.E.	1.435		+.003		
			Def. N.S.	49 02		S.S.E.	1.422	1			Very steady.
			wt. 1 gr.	14 17		S.S.E.	1.499		1	1.447	very steady.
		1	wt. 2 grs.	30 00		S.S.E.	1.454	1			
7	65 2	4 28 30	wt. $2\frac{1}{2}$ grs. Def. N.	39 40		S.S.E. 1/2 E.	1.425	1		1	
1 '		. 20 00	Def. S.	28 5		S.S.E. $\frac{1}{2}$ E.	1.486		1		Very steady.
1			Def. N.S.	48 12		S.S.E. <sup>1</sup> / <sub>2</sub> E.	1.466		1 '		,,
9	$-66 \ 3$	0 36 46	Def. N.	26 59	34	E.	1.519	-026	+.004	1.497	
	1	1	Def. S.	28 3	33	E.	1.506		+.004	1.484 >1.482	Very steady.
1		0 00 15	Def. N.S.	48 00		Е.	1.483				
10	-06 4	3 38 49		26 13		s.s.w.	1.553				Vous et 3
1 .	1		Def. S. Def. N.S.	28 00 47 30		S.S.W.	1.538	050	+.004		very steady.
	1		Del. N.S.	1 */ 3	1 34	s.s.w.	1 310	000	T 007	1 110 )	

					١.		ķ	Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo- meter.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.		. ,		. ,		distribution of the second					
Feb. 11.	-67 35	39 31		26 35	33		1.534		+.004		-
			Def. S.	27 55	32	N.E.	1.544	016	+.004	1.532 >1.519	Very unsteady.
10	-66 45	20 02	Def. N.S. Def. N.	47 35 26 12	31	N.E. S.S.E.	1.510 1.556		+·008 +·003		
1 %.	00 40	39 23	Def. S.	28 17	37 37	S.S.E.	1.522	049	+.003		Very unsteady.
	*		Def. N.S.	47 12	37	S.S.E.	1.537	049			,
13.	-6700	40 07		26 22	37	E.N.E.	1.547	025	+.003	1.525	12 m
			Def. S.	28 10	36	E.N.E.	1.529	025	+.003		
			Def. N.S.	47 42	35	E.N.E.	1.504	025	+.007		Table steady.
			wt. 1 gr.	14 00	32	E.N.E.	1.529	025	002	1.90%	Table steady.
			wt. 2 grs.	28 17	32	E.N.E.	1.534		002		
16	-64 52	90 97	wt. $2\frac{1}{2}$ grs. Def. N.	37 27	32	E.N.E.	1.496		002	• •	
10.	-04 52	38 37	Def. N.	27 10 28 02	37 37	S. $\frac{3}{4}$ E. S. $\frac{3}{4}$ E.	1.504 1.536	4	+.003		Very unsteady.
17.	-64 52	40 12	Def. N.	27 34	38	N. by w.	1.488		+.003		
-,-	01 02	10 12	Def. S.	29 12	38	N. by w.	1.473		+.003		Very unsteady.
			Def. N.S.	48 10	38	N. by w.	1.473		+.006		
18.	-64 22	40 49		26 52	38	s. by E.	1.519		+.003	1.460 7	***************************************
			Def. S.	28 42	37	s. by E.	1.500	-053	+.003	1.490	Very unsteady.
19.	-6349	42 00	Def. N.	28 35	39	E. by s.	1.431		+.003		
			Def. S.	29 47	37	E. by s.	1.443	1	+.003		Very unsteady.
20	CO 00	1	Def. N.S.	48 15	36	E. by s.	1.468		+.006		·
20.	-63 22	45 35	Def. S. Def. N.S.	29 02	44	s.e. by e. ½ e. s.e. by e. ½ e.	1.48%	-·049 -·049	+.002		Very unsteady.
21.	-63 36	46 41		48 00 27 00	45 42	S.E. Dy E. 2 E. S.S.E.	1.512	049	+.005  +.002	1	
. ~1.	-05 50	40 41	Def. S.	28 37	41	S.S.E.	1.505				Table unsteady.
ŀ			Def. N.S.	47 52	41	s.s.e.	1.491	1	+.006		l word ansieury.
24.	-62 36	51 40		47 54	36	E.	1.490		+.007		
		İ	Def. N.	26 45	36	E.	1.526	-031	+.003	1.498 >1.466	Very unsteady.
			Def. S.	29 27	34	Е.	1.460		+.004		
25.	-61 25	53 38		27 05	40	E.S.E.	1.507	1 -	+.003		
			Def. S.	28 32	39	E.S.E.	1.510		+.003		Unsteady.
00	C		Def. N.S.	47 30	38	E.S.E.	1.516	039	+.006	1.483	
26.	-61 17	57 28		25 30	41 42	S.E. ½ E.	1.595 1.566		+·002 +·002		Table unsteady.
İ			Def. S. Def. N.S.	27 30 46 45	44	S.E. $\frac{1}{2}$ E. S.E. $\frac{1}{2}$ E.	1.567		+.002		Table unsteady.
27.	_61 00	64 03		25 17	37	S.E. $\frac{1}{2}$ S.	1.607		+.003		
l ~''		1 - 30	Def. S.	26 30	36	S.E. $\frac{1}{2}$ S.	1.622				Table steady.
			Def. N.S.	46 47	35	S.E. $\frac{1}{2}$ S.	1.564	050	+.008	1.522	
28	$-61 \ 36$	6 70 46	Def. N.	24 22	40	s.s.E.	1.660	-052	+.003	1.611 5	
	1	l	Def. S.	25 57	39	S.S.E.		-052	+.003	1.605 >1.604	Table unsteady.
l.,	0-		Def. N.S.	45 42	38	S.S.E.	1.640	052	+.007	1.595	
Mar. 1.	-62 10	72 25		23 10		S.S.E.	1.731	-:052	+.002	1.681	
			Def. S.	25 37	1	S.S.E.	1.705	052	+.002	1.624	
			Def. N.S.	44 50 11 37	44	S.S.E.	1.705 1.837			1.784*	Table steady.
1	1		wt. 1 gr. wt. 2 grs.	25 00	43	S.S.E. S.S.E.	1.719				ł
1		1	wt. $2\frac{1}{2}$ grs.	32 12		S.S.E.	1.708				
2	-62 40	76 09	Def. N.	23 50		s.	1.693				
1 ~	1	1	Def. S.	25 10		s.	1.699	056	+.002	1.645	
	ŀ		Def. N.S.	44 45	41	s.	1.710	-056	+.006	1.660 1.656	Very steady.
1		1	wt. 1 gr.	11 35		s.	1.838			11./81* (	, cry steady.
1	1		wt. 2 grs.	24 47		s.	1.733		001		
	i	ì	wt. $2\frac{1}{2}$ grs.	32 00	39	s.	1.718	056	J·001	1.661	i

<sup>\*</sup> Not included in the mean; angle of deflection become too small.

					١.	:		Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo- meter.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.	0 /	0 /		0 (					4		
Mar. 3.	-64 20	79 38	Def. N.	22° 38	33	s. by w. $\frac{1}{2}$ w.	1.763	055	+.004	1.712	
		. *	Def. S.	24 17		s. by w. $\frac{1}{2}$ w.				1 - 1	Table unsteady,
=	61 90	04:40	Def. N.S.	44 12	32	s. by w. $\frac{1}{2}$ w.			+.009		
<b>ə.</b>	-61 38	84 40	Def. N. Def. S.	23 02	39	S.E.	1.740		+.003		Table unsteady.
			Def. N.S.	24 20 44 40	40 41	S.E.	1.752 1.716	051	+.007		Table unsteady.
6.	-6042	88 12		22 40	36		1.761	025	+.004	1.740	
-	00 20	00 12	Def. S.	23 55	36	$N.E. \frac{1}{2} N.$	1.780		+.004		Table unsteady.
			Def. N.S.	44 50	35	N.E. $\frac{1}{2}$ N.	1.705		+.008		
7.	-61 20	91 09		22 02	40	s. by E.	1.800	-055	+.003	1.748	
-			Def. S.	23 05	41	s. by E.	1.831		+.003		
	00		Def. N.S.	43 30	42	s. by E.	1.805		+.007		,
	-61 26	91 20		22 00	40	s.w. by s.	1.801		+.004		Table unsteady.
			Def. S. Def. N.S.	23 22	40	s.w. by s.	1.812		+.004		Table unsteady.
8	-61 14	00 03		43 37	39	s.w. by s.	1.800 1.795		+·008 +·004		
0.	01 14	92 03	Def. S.	22 05 23 37	39 38	E.		042			
			Def. N.S.	43 32	37	E.	1.804		+.008	11.770	
			wt. 1 gr.	11 17	36	E.	1.890			1.843* >1.762	Table steady.
			wt. 2 grs.	23 50	35	E.	1.801	•		1.754*	
			wt. $2\frac{1}{2}$ grs.	29 05	34	E.		045		1.823*	
9.	-60 35	92 25	Def. N.	22 17	41	Е.		045			
			Def. S.	23 55	37	E.	1.780	-045	+.004		Table unsteady.
10	CO 00	05 00	Def. N.S.	43 40	38	E.	1.791		+.008		
10.	-60 03	95 36	Def. N. Def. S.	20 57	36	S.E. $\frac{1}{2}$ S.	1.867		+.004		Very unsteady.
11	-59 52	00 30		23 07 21 05	36 38	S.E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S.	1.831 1.810		+.004   +.004		·
	-09 52	99 50	Def. S.	22 57	37	E. ½ S.	1.839		+.004		Very unsteady.
			Def. N.S.	43 45	36	$E. \frac{1}{2} S.$	1.785		+.009		t ory unisonary.
	-5959	99 39		21 42	40	E. $\frac{1}{2}$ N.	1.820	042	+.004	1.782	ļ
			Def. S.	23 32	40	E. $\frac{1}{2}$ N.	1.804	042	+.004	1.766	
			Def. N.S.	43 25	39	E. $\frac{1}{2}$ N.	1:813	042	+.008	1.779 \ 1.773	Table unsteady
			wt. 1 gr.	11 20	35	$E \cdot \frac{1}{2} N \cdot$	1.884	-042	003	1.839*	5 P.M.
			wt. 2 grs.	23 42	35	$E \cdot \frac{1}{2} N \cdot$		042			
- 19	F# 0F	00 00	wt. $2\frac{1}{2}$ grs.	30 02	34	$E \cdot \frac{1}{2} N \cdot$	1.820				
	$-57  35 \\ -56  53$			41 05	35	E. by s.	2.006 1.848		+·009		Very unsteady 6 P.M
17.	-30 33	101 24	Def. S.	$\begin{vmatrix} 21 & 15 \\ 22 & 57 \end{vmatrix}$	41	E. by s.	1.839	-047	+.003	1.705 1.786	Very unsteady.
			Def. N.S.	43 35	40	E. by s.		047			l ory unsocurey.
15.	-55 52	103 06	Def. N.	21 15		E. by N.	1.848	042	+.004	1.810	
			Def. S.	22 35	39	E. by N.	1.864	-042	+.004	1.826 1.816	Very unsteady.
			Def. N.S.	43 00	38	E. by N.	1.845	042	+.008	1.811	
16.	-54 48	106 04		21 30	40	N.E.	1.832	036	+.004	1.800 7	
			Def. S.	22 52	40	N.E.	1	036			Very unsteady.
1.77		100 05	Def. N.S.	43 20	39	N.E.	1.819		+.008		1
17.	-54 17	108 05		20 20	41	S.E.	1.912		+.004	1	
			Def. S. Def. N.	22 22 21 35	41 40	S.E.	1.878 1.826		$ +.004 \\ +.004$		Very unsteady, ship pitching heavily.
,*			Def. N.	23 10	40	E. E.	1.830		+.004		Procuing meavity.
18.	-53 00	110 08		21 37	40	N.N.E. 1/2 E.	1.825		+.004		
	30,00	1	Def. S.	22 40	40	N.N.E. $\frac{1}{2}$ E.	1.858		+.004		Very unsteady, a
			Def. N.S.	42 57	39	N.N.E. 1/2 E.	1.846	034	+.008	1.820	heavy swell.
19.	-51 20	111 23	Def. S.	23 20	41	N.N.E. $\frac{1}{2}$ E.	1.816	-034	+.004	1.786 7 1.787	Very unsteady, a
	,		Def. N.S.	43 22	41	N.N.E. $\frac{1}{2}$ E.					heavy swell.

<sup>\*</sup> Not included in the mean.

				Angle of	٠. ا		ty.	Corre	ctions.			
Date.	Lat.	Long.	Method employed.	deflec-	Thermo- meter.	Ship's head.	Intensity.	Ship's attraction.	Tempe- rature.	Corrected Intensity		Remarks.
1845.												
Mar. 20.	$-4\mathring{9}$ 01	111° 47	Def. N.	21° 20	45	n.e. by n.	1.843	027	+.003	1.819		
			Def. S.	23 32	45	N.E. by N.	1.805	027		1.781		
			Def. N.S.	43 15	45	N.E. by N.	1.825	-027	+.006		708	Table unsteady,
			wt. 1 gr.	11 10	44	N.E. by N.	1.911	027	002	1.9921	150	swell from west.
				23 32	44	N.E. by N.	1.823	027	002	1.794		
00	47 01	115 15		$\begin{vmatrix} 30 & 02 \\ 21 & 05 \end{vmatrix}$	45	N.E. by N.	1.820	027	$002 \\ +.002$	1.791		·
22.	-4/ %1	113 13		$     \begin{array}{c cccc}     21 & 05 \\     22 & 10     \end{array} $	49 49	E.N.E.	1.857 1.892	-·035 -·035	+.002		205	Steady, light swell
		6		43 20	48	E.N.E.	1.821	-·035	+.002		020	from west.
25.	-43 20	116 52		23 27*	51	$N \cdot \frac{1}{2} E$ .	1.712			1.689		
	10 ,00			23 35	51		1.799	1 1	+.002			
				43 45	51	$N \cdot \frac{1}{2} E.$	1.785		+.003	1.469	760	Vormunstandy hasyn
			wt. 1 gr.	12 07	<b>50</b>		1.764	025	<b></b> ∙001	1.738	700	Very unsteady, heavy swell from west.
			wt. 2 grs.	23 32	<b>50</b>		1.823	-025	001	1.797		
			wt. $2\frac{1}{2}$ grs.	31 17	<b>50</b>	$N_{\cdot} \frac{1}{2} E_{\cdot}$	1.752	025		1.726		
26.	-41 18	116 09		22 30	54	N. by w.	1.771	020	+.001			
				23 57	54	N. by w.	1.776	020	+.001	1.757	746	Unsteady, light swell.
27.	-38 52	116 15		$\begin{vmatrix} 44 & 15 \\ 22 & 37 \end{vmatrix}$	54 58	n. by w. n. by w.	1·747 1·765	020 012	+.002	1.753		
21.	-30 32	110 15		23 52	58	n. by w.	1.770	-012			738	Table steady.
				44 40	60		1.716	012		1.704	,00	Table Sacady.
28.	-37 03	116 57		23 25	59	N. by E.	1.718	012		1.706		
		1		24 45	60	n. by E.	1.725	012		1.713		
				44 30	61	n. by E.	1.728	-012		1.716	605	Table very steady,
		1		12 45	62		1.678	012		1.000	095	nearly a calm.
		l		25 40	62		1.678	012		1.666		
	26.70			32 07	63		1.714	012		1.702		
29.	-36 12	116 50		23 40	66	i e	1.701	012	-·001	1.688	CM9	Table unates du
				25 37 45 05	$\frac{67}{68}$	N.N.E.	1.673 1.685	-·012	<b>-</b> ⋅001		0/3	Table unsteady.
30	-35 18	117 07		23 22	66		1.719	-·012	001			
	00 10	, 0,		24 45	66		1.725	-·012	001		702	Table unsteady.
				44 52	66		1.701	012	002			,
April 7.	-3502	117 56		23 50	68		1.692		001			
		1	Def. S.	25 18	68		1.692		001			
		1		45 06	69		1.685		001			
		1		12 22	69		1.726		001		1	
			wt. 2 grs.	25 24	69		1.695	• • • • • • • • • • • • • • • • • • • •	001		-	
	King G	oorgo'a		32 52 23 42	68	Observed on shore.			001  002		688	The observations were made on the
11.	Sound,	West		23 42 25 12	82 82	on shore.	1.700	•••••	002			same spot where
	Austral			44 59	83		1.692	•••••	005		. ]	Captains FLIN- DERS and FITZ-
Section 2	11 (15)	114.		12 37	84		1.692	••••	+.001		I	ROY had pre- viously observed.
		- 1		25 30	84		1.689		+.001	1.690	.	. LOUDLY ODDOLYOU.
			wt. $2\frac{1}{2}$ grs.	33 01	85		1.670		+.002	1.672	1	
19.			Def. N.S.	44 09	54	s.s.w.	1.754	056	+.001	1.699 ≒		
		Sound.		44 20	54		1.740	051	+.001	1.690		
	Swing	ing the		44 30	54		1.728	041	+.001	1.670		
		or local		44 44	54		1.710	032	+.001	1.691	ĺ	
	attract	11011.		44 50	54 54		1·702 1·687		+.001			
		]		$\begin{array}{c c} 45 & 04 \\ 45 & 01 \end{array}$	54 54		1.691	-012	+.001	1.680	1	
				44 59	57		1.692	012	+.001	1.681		The table was very
		.		45 03	58		1.688	012	.000	1.676	683	steady during
										· /-	1	these observations.

<sup>\*</sup> The degree should probably be 22°; not included.

<sup>†</sup> Not included in the mean.

								Corre	ctions.	1	
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo- meter.	Ship's head.	Intensity.	Ship's attrac-	Tempe-	Corrected Intensity.	Remarks.
				6011.	E T		H	tion.	rature.		
1845.			·								
Apr. 19.	Swinging	ng the	Def. N.S.	45° 01	5 <b>9</b>	N.E.	1.691	012	-000	1.679 >1.683	
	ship for		Def. N.S.	44 49	60	E.N.E.	1.702	022	.000	1.680	N.S. on shore
	attrac	tion.	Def. N.S.	44 47	60	E.	1.705	032	.000	1.673	
		1 1	Def. N.S.	44 33	63	E.S.E.	1.723	041	001	1.681	
			Def. N.S.	44 20	63	S.E.	1.740	051	001	1.688	
			Def. N.S. Def. N.S.	44 14	63	S.S.E.	1.748	-·056 -·061	-·001	1.691	
23.	-35 36	114 44		44 11 23 57	63	s. n.w.	1.751 1.686	-012	.000	1.674	1
.00	00 00	114 44	Def. S.	24 47	64		1.722	-012	•000	1.710 >1.688	
			Def. N.S.	45 00	64	N.W.	1.692	-012	001	1.679	Table unsteady.
24.	<b>-34</b> 16	113 01	Def. N.	24 40	67	n.w. by n.		012	001	1.6307	
			Def. S.	25 37	69	N.W. by N.		012	001	1.661 >1.641	Table unsteady.
			Def. N.S.	45 37	70	n.w. by n.		012	002	1.633	amoready.
25.	-32 32	111 36	Def. N.	25 02	67	N.w. by N.		008	001	1.614	
			Def. S.	26 17	69	n.w. by n.	1.634	008	-001	1.625 >1.613	Table unsteady.
			Def. N.S.	46 05	70	N.W. by N.		008	003	1.601	
27.	-29 20	106 55		25 07	72	w.n.w.	1.619	016	-002	1.601	
			Def. S.	27 32	72	w.n.w.	1.566	<b> </b> −·016	002		Table steady.
			Def. N.S.	47 15	72	w.n.w.	1.531	<b> </b> −·016	004	1.511	
28.	-2747	106 36	Def. N.	27 17	68	N. by w. $\frac{1}{2}$ w.		.000	001	1.496	
			Def. S.	29 02	69	N. by w. $\frac{1}{2}$ w.		•000	001	1.481 >1.490	Very unsteady, heavy swell.
20	00 00		Def. N.S.	47 47	69	N. by w. ½ w.		.000	003		neavy swem.
29.	-26 00	105 11	Def. N.	27 30	72	N.W.	1.486	005	001	1.480	
			Def. S.	29 10	74	N.W.	1.474	-005	001	1.468 >1.470	Very unsteady, heavy swell.
Mor. 1	04.00	00 00	Def. N.S. Def. N.	48 12	75	N.W.	1.471	005	-·004 -·001		menty swell.
may 1.	-24 00	99 23	Def. N.	29 07 31 00	69 69	w. w.	1·396 1·381	-·021 -·021	001	$\begin{vmatrix} 1.374 \\ 1.359 \end{vmatrix}$ $\begin{vmatrix} 1.367 \end{vmatrix}$	
		1	Def. N.S.	49 30	70	w.	1.393	021	003	1.369	Very unsteady, much motion.
2.	-24 01	97 30		29 02	70	$w.\frac{1}{2} N.$	1.410	017	001	1.3927	
	W 1 0 1	3, 00	Def. S.	30 50	71	$W \cdot \frac{1}{2} N$	1.390	017	001	1.372 >1.379	Table -4 1- 17/41
			Def. N.S.	49 32	71	$W. \frac{1}{2} N.$	1.392	017	003		Table steady, little motion.
3.	-24 00	96 06		29 40	76	$W \cdot \frac{1}{2} N$ .	1.381	017	001	1.363	
			Def. S.	31 02	76	$W \cdot \frac{1}{2} N$ .	1.380	017	001	1.362	
			Def. N.S.	50 15	77	$w. \frac{1}{2} N.$	1.350	017	004	1.329	
			wt. 1 gr.	15 02	77	$W \cdot \frac{1}{2} N \cdot$	1.423	017	+.001	1.407	Table steady, no
			wt. 2 grs.	31 47	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.380	017		1.364	2
_			wt. $2\frac{1}{2}$ grs.	41 10	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.383	017	1 '	1.367	-
6.	-2247	91 00		30 57	76	N.W.	1.320	+.008		1.327	
			Def. S.	32 25	79	N.W.		+.008			Very unsteady, heavy westerly
_		00 44	Def. N.S.	60 50	80	N.W.		+.008			swell.
7.	-21 50	89 44	Def. N.	30 45	72	N.W.		+.008			
			Def. S. Def. N.S.	32 15	74	N.W.	1.322	1 .	001	1.329 >1.326	<b>'</b>
8.	90 46	87 59		51 10 31 45	75	N.W.	1.308			1 -	
0.	-20 40	01 39	Def. S.	32 20	75   76	N.w. by w.				1.282	
			Def. N.S.	51 25	77	N.w. by w.	1.318			1.321	
			Def. N.S.	32 00	78	N.w. by w.				$\begin{vmatrix} 1.292 \\ 1.270 \end{vmatrix}$ 1.294	W. Burdon, Esq
	1		Def. S.	32 37	77	N.W. by W.				1.309	R.N., observer.
	•	1	Def. N.S.	51 27	77	N.W. by W.		+.004			
9.	-20 38	85 26		31 42	77	$W \cdot \frac{1}{2} N$	1.286			1.271	
		-5 20	Def. S.	33 02	77	$W \cdot \frac{1}{2} N$	1.286			1.271 >1.268	Very unsteady.
		1	Def. N.S.	51 50	77	$W \cdot \frac{1}{2} N$	1.270				heavy swell.
	<u> </u>	1				1 2				<u>                                     </u>	1

								l a			T
1				Amala af	٨.		4.	Correc	ctions.		
Date.	Lat.	Long.	Method	Angle of deflec-	Thermo- meter.	Ship's head.	Intensity.	Ship's		Corrected	Remarks.
Ducc.	AMI.	Long.	employed.	tion.	he me	omp s nead.	nte.	attrac-	Tempe-	Intensity.	wellarks.
<i>:</i>			:		Ε.		1	tion.	rature.		
3045											
1845. May 10.	-2° 26	82 22	Def. N.	31 37	77̈́	vv. 1 2v	1.288	<b>-</b> ·014	<b></b> ·001	1.273	
May 10.	-20 20	02 22	Def. N.		78	W. $\frac{1}{2}$ N.	1.277	-014	-·001	1.262	
			Def. N.S.	33 15 52 10	80	W. $\frac{1}{2}$ N.	1.260	-014	-·005	1.241	
			Def. N.	31 35	75	$W_{\bullet} \stackrel{1}{\stackrel{1}{2}} N_{\bullet}$	1.289	-014	-·001	$ \frac{1.241}{1.272}\rangle 1.257$	Very unsteady.
			Def. S.	33 27	75 75	W. $\frac{1}{4}$ N.	1.269	-·016	<b></b> 001	1.252	
			Def. N.S.	52 07	74	$W \cdot \frac{1}{4} N \cdot$	1.260	_·016	<b>003</b>	1.241	W. Burdon, Esq., R.N., observer.
11.	<b>-20</b> 36	79 22	Def. N.	31 52	77	W. $\frac{1}{4}$ N. W. $\frac{1}{4}$ N.	1.274	<b>-016</b>	001	1.257	
	~~ ~ 0 0 0 O	13 22	Def. S.	33 37	77		1.262	_·016	001	1.245	W. Burdon, Esq.,
			Def. N.S.	52 07	78		1.260	016	-005	1.230	R.N., observer.
			Def. N.	31 52	78	$\mathbf{W} \cdot \frac{1}{4} \mathbf{N} \cdot \mathbf{W}$	1.274	_·016	002	$ \frac{1.255}{1.256}\rangle^{1.247}$	Table unsteady.
			Def. S.	33 40	77	$W \cdot \frac{1}{4} N$	1.260	016	002	1.242	
			Def. N.S.	52 00	78	$W \cdot \frac{1}{4} N \cdot$	1.262	016	005	1.241	
12.	-2044	78 31	Def. N.S.	52 17	84	w.	1.249	<b>018</b>	006	1.225	
		• 0 0 1	Def. N.S.	52 20	86	w.n.w.	1.248	004	006	1.238	
			Def. N.S.	52 32	88	N.W.	1.239	+.008	006	1.241	
,			Def. N.S.	52 50	91	N.N.W.	1.226	+.006	008	1.224	
ŀ			Def. N.S.	51 20	80	S.	1.296	046	005	1.245 >1.238	Table very unsteady,
			Def. N.S.	51 22	82	s.s.w.	1.294	043	005	1.246	calm.
V			Def. N.S.	51 30	82	s.w.	1.287	037	005	1.245	
			Def. N.S.	51 55	83	w.s.w.	1.267	026	005	1.236	
			Def. N.S.	52 25	82	N.N.E.	1.242	+.006	005	1.243	
13.	-20 39	77 43	Def. N.S.	52 42	77	w.	1.227	018	004	1.205	
			Def. N.S.	52 15	77	N.W.	1.250	+.008	004	1.254	
1			Def. N.S.	52 32	77	N.	1.239	+.008	004	1.243	Very unsteady ;
Ĭ.			Def. N.S.	52 22	77	N.E.	1.247	+.008	004	1.251	calm.
			Def. N.S.	52 07	78	E.	1.260	018	005	1.237	1
l			Def. N.S.	51 45	77	S.E.	1.275	-037	004	1.234	
14.	-20 29	76 22	Def. N.	32 27	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.249	016	001	1.232	
1			Def. S.	33 52	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.252	-016	001	1.235	
			Def. N.S.	52 50	76	W. $\frac{1}{2}$ N.	1.226	-016	004	1.206	Very unsteady.
			Def. N.	33 20	76	$W \cdot \frac{1}{2} N \cdot$	1.212	-016	001	1.195	very unsteady.
			Def. S.	33 37	76	$W_{\bullet} \frac{1}{2} N_{\bullet}$	1.262	-016	001	1.245	W. Burdon, Esq.,
			Def. N.S.	52 30	75	W. $\frac{1}{2}$ N.	1.238	016	004	1	R.N., observer.
16.	-20 28	70 46		32 45	78	W. $\frac{1}{4}$ N.	1.236	1 .	002		
			Def. S.	34 05	78	$W \cdot \frac{1}{4} N \cdot$	1.200	-017	002	1.181 >1.199	Table steady.
	22.00	Con	Def. N.S.	52 55	78	W. $\frac{1}{4}$ N.	1.222	1 -	005	1 . 2	
18.	-21 06	68 12		32 57	80	w.s.w.	1.227	026	002	1.199	
			Def. S.	34 37	80	w.s.w.	1.221	026	002	1.193 >1.191	Very unsteady.
10	01 11	67 54	Def. N.S.	53 10	83	W.S.W.	1.212		-:005	1 2	
19.	-21 11	0/ 04	Def. N. Def. S.	33 12	75	n.w. by n.	1.217	1	1	1.215	
l	1		Def. N.S.	34 45 53 10		N.w. by N.	1.215		-·001 -·004	$egin{array}{ c c c c c c c c c c c c c c c c c c c$	
			wt. 1 gr.	18 00		N.W. by N.	$ 1.212 \\  1.197$				1
1			wt. 2 grs.	37 52		N.W. by N.	1.183		+.001	1.197	Table standy needs
			wt. $2 \text{ grs.}$ wt. $2 \frac{1}{2} \text{ grs.}$	49 32		n.w. by n.	1.196	1	+.001	1.183 >1.203	Table steady, nearly a calm.
1			$\begin{array}{c c} \text{W.} & z_{\overline{2}} \text{ grs.} \\ \text{Def. N.} \end{array}$	33 37			1.202		$\begin{bmatrix}001 \\ +.001 \end{bmatrix}$	1.200	
	1		Def. S.	34 45		N.W. by N.	3	1			
1			Def. N.S.	53 20		N.W. by N.	1.215 1.204	1	-·001 -·004	1.213	W. Burdon, Esq., R.N., observer.
20.	_21 12	67 29	1	33 25		w. by n.	1.204		1	1.1867	1
1 20.	- 21 12	01 29	Def. S.	34 45			1.215			1.201	
1		1	Def. N.S.	53 05		w. by n. w. by n.	1.214			1.106	
	,		Def. N.	33 32		w. by N.	1.205				Table steady.
			Def. S.	34 02		w. by N.	1.243				W. Burdon, Esq.,
1	1	1	Def. N.S.	52 55		w. by N.	1.223				R.N., observer.
l .			= === =:			»,				ر ۵۰۰۰	

Date. Lat.  1845. May 21. —21 02  23. —20 31  27. —20 05 Port L Mauri  30. —21 44  June 2. —26 25	59 42 57 31 ouis, tius.	wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N. Def. S. Def. N.S.	Angle of deflection.  33 40 34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 45 34 58 35 52	76 76 76 76 77 77 78	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1.201 1.216 1.201 1.175 1.191 1.182 1.194	Ship's attraction. 013013013013013013	001 004 +-001 +-001 +-001	1·202 1·184 1·163 1·179 1·170	
1845. — 2î 02 23. — 20 31 ' 27. — 20 05 Port L Mauri 30. — 21 44	66 02 59 42 57 31 ouis, tius.	Def. N. Def. S. Def. N.S. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	deflection.  33 40 34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 77	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1·201 1·216 1·201 1·175 1·191 1·182 1·194	Ship's attraction. 013013013013013013	Temperature. 001001004 +-001 +-001	1.187 1.202 1.184 1.163 1.179 1.170	Remarks.
1845. —21 02  23. —20 31  27. —20 05 Port L Mauri  30. —21 44	66 02 59 42 57 31 ouis, tius.	Def. N. Def. S. Def. N.S. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	deflection.  33 40 34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 77	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1·201 1·216 1·201 1·175 1·191 1·182 1·194		001 001 004 +-001 +-001 +-001	1.187 1.202 1.184 1.163 1.179 1.170	Remarks.
1845. —21 02  23. —20 31  27. —20 05  Port L  Mauri  30. —21 44	59 42 57 31 ouis, tius.	Def. N. Def. S. Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. S. Def. N.S.	33 40 34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 77	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1·201 1·216 1·201 1·175 1·191 1·182 1·194		001 001 004 +-001 +-001 +-001	1·187 1·202 1·184 1·163 1·179 1·170	
23. —20 31  27. —20 05 Port L Mauri  30. —21 44	59 42 57 31 ouis, tius.	Def. S. Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 77	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1·201 1·216 1·201 1·175 1·191 1·182 1·194	013 013 013 013 013	001 001 004 +-001 +-001	1·202 1·184 1·163 1·179 1·170	181 Table steady.
23. —20 31  27. —20 05 Port L Mauri  30. —21 44	59 42 57 31 ouis, tius.	Def. S. Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 78	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1.216 1.201 1.175 1.191 1.182 1.194	013 013 013 013 013	001 004 +-001 +-001 +-001	1·202 1·184 1·163 1·179 1·170	181 Table steady.
23. —20 31  27. —20 05  Port L  Mauri  30. —21 44	59 42 57 31 ouis, tius.	Def. S. Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 78	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1.216 1.201 1.175 1.191 1.182 1.194	013 013 013 013 013	001 004 +-001 +-001 +-001	1·202 1·184 1·163 1·179 1·170	181 Table steady.
23. —20 31  ' 27. —20 05 Port L Mauri 30. —21 44	59 42 57 31 ouis, tius.	Def. S. Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 78	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1.216 1.201 1.175 1.191 1.182 1.194	013 013 013 013 013	001 004 +-001 +-001 +-001	1·202 1·184 1·163 1·179 1·170	181 Table steady.
23. —20 31 ' 27. —20 05 Port L Mauri 30. —21 44	57 31 ouis, tius.	Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	34 40 53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 76 77 77 78	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1.201 1.175 1.191 1.182 1.194	013 013 013 013	004 +-001 +-001 +-001	1·184 1·163 1·179 1·170	181 Table steady.
' 27. —20 05 Port L Mauri 30. —21 44	57 31 ouis, tius.	Def. N.S. wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	53 15 18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 76 77 77 78	w. by n. w. by n. w. by n. w. by n. w. by n. w. by n.	1.201 1.175 1.191 1.182 1.194	013 013 013	+·001 +·001 +·001	1·163 1·179 1·170	Table steady.
' 27. —20 05 Port L Mauri 30. —21 44	57 31 ouis, tius.	wt. 1 gr. wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. N.S. Def. N.S.	18 22 37 37 50 20 33 47 35 30 53 55 34 58	76 76 76 77 77 77	w. by n. w. by n. w. by n. w. by n. w. by n.	1·175 1·191 1·182 1·194	013 013 013	+·001 +·001 +·001	1·163 1·179 1·170	Table steady.
' 27. —20 05 Port L Mauri 30. —21 44	57 31 ouis, tius.	wt. 2 grs. wt. 2½ grs. Def. N. Def. S. Def. N.S. Def. N.S. Def. S. Def. N.S.	37 37 50 20 33 47 35 30 53 55 34 58	76 76 77 77 78	w. by n. w. by n. w. by n. w. by n.	1·191 1·182 1·194	-·013 -·013	+.001	1.179	
' 27.—20 05 Port L Mauri 30.—21 44	57 31 ouis, tius.	wt. $2\frac{1}{2}$ grs. Def. N. Def. S. Def. N.S. Def. N. Def. S. Def. N.S.	50 20 33 47 35 30 53 55 34 58	76 77 77 78	w. by n. w. by n. w. by n.	1·182 1·194	013	+.001	1·170 j	
' 27. —20 05 Port L Mauri 30. —21 44	57 31 ouis, tius.	Def. N. Def. S. Def. N.S. Def. N. Def. S. Def. N.S.	33 47 35 30 53 55 34 58	77 77 78	w. by n. w. by n.	1.194				
' 27.—20 05 Port L Mauri 30.—21 44	57 31 ouis, tius.	Def. S. Def. N.S. Def. N. Def. S. Def. N.S.	35 30 53 55 34 58	77 78	w. by N.		013			
Port L Mauri 30.—21 44	ouis, tius.	Def. N.S. Def. N. Def. S. Def. N.S.	53 55 34 58	78				1.		
Port L Mauri 30.—21 44	ouis, tius.	Def. N. Def. S. Def. N.S.	34 58		1	1.185	3	<b></b> 001·		171 Very unsteady.
Port L Mauri 30.—21 44	ouis, tius.	Def. S. Def. N.S.	, ,	0.3	w. by N.	1.179	013	<b></b> ·004	1.162	
Port L Mauri 30.—21 44	ouis, tius.	Def. S. Def. N.S.	, ,	81	h .	1.147		002	1.145	. [
Mauri 30.—21 44	tius.	Def. N.S.		81		1.170		002	1.168	
30. —21 44			55 32*	81	Observed	1.115		1	) <b>3</b>	156 Lieut. MOORE,
	53 34			81	on shore.	1.135		+.001		R.N., observer.
	53 34	wt. 1 gr.	19 01	1	11		•••••			
	53 34		38 12	81	μ,	1.175		+.001		
June 2. —26 25	00 0-		33 27	80	$w.s.w. \frac{1}{2} w.$	1	•			
June 2. — 26 25	į	Def. S.	34 40	82	$w.s.w. \frac{1}{2} w.$			002	1.193 >1.	179 Very unsteady.
June 2. —26 25		Def. N.S.	53 37	82	$w.s.w. \frac{1}{2} w.$	1.192	024	<b></b> 005	1.163	
	49 12		34 27	79	N.w. by w.	1.168	<b>-</b> ∙005	<b></b> ⋅002		
1 1			35 47	79	N.W. by W.	1.173	005	002		160 Very unsteady.
1 . 1	1		54 22	79	n.w. by w.	1.161	005	004		100 . 0., 0
427 12	16 00		, , , , ,				1	_·001		•
427 12	40 09		34 45	68						
	1		36 20	68			024	<b>-</b> ⋅001		129 Unsteady.
	1		54 30	68		1.155	<b></b> 024	<b></b> ∙001		
528 24	43 00	Def. N.	34 55	74	w.	1.150	020	<b>001</b>	1.129	
		Def. S.	36 30	74	w.	1.145	<b>020</b>	<b>001</b>	1.124	125 Very unsteady.
	1		54 45	76				<b>003</b>		
628 44	49 01		35 47	73				<b>_</b> ∙001		
0, 20 11	-~ 0.		36 55	76	1		<b>-</b> ⋅009	_·001		1177
						1.129				117 Very unsteady.
7 00 00			54 55	78			009	003		
728 35	40 24		34 47	73	W. ½ N.	1.156	<b></b> 017	<b></b> ∙001		1
	1		36 40	74	W. ½ N.	1.138	<b></b> ·017	·001		128 Very unsteady.
. 1		Def. N.S.	54 47	74	W. ½ N.	1.145	<b></b> 017	<b></b> 003	1.125	
828 57	37 52	Def. N.	35 42	72		1.120	<b></b> ∙020	001	1.099	1
	-		37 47	76	1	1.095	-020	001		
	1		55 10	78	1.	1.128	020	004	1.104	
.	l		19 45	80	1	1.100	·020	+.002		094 Table steady, near
· 1	1	wt. 1 gr.								calm.
	-	_ U	40 30	80	, ,	1.118	020	+.002	1-100	
10 -0		40	53 57	82			<b>020</b>	+.002		
1230 33	33 19		36 17	66	w.n.w.	1.098		001		
1 1			37 40	66			<b></b> ·009			085 Table unsteady.
	1	Def. N.S.	56 15	66	w.n.w.	1.086	009	001	1.076	
1331 06	31 34		36 27	65	w. by s. $\frac{1}{2}$ s.		-026	001		
35			37 52	•	w. by s. $\frac{1}{2}$ s.		026	001		061 Table steady.
.   1	1		56 32				026	001		,
14 99 61	ലെ ം				w. by s. $\frac{1}{2}$ s.					
1433 01	2y 30		36 57	71		1.075	020	<b>-</b> ⋅001		
	-		38 35	72		1.067	020	001		046 Table unsteady.
	1	Def. N.S.	56 57	73	w.	1.062	<b>020</b>	<b></b> 003		
1534 31	27 04		36 40	74		1.085	014	001		
			38 42	76			014	001	1.048	
	.		56 47	78	1 = 1	1.067	014	004	1.040 i	
				80						059 Table very unstead
4 1	1		19 47			1.092	014	+ 001	1013	long heavy swell
1 1	. 1		45 02	80	$W_{\bullet} = N_{\bullet}$	1.027	014	+.001	1.014+	
•	- 1	wt. 2½ grs.	58 57	82	W. ½ N.	1.003	014	+.001	1.020	i

<sup>\*</sup> Probably the degree is erroneous; the result is not included in the mean.

<sup>†</sup> Not included.

## Observations of the Magnetic Force. (Continued.)

					1	·	·y.	Correc	ctions.		
Date.	Lat.	Long.	Method employed.	Angle of deflec- tion.	Thermo- meter.	Ship's head.	Intensity.	Ship's attrac- tion.	Tempe- rature.	Corrected Intensity.	Remarks.
1845.				0 /	0						
June 16.	$-3\mathring{5} \ 4\acute{6}$	23 35	Def. N.	38 00	<b>7</b> 5	w. by n.	1.042	012	001	1.029	
			Def. S.	39 17	77	w. by n.	1.043	012	001		Table steady.
		1	Def. N.S.	57 02	78	w. by n.	1.057	012	004	1.041	
17.	$-35 \ 36$	21 40	Def. N.	38 45	67	w.n.w.	1.020	007	001	1.012	
"			Def. S.	39 47	67	w.n.w.	1.026	007	001		Table steady.
			Def. N.S.	57 12	67	W.N.W.	1.053	007	001	1.045	
18.	-35 07	20 46	Def. N.	38 22	64	w. by s.	1.031	019	.000	1.012	
1			Def. S.	39 50	63		1.024	019	.000		Table steady, nearly calm.
	1. 1		Def. N.S.	57 30	63	w. by s.	1.042	019	001	1.022	
23.	-34 12		Def. N.S.	57 01	62	s.	1.060	040	.000	1.020	
	At ancl		Def. N.S.	<b>57</b> 08	66	s.s.w.	1.056	037	-:001	1.018	
	Simon's	Bay.	Def. N.S.	57 29	68	s.w.	1.042	031	001	1.010	
			Def. N.S.	57 52	68	w.s.w.	1.030	022	001	1.007	
		.	Def. N.S.	58 07	70	w.	1.021	014	002	1.005	
			Def. N.S.	58 11	70	W.N.W.	1.019	003	002	1.014	
			Def. N.S.	58 07	82	N.W.	1.020	002	004	1.014	1
i i			Def. N.S.	58 16	82	N.N.W.	1.018	.000	004	1.014	Swinging ship for
			Def. N.S.	58 09	83	N.	1.020	+.002	005	1.017	local attraction.
Sanga.			Def. N.S.	58 10	84	N.N.E.	1.020	.000	005	1.015	
			Def. N.S.	58 09	85	N.E.	1.020	002	005	1.013	
<b>1</b>			Def. N.S.	58 07	85	E.N.E.	1.021	003	005	1.013	
e de la constante de la consta			Def. N.S.	57 58	86	Е.	1.026	014	005	1.007	
			Def. N.S.	57 53	87	E.S.E.	1.030	022	005	1.003	
			Def. N.S.	57 30	88	S.E.	1.042	031	006	1.005	
ı			Def. N.S.	57 10	90	S.S.E.	1.055	037	006	1.012	
			Def. N.S.	58 08	68	On shore.	1.021		001	1.020	In the Dock Yard.
30.	-33 56	18 29	Def. N.	39 31	59	רו	0.992			0.992	
TO THE TOTAL PROPERTY.		-0 23	Def. S.	40 39	61		1.000			1.000	
			Def. N.S.	58 16	62		1.016			1.016	
			wt. 1 gr.	21 38	63		1.004			1.004	
8			wt. 2 grs.	46 31	64		1.001			1.001	
4			wt. $2\frac{1}{2}$ grs.	65 30	65	Observed				0.999 >1.001	
July 2	Magnet	ic Ob-	Def. N.	39 22	59	on shore.	0.997			0.997	
July ~	servator		Def. S.	40 39	60	on shore.	1.000			1.000	
	of Good		Def. N.S.	58 21	61	11 .	1.013			1.013	
The state of the s	01 0000	Tropes	wt. 1 gr.	22 06	63		0.986			0.986	
			wt. 2 grs.	46 21	64		1.004	,		1.004	
				65 30	64	11	0.999			0.999	
			wt. $2\frac{1}{2}$ grs.	00 00	01	۲.	0 333			ر ووو ت	

General Table of the Declinations observed on board Her Majesty's hired Bark "Pagoda."

Date.	Lat.	Long.	No. of observations.	Declination.	Date.	Lat.	Long.	No. of observations.	Declination.
1845. Jan. 10. 11. 12. 13. 15. 16. 17. 19. 20. 22. 23. 24. 25. 26. 27. 29. 31. Feb. 1. 2. 3. 4. 5. 6. 7. 9. 10. 11. 12. 13. 14. 16. 17. 18. 19. 20. 21.	-34 42 -35 26 -35 17 -35 10 -38 43 -39 18 -40 15 -44 45 -46 24 -48 27 -50 45 -51 47 -52 56 -53 52 -55 29 -61 12 -62 03 -61 54 -61 49 -62 05 -63 18 -66 26 -66 55 -67 34 -66 41 -67 06 -67 01 -64 52 -64 52 -64 52 -63 57 -63 37	17 36 15 08 14 00 13 25 14 28 14 28 14 35 13 19 13 34 10 51 10 18 9 34 7 53 6 12 5 54 4 09 9 30 12 45 16 40 19 13 20 58 21 10 25 05 28 33 37 25 38 32 40 03 40 30 38 37 40 49 41 37 45 31 47 01	observations.	+29 51 +28 39 +27 15 +25 40 +25 09 +28 20 +27 40 +26 34 +25 54 +23 55 +23 37 +23 46 +21 34 +21 23 +17 30 +20 29 +22 07 +23 11 +26 16 +28 05 +28 05 +28 56 +30 24 +31 37 +35 39 +37 18 +36 59 +36 38 +36 38 +36 38 +36 38 +37 34 +36 38 +37 34 +36 38 +36 38 +37 34 +36  1845. March 28. 29, 30. 31. April 11. 21. 22. 23. 24. 25. 26. 27. 28. 29, 30. May 1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18.	$ \begin{bmatrix} -36 & 51 \\ -36 & 10 \\ -35 & 12 \\ -35 & 28 \\ -35 & 02 \\ -35 & 10 \\ -35 & 42 \\ -35 & 33 \\ -34 & 18 \\ -32 & 42 \\ -30 & 25 \\ -29 & 20 \\ -27 & 41 \\ -26 & 10 \\ -24 & 07 \\ -23 & 58 \\ -24 & 07 \\ -23 & 56 \\ -24 & 17 \\ -24 & 05 \\ -22 & 56 \\ -22 & 15 \\ -20 & 37 \\ -20 & 36 \\ -20 & 37 \\ -20 & 36 \\ -20 & 34 \\ -20 & 39 \\ -20 & 24 \\ -20 & 39 \\ -20 & 24 \\ -20 & 39 \\ -20 & 24 \\ -20 & 34 \\ -20 & 34 \\ -20 & 34 \\ -20 & 34 \\ -20 & 34 \\ -20 & 34 \\ -20 & 34 \\ -21 & 11 \\ -21 & 12 \\ \end{bmatrix} $	116 36 116 43 117 41 117 04 117 56 118 06 115 40 114 42 113 12 111 43 109 07 106 55 106 35 105 16 102 28 99 21 97 34 95 46 92 11 90 40 89 42 88 06 85 32 79 20 78 34 77 45 76 23 77 49 69 37 68 12 67 54 67 29	observations.  3 8 5 1 3 4 5 4 2 2 3 2 4 4 6 6 4 1 9 9 2 5 5 3 5 7 2 1 3 3 1 1 2 2 2 5 5 3 2 2	+ 4 31 + 4 52 + 6 20 + 6 55 + 5 57 + 5 59 + 6 36 + 7 20 + 6 30 + 6 30 + 6 30 + 6 30 + 5 32 + 5 5 32 + 5 5 31 + 6 36 + 7 20 + 6 30 + 6 30 + 5 31 + 5 5 32 + 5 5 32 + 5 5 4 + 7 5 20 + 6 35 + 7 5 20 + 6 35 + 7 5 20 + 6 37 + 7 5 20 + 6 30 + 7 5 20 + 6 30 + 7 5 20 + 7 5 20 + 6 30 + 7 5 20 + 7 5 2	
22, 22, 25, 26, 27, 28, March 1, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 20, 23, 24, 25, 26, 27,	-03 37 -63 34 -61 33 -61 18 -61 04 -61 43 -62 10 -62 46 -63 05 -61 41 -60 50 -61 23 -61 16 -60 46 -60 03 -59 22 -58 31 -58 30 -56 42 -54 05 -53 12 -49 05 -46 32 -44 59 -43 41 -41 02 -38 40	47 01 49 29 53 40 57 41 63 45 69 36 72 25 76 30 80 20 85 20 87 41 91 26 91 43 92 20 95 15 100 31 98 59 98 32 101 15 106 17 108 15 110 24 112 47 115 53 116 57 116 42 116 17	7 2 6 6 4 1 7 11 1 7 3 10 7 6 4 4 7 1 3 2 3 6 10 10 10 2 6 6 10 10 10 10 10 10 10 10 10 10 10 10 10	+40 30 +40 30 +41 57 +45 51 +46 01 +50 35 +52 17 +47 19 +47 47 +49 28 +49 02 +48 01 +44 53 +41 02 +39 50 +40 37 +37 37 +32 54 +26 34 +21 52 +17 09 +12 02 +9 43 +7 04 +4 10 +6 56	21. 22. 23. 24. 27. 30. 31. June 1. 5. 6. 7. 8. 9. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 23.	-21 01 -20 39 -20 30 -19 54 -20 09 -20 50 -21 54 -23 44 -25 47 -26 30 -27 12 -28 19 -28 36 -28 57 -30 18 -30 30 -30 35 -31 09 -32 54 -34 44 -35 39 -35 40 -35 08 -34 55 -34 12	66 24 63 01 59 42 57 55 57 31 55 32 53 00 51 48 49 40 46 02 43 07 40 14 37 49 35 55 33 42 33 13 11 29 49 26 50 23 35 21 37 20 24 19 33 18 27	2 3 2 3 1 2 2 4 3 2 3 5 5 3 4 5 5 7 2 6 6 1 9 4 9 5 5 2 1 2 3 3 16	+ 7 36 + 7 46 + 8 27 + 9 44 + 9 27 + 9 44+ + 11 15 + 13 44 + 14 22 + 15 09 + 16 23 + 20 25 + 21 19 + 21 57 + 22 34 + 23 37 + 26 29 + 27 28 + 25 09 + 26 46 + 28 44 + 29 26 + 29 16 + 29 15 + 21 57 + 29 15

<sup>\*</sup> On shore at King George's Sound.

<sup>†</sup> On shore at Port Louis, Mauritius.

General Table of the Inclinations observed on board Her Majesty's hired Bark "Pagoda."

		Inclina	ation.					Inclin	ation.	
Date.	Lat. Lo	ong. Fox. F. 1.	Fox. C. 9.	Mean.	Date.	. Lat.	Long.	Fox. F. 1.	Fox, C. 9.	Mean.
1844. November 10, 21, 21, 1845.  January 7, 9, 10, 11, 12, 13, 14, 15, 16, 27, 30, 31, February 1, 22, 33, 44, 55, 66, 77, 18, 19, 20, 21, 24, 25, 26, 27, 28, March 1, 22, 33, 14, 166, 17, 18, 19, 20, 21, 24, 25, 26, 27, 28, March 1, 22, 33, 34, 14, 16, 17, 18, 19, 20, 21, 24, 25, 26, 27, 28, March 1, 22, 33, 5, 66, 77, 28, 9, 10, 11, 13, 14, 16, 17, 18, 19, 20, 21, 24, 25, 26, 27, 28, March 1, 21, 21, 24, 25, 26, 27, 28, March 1, 21, 21, 21, 24, 25, 26, 27, 28, March 1, 21, 21, 21, 24, 25, 26, 27, 28, March 1, 21, 21, 21, 21, 21, 21, 21, 21, 21,	-33 56 18 -33 56 18 -33 56 18 -34 12 18 -34 12 18 -34 14 18 -34 45 17 -35 18 13 -37 25 13 -35 17 14 -39 10 14 -40 31 14 -42 50 13 -44 50 13 -44 50 13 -49 01 11 -48 35 10 -50 39 10 -51 39 7 -53 57 66 -53 37 7 -55 13 55 -60 43 49 9 -51 50 19 -62 06 12 -61 55 16 -61 50 19 -62 36 37 -65 37 28 -66 37 38 -66 57 38 -66 57 38 -66 57 38 -66 57 38 -66 57 38 -66 57 38 -66 57 38 -66 57 38 -66 33 36 -66 57 38 -66 57	8 29	***  -53 50  -53 34  -51 27  -51 16  -51 18  -53 12  -54 59  **  -57 35  -57 24  -57 35  -57 25  -57 25  -63 17  -63 55  -64 44  -64 25  -63 35  -64 44  -64 25  -65 35  -66 41  -67 56  -68 31  -69 27  -70 20  -69 30  -69 30  -69 30  -69 31  -70 20  -69 30  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 31  -70 20  -69 30  -70 20  -70 20  -70 20  -70 20  -70 20  -70 20  -70 20  -70 20  -70 20  -70 20  -70 30  -70 40  -70 41	Mean.	1845. March 18. 19. 20. 22. 24. 25. 26. 27. 28. 29. 30. April 7. 11. 12. 20. 23. 24. 25. 27. 28. 29. May 1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 27. 30. June 2. 3. 4. 5. 6. 7. 8. 91. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 27. 30. June 12. 23. 27. 30. June 13. 14. 15. 16. 17. 18. 19. 19. 20. 21. 22. 23. 27. 30. June 13. 14. 15. 16. 17. 18.	-53 00 -51 10 -48 59 -47 21 -45 08 -43 21 -41 08 -43 21 -41 08 -33 02 -35 13 -35 02 -35 05 -35 05 -35 05 -35 05 -35 05 -35 06 -35 33 -34 16 -32 28 -29 18 -27 41 -21 22 -22 47 -21 47 -21 47 -21 47 -20 38 -20 26 -20 36 -20 36 -20 36 -20 39 -20 29 -20 29 -20 29 -20 29 -20 29 -20 39 -20 29 -20 39 -20 29 -20 39 -20 29 -20 39 -20 29 -20 39 -20 29 -20 39 -2	110 22 111 26 112 22 111 26 116 50 116 50 116 50 116 50 116 50 116 50 116 50 116 50 117 16 117 56 117 20 118 20 118 26 Cape of Cape o	Fox, F. 1.  -77 28 -76 41 -76 30 -75 31 -72 45 -70 11 -68 49 -66 28 -65 28 -65 48 -65 11 -65 11  * -65 28 -64 44 -69 19 -57 17 -55 49 -54 03 -54 16  * -52 49 -52 17 -50 57 -51 14 -51 39 -51 50 -52 03 -54 03 -54 03 -52 00 -52 20 -52 51  * -53 39 -54 03 -54 03 -54 09 -54 14 -54 38 -58 36 -58 44 -58 50 -57 38 -58 44 -58 50 -57 28 -57 34 -57 66 -56 08 -57 38 -57 38 -58 37 -53 37 -53 37 -53 37 -53 37 -53 37 -53 37 -53 37 -53 37 -53 37 -53 37 -53 39 -54 08	- 77 39' - 77 36 - 76 04 - 75 327 - 72 10 - 71 14 - 68 04 - 66 21 - 66 00 - 65 24 - 64 55 § - 64 55 § - 64 55 9 - 65 14 - 65 59 - 65 14 - 65 59 - 65 14 - 65 59 - 65 14 - 65 59 - 65 14 - 65 59 - 65 14 - 65 59 - 65 14 - 65 59 - 65 14 - 65 59 - 53 46 - 54 18 - 51 21 - 51 33 - 51 21 - 51 46 - 52 00 - 51 58 - 53 01 - 53 01 - 53 59 - 53 53 - 53 59 - 53 53 - 53 59 - 53 5	Mean.  - 77 34 - 77 09 - 76 17 - 75 32 - 73 27 - 72 28 - 70 43 - 68 27 - 65 36 - 65 44 - 65 36 - 65 14 - 65 59 - 65 11 - 64 18 - 59 25 - 57 22 - 55 07 - 54 11 - 54 21 - 54 21 - 54 27 - 52 49 - 52 35 - 53 30 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 36 - 53 37 - 57 26 - 56 37 - 57 34 - 57 36 - 58 36 - 58 36 - 58 36 - 58 37 - 57 36 - 56 37 - 57 36 - 56 37 - 57 36 - 56 37 - 57 36 - 56 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 57 36 - 58 37 - 58 37 - 58 37 - 58 37 - 58 37 - 58 37 - 58 37 - 58 38 - 58 37 - 58 37 - 58 38 - 58 37 - 58 37 - 58 38 - 58 38

<sup>\*</sup> Magnetic Observatory, Cape of Good Hope.

<sup>‡</sup> Probably a wrong degree; omitted in the mean.

<sup>|</sup> King George's Sound.

<sup>†</sup> Dock Yard, Simon's Bay.

<sup>§</sup> Needle A. ¶ Needle B.

<sup>\*\*</sup> Port Louis, Mauritius.

General Table of the Intensities of the Magnetic Force observed on board Her Majesty's hired Bark "Pagoda."

			Inter	isity.					Inten	sity.	
Date.	Lat.	Long.	Fox, F. 1.	Fox, C. 9.	Mean.	Date.	Lat.	Long.	Fox, F. 1.	Fox, C. 9.	Mean.
1844. Dec. 1 and 5. 21.		18 29 18 26	0·999* 1·005†		0·999 1·005	1845. March 19. 20.		$11\overset{\circ}{1}\ 2\overset{\circ}{6}$ $112\ 22$	1·787 1·798	1.821	1·787 1·810
1845. January 10.	-34 45	17 48	0.981	0.985	0.983	22. 24.	$\begin{vmatrix} -47 & 21 \\ -45 & 08 \end{vmatrix}$	115 15 116 50	1.825	1·842 1·820	1·834 1·820
11. 12.	$\begin{vmatrix} -35 & 29 \\ -35 & 17 \end{vmatrix}$	15 09 14 00	••••••	$0.968 \\ 0.923$	$\begin{array}{c} 0.968 \\ 0.923 \end{array}$	25.	$-43 21 \\ -41 09$	116 50 116 26	1·760 1·746	1.804 1.758	1·782 1·752
13.	-35 18	13 26	0.950	0.933	0.942	26. 27.	$-38 \ 46$	116 15	1.738	1.722	1 730
14. 15.	$\begin{vmatrix} -37 & 25 \\ -38 & 40 \end{vmatrix}$	$13 24 \\ 14 27$	0.965 1.008	0.978	0·965 0·993	28. 29.	$\begin{vmatrix} -37 & 02 \\ -36 & 12 \end{vmatrix}$	116 57 116 49	1.695 1.673	1.677 1.670	1.686 1.672
16.	-39 10	14 40	0.989	0.964	0.977	30.	-35 13	117 18	1.702	1.694	1.698
17. 18.	$\begin{vmatrix} -40 & 31 \\ -42 & 50 \end{vmatrix}$	14 23 13 00	0.994 0.997	0.984	0·989 0·997	April 7.	$-35 02 \\ -35 02$	117 56 117 56	1.688 1.688	1.688	1.688§
19.		13 19	1.007		1.007	12.	-35 05	117 56		1.688	اً ا
$\begin{array}{c} 21. \\ 22. \end{array}$	$-49 01 \\ -48 35$	$11 28 \\ 10 51$	1.051 1.060	1.051	1.051 1.060	23. 24.	$-35 33 \\ -34 16$	114 40 113 01	1.688 1.641	1.672	1.680 1.641
23. 24.	-50 39	10 22	1.094	1.093	1.094	25.	-32 28	111 31	1.613	1.573	1.593
24. 25.	$\begin{vmatrix} -51 & 49 \\ -53 & 07 \end{vmatrix}$	9 33 7 43	1·120 1·122	1·109 1·134	1·115 1·128	27. 28.	$\begin{vmatrix} -29 & 18 \\ -27 & 41 \end{vmatrix}$	106 52 106 34	1·553 1·490	1·499 1·478	1·526 1·484
$26. \\ 27.$	$-53 57 \\ -55 13$	6 05 5 53	1·143 1·161	1.141	1.142	29.	-25 53	105 03	1.470	1.447	1.459
30.		4 00	1.240	1.143	$1.152 \\ 1.240$	May 1. 2.	$\begin{bmatrix} -23 & 59 \\ -24 & 01 \end{bmatrix}$	99 15 97 28	1·367 1·379	1·381 1·381	1·374 1·380
31. February 1.	$\begin{bmatrix} -61 & 10 \\ -62 & 06 \end{bmatrix}$	$\begin{array}{c} 9 & 05 \\ 12 & 52 \end{array}$	1.285	1.288	1.247	3.	-23 55	96 01	1.365	1.377	1.371
2.	-61 55	16 30	1.331	1·349 1·321	$1.349 \\ 1.326$	4. 5.	$\begin{vmatrix} -24 & 17 \\ -24 & 02 \end{vmatrix}$	93 50 92 07		1·352 1·367	1·352 1·367
3. 4.		$19 14 \\ 20 33$	1·334 1·353	1.347	1.334	6.	-2247	91 00	1.324		1.324
5.		21 48	1 999	1.362	$1.350 \\ 1.362$	7. 8.	$\begin{vmatrix} -21 & 47 \\ -20 & 42 \end{vmatrix}$	89 41 87 55	1·326 1·294	1·314 1·298	1·320 1·296
6. 7.	$\begin{vmatrix} -64 & 23 \\ -65 & 37 \end{vmatrix}$	$24 12 \\ 28 39$	1·401 1·432	1·398 1·432	$1.400 \\ 1.432$	9.	-20 38	85 14	1.265	1.263	1.264
8.	-66 27	30 45		1.448	1.448	10. 11.	$\begin{vmatrix} -20 & 26 \\ -20 & 36 \end{vmatrix}$	82 11 79 16	1·257 1·247	1·248 1·213	$1.253 \\ 1.230$
9. 10.		$\begin{array}{c} 36 \ 48 \\ 38 \ 50 \end{array}$	1·482 1·491	1·470 1·483	1·476 1·487	12.	-20 44	78 31	1.238	1.234	1.236
11.	-67 37	40 00	1.519	1.496	1.508	13. 14.	$\begin{bmatrix} -20 & 39 \\ -20 & 29 \end{bmatrix}$	77 43 76 22	1·237 1·222	1.233	1·235 1·222
12. 13.		39 53 40 12	1·494 1·499	1·496 1·490	1·495 1·495	16.	-20 27	70 41	1.199	1·205 1·210	1.202
14.	-6624	40 01	•••••	1.494	1.494	17. 18.	$\begin{vmatrix} -20 & 34 \\ -21 & 07 \end{vmatrix}$	69 24	1.191	1.210	1·210 1·191
16. 17.		38 37 40 12	1·470 1·463	1·450 1·482	1·460 1·473	19.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	67 54	1·203 1·201	1·206 1·190	1.205
18.	-64 22	40 49	1.460		1.460	20. 21.	$\begin{bmatrix} -21 & 12 \\ -21 & 02 \end{bmatrix}$	67 29 66 26	1.181	1.178	1·196 1·180
19. 20.		$\frac{41}{45} \frac{35}{44}$	1·416 1·437	1·453 1·462	1·434 1·450	22.	-20 40	62 58	1.171	1.173	1.173
21.	-63 36	46 46	1.457	1.470	1.464	23. 27.	$\begin{vmatrix} -20 & 31 \\ -20 & 09 \end{vmatrix}$	59 42 57 31	1·171 1·156	1.156	1·171 1·156
$egin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{bmatrix} -62 & 36 \\ -61 & 30 \end{bmatrix}$	$51 40 \\ 53 44$	1·466 1·476	1.498	1·466 1·487	30. June 2.	$ \begin{array}{r rrrr} -21 & 47 \\ -26 & 25 \end{array} $	53 30 49 12	1·179 1·160	1.161	1·170 1·160
26.	-61 19	57 34	1.535	1.506	1.521	3.	-26 26	48 20		1.164	1.164
27. 28.	$\begin{bmatrix} -61 & 05 \\ -61 & 43 \end{bmatrix}$	$64 12 \\ 71 08$	1·553 1·604	1.560 1.605	1·557 1·605	4. 5.	$\begin{vmatrix} -27 & 13 \\ -28 & 13 \end{vmatrix}$	$\begin{array}{c cccc} 46 & 00 \\ 42 & 50 \end{array}$	1·129 1·125	1.159	1·144 1·125
March 1.	-62 10	72 25	1.657	1.642	1.650	6.	-28 44	42 01	1.117		1.117
2. 3.	$\begin{vmatrix} -62 & 44 \\ -64 & 20 \end{vmatrix}$	76 12 79 38	1.656 1.706	1.653 1.678	$1.655 \\ 1.692$	7. 8.	$\begin{vmatrix} -28 & 35 \\ -28 & 57 \end{vmatrix}$	40 24 37 49	1·128 1·094	1.111	1·128 1·103
5.	$-61 \ 40$	84 54	1.689	1.730	1.710	11.		33 41		1.105	1.105
6. 7.		88 23 91 14	1·729 1·759	1·747 1·749	1·738 1·754		$\begin{vmatrix} -30 & 33 \\ -31 & 06 \end{vmatrix}$	33 19 31 30	1·085 1·061	1.063	1·085 1·062
8.	-61 10	92 07	1.762	1.758	1.760	14.	-33 01	29 36	1.046		1.046
9. 10.	-60 03	92 30 95 50	1·745 1·798	1·750 1·770	1·748 1·784		$\begin{vmatrix} -34 & 31 \\ -35 & 46 \end{vmatrix}$	27 04 23 35	1·059 1·033	•••••	1·059 1·033
11.	-59 52	99 40	1.772	1.836	1.804	17.	-35 38	21 40	1.025	1.033	1.029
13. 14.	-56.55	99 23 101 30	1.786	1·813 1·802	1·813 1·794	18. 23	$\begin{vmatrix} -35 & 07 \\ -34 & 12 \end{vmatrix}$	20 46 18 26	1.013 1.012	1.001	1.013 1.007¶
15. 16.	-55 46	103 12	1.816	1.815	1.816	Magnetic Ob	servatory,	Cape of	1.001	1.000	1.000
17.	-54 14	106 10 108 10	1.801 1.816	1·817 1·821	1·809 1·819	Good Hope, 21	nd and 11t	h of July.	1 001	1 000	1000
18.		110 22	1.814	1.825	1.820						

<sup>\*</sup> Observed on shore, Magnetic Observatory, Cape of Good Hope.

<sup>†</sup> Observed on shore, Dock-yard, Simon's Bay.

<sup>‡</sup> Not included in the mean.

<sup>§</sup> King George's Sound; observed on shore.

<sup>||</sup> Port Louis, Mauritius; observed on shore.

<sup>¶</sup> Simon's Bay, on board.

Observations of the Magnetic Inclination between the Cape of Good Hope and Van Diemen Island, by Lieut. Alexander Smith, R.N.

Date.	Lat.	Long.	Corrected Inclination.	Date.	Lat.	Long.	Corrected Inclination.
1844. July 29. 30. 31. August 1. 2. 4. 5. 6. 7. 8. 9. 10. 11. 13. 14. 15. 16. 17. 18.	-38 00 -38 28 -39 06 -39 42 -39 33 -39 33 -39 50 -40 01 -40 32 -41 00 -41 00 -40 43 -40 56 -39 34  -39 00 -38 31 -38 22 -38 08 -38 10	4 20 7 45 12 00 15 44 23 05 26 52 28 36 32 22 36 40 41 40 46 13 49 12 53 30 60 55  65 44 68 45 70 10 73 35 75 22	-52 00 -53 03 -55 42 -57 06 -59 32 -61 47 -62 08 -62 56 -64 09 -64 42 -65 19 -66 08 -66 25 -67 27 -67 18 -67 19 -66 45 -66 45 -66 42	1844. Aug. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. Sept. 1. 2. 3. 4. 5. 6.	-38 25 -38 48 -39 04 -39 58 -40 06 -40 06 -40 02 -39 52 -39 54 -40 08 -40 03 -41 16 -41 54 -41 58 -42 17 -42 35 -43 00 -43 16 -43 28 -44 06	76 44 77 50 79 45 84 00 87 00 90 52 95 10 99 22 102 00 105 55 109 06 113 25 117 40 119 00 122 30 125 40 129 36 133 44 137 10 141 37	$\begin{array}{c} -6\mathring{6} & 54 \\ -67 & 14 \\ -67 & 17 \\ -67 & 43 \\ -68 & 13 \\ -68 & 41 \\ -69 & 08 \\ -69 & 00 \\ -69 & 00 \\ -69 & 22 \\ -70 & 30 \\ -71 & 20 \\ -71 & 33 \\ -71 & 45 \\ -72 & 08 \\ -72 & 13 \\ -71 & 55 \\ -72 & 14 \\ \end{array}$

Observations of the Magnetic Force between the Cape of Good Hope and Van Diemen Island, by Lieut. Alexander Smith, R.N.

THE PERSON NAMED IN COLUMN TWO								
Date.	Lat.	Long.	Method employed.	Angle of deflection.	Thermo- meter.	Ship's head.	Intensity. Hobarton = 1.800.	Remarks.
1844.	0 /	0 /		0 /				
July 30.	-38 28	$2\overset{\circ}{7}$ $4\overset{\prime}{5}$	wt. 2 grs.	$2\mathring{0}$ $1\overset{\prime}{3}$	52	S.E. $\frac{1}{2}$ E.	0.953 0.953	
Aug. 5.	-3950	28 36	wt. 2 grs.	17 04	60	s.e. by e.	1.121 $1.117$	
	-39 50	28 36	wt. 3 grs.	$26 \ 35$	59	s.e. by E.	1.113	
9.	-41 00	46 13	wt. 2 grs.	14 50	60	E. $\frac{1}{2}$ S.	1.288	
	-41.00	46 13	wt. 3 grs.	22 46	61	E. ½ S.	1.289 } 1.200	
15.	-39 00	65 44	wt. 2 grs.	13 35	47	s.e. by E.	1.403	Much motion.
	-3900	65 44	wt. 3 grs.	21 26	44	s.e. by E.	1.364	much motion.
18.	-38 08	73 35	wt. 2 grs.	12 57	58	E.	1.471 1.454	Smooth water.
	<b>-38 08</b>	73 35	wt. 3 grs.	20 18	59	E.	1.437	Smooth water.
19.	-38 10	75 22	wt. 2 grs.	13 28	66	S.E. 1/2 E.	1.415	Smooth.
	-38 10	75 22	wt. 3 grs.	20 02	66	S.E. 1/2 E.	1.456 1.435	Sinoth.
24.	-40 06	87 00	wt. 2 grs.	12 14	64	E.S.E.	1.555	
	-40 06	87 00	wt. 3 grs.	17 42	60	E.S.E.	1.640 $1.597$	
28.	-39 54	102 00	wt. 2 grs.	11 13	51	E.S.E.	$1.694 \} 1.724$	
	-39 54	102 00	wt. 3 grs.	16 31	51	E.S.E.	1.754	
30.	$-40 \ 31$	109 06	wt. 2 grs.	11 04	58	E.S.E.	1.717 1 1.751	
	$-40 \ 31$	109 06	wt. 3 grs.	16 14	59	E.S.E.	1.785 $1.751$	
Sept 3.	$-42 \ 35$	125 40	wt. 2 grs.	10 04	56	E. by s.	1.006 1	
1	$-42 \ 35$	125 40	wt. 3 grs.	15 12	55	E. by s.	1.902 1.894	
5.	-43 14	133 22	wt. 2 grs.	10 21	49	E. by s.	1.0945	
	-43 14	133 22	wt. 3 grs.	15 11	48	E. by s.	1.904	
6.	-43 28	137 10	wt. 2 grs.	10 06	51	E. 1/2 S.	1 2 2 7 2 3	
	-43 28	137 10	wt. 3 grs.	15 36	51	E. $\frac{1}{2}$ S.	$\begin{vmatrix} 1.879 \\ 1.854 \end{vmatrix}$ 1.866	
Oct. 2.	-4252	147 24	wt. 2 grs.	10 33	54	1)	1.800 1	
	-42 52	147 24	wt. 3 grs.	16 05	54	$\left  \right. \right.$ On shore.	$1.800 \} 1.800$	Hobarton: Magneti Observatory.

Hobarton is taken as the base station; no correction has been applied for the effect of the ship's iron. In the results entered in the map of the Magnetic Force from Lieut. Smith's observations on the 24th, 28th, and 30th of August, the determinations with 2 grains only have been used; those with 3 grains are so discordant with other results as necessarily to indicate an error in them.

Observations of the Magnetic Inclination between Van Diemen Island and the Cape of Good Hope, by Lieut. Joseph Dayman, R.N.

## Observations of the Magnetic Force between Van Diemen Island and the Cape of Good Hope, by Lieut. Joseph Dayman, R.N.

Date.	Lat.	Long.	Weights.	Angle of deflection.	Thermo- meter.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity. Hobarton = 1.800.	Remarks.
1844.			Orre							
Dec. 6.	$-42^{\circ}52^{\circ}$	147 24	grs. 2	10 43	7î	1	1.800	١		
Dec. o.	-42 52		3	16 11	71	On shore.	1.800	· <b>&gt;</b>	1.800	Magnetic Observa- tory, Hobarton.
16.	$-42 \ 32 \ -44 \ 48$			10 21	55	w. by s.	1.863	}		tory, Hobarton.
10.	$-44 \ 48$		2	15 32	55	w. by s.	1.873	<b>  }:041</b>	1.827	-
1 17	$-44 \ 48$ $-44 \ 30$		3		67	w. by s.	1.834	{		
17.		143 56	2	10 31				<b>}</b> • 041	1.815	
10	-44 30	143 56	3	15 29	67	w. by s.	1.879	1		
18.			2	10 20	69	w. by s.	1.866	}•041	1.818	
	-44 34	142 51	3	15 44	70	w. by s.	1.851	.059	1.040	
19.		139 37	3	15 18	63	s.w. by s.	1.901	<b>~∙0</b> 53	1.848	
21.		137 18	2	10 29	69	w.	1.840	<b>}</b> · 037	1.828	
	-4224	137 18	3	15 24	70	w.	1.889	Į ,		
23.	-41 46	133 26	2	10 32	58	N.	1.831	-020	1.846	
1	-41 46	133 26	3	15 18	57	N.	1.901	Į		
28.			2	10 05	63	n.w. by n.	1.912	}020	1.856	A long heavy swell.
	-40 05	128 23	3	15 49	63	n.w. by n.	1.840	] ~~"	_ 550	
30.		124 04	2	10 38	65	N. by w.	1.814	020	1.793	A long heavy swell.
	-39 25		3	16 04	65	n. by w.	1.813	J ~~~	- 130	2000 2007 5000
31.	-38 00	123 38	2	10 25	62	N.N.W.	1.852	}020	1.799	A long heavy swell.
1	-38 00	123 38	3	16 19	62	N.N.W.	1.786	7 - 020	1 799	li long neary swem
1845.						_				
Jan. 1.	-38 21	122 46	2	10 49	71	N.W. by W.	1.783	-025	1.777	
ľ	-38 21	122 46	3	15 59	72	n.w. by w.	1.822	J - 020	- , , ,	
3.		124 58	2	10 55	69	N.W.	1.767	}020	1.771	
ľ	-3714	124 58	3	16 03	69	N.W.	1.815	5 - 020	- , , .	
6.	-3628	118 57	2	11 11	67	N.N.W.	1.725	}020	1.716	
	-3628	118 57	3	16 41	67	N.N.W.	1.747	7-020	1-710	
7.	-35 22	117 46	2	11 04	65	N.N.W. $\frac{1}{2}$ W.	1.743	}020	1.722	
	-35 22	117 46	3	16 44	64	N.N.W. $\frac{1}{2}$ W.	1.742	> - 020	1-722	
11.		116 42	2	10 55	68	s.s.w.	1.767	1	1.735	
	-3606	116 42	3	16 26	68	s.s.w.	1.773	<b>}</b> - •055	1.715	
16.		112 59	2	11 24	66	N.W.	1.693	1	1.000	
1	-34 58	112 59	3	17 07	66	N.W.	1.704	<b>}</b> -·012	1.686	
17.		111 04	2	11 54	67	N.W. by W.	1.623	1	- 0	
1 -1.	$-33 \ 47$	111 04	3	17 53	67	n.w. by w.	1.629	\ \ \ \017	1.609	
18.		108 24	2	11 57	69	n.w. by w.	1.616	1		
1	$-33 \ 37$		3	17 59	69	n.w. by w.	1.624	<b>}</b> - • 017	1.603	
20.		1	2	12 30	72	N.W. $\frac{1}{2}$ N.	1.546	1		
<b>1</b> ~0.	$-29 \ 40$ $-29 \ 40$		3	18 58	72	$\begin{array}{c c} N.W. \frac{1}{2} N. \\ N.W. \frac{1}{2} N. \end{array}$	1.543	<b>}</b> 007	1.537	
21.		105 28	2	13 02	73	N. W. 2 N.	1.484	1		
21.	-28 04 $-28 04$		3	19 24	73	N.	1.210	<b>}</b> - •004	1.493	
22.	-26   44		2	13 03	76	N.W.	1.483	1		
22.	1		}			1	1.462	<b>}</b> •007	1.466	
മാ	-26 44		3	20 05	76	N.W.				
23.			2	13 39	75	N.W.	1.418	<b>}</b> 007	1.421	
24	-2552		3	20 24	75	N.W.	1.439	1		
24.			2	13 31	76	N.W.	1.432	}006	1.415	
2-	-24 50		3	20 51	76	N.W.	1.410	1		
25.	1		2	13 30	75	w.N.w.	1.435	010	1.407	
ł	-24 00		3	21 02	75	w.n.w.	1.400			
27.		95 40	2	14 22	78	w. by N. $\frac{1}{2}$ N.		-012	1.334	1.
l	-23 11		3	21 58	78	w. by $n \cdot \frac{1}{2} n$ .		[]		
28.		93 48	2	14 16	78	w. by N. $\frac{1}{2}$ N.		]012	1.337	
	-2254		3	22 03	79	w. by N. $\frac{1}{2}$ N.		1	•	
29.			2	15 02	77	W. $\frac{1}{2}$ N.	1.291	]017	1.277	
	-22 19		3	22 46	77	$W \cdot \frac{1}{2} N$	1.297	1		
30.			2	14 58	80	$W \cdot \frac{1}{2} N \cdot$	1.296	}017	1.288	1
l.	-22 17		3	22 28	81	$W \cdot \frac{1}{2} N \cdot$	1.314		1 200	]
31.			2	15 11	80	$W \cdot \frac{1}{2} N \cdot$	1.278	\\ \ \ -·017	1.274	
1	-22 11	86 30	3	22 38	80	$W \cdot \frac{1}{2} N \cdot$	1.304		- ~	
				1				<u> </u>		

Lieut. Dayman's observations of the Magnetic Force. (Continued.)

Date.	Lat.	Long.	Weights.	Angle of deflection.	Thermo- meter.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity. Hobarton = 1.800.	Remarks.
1845. Feb. 1.	-22 08 -22 08		grs. 2 3	15 13 23 25	81 81	$\begin{array}{c} W \cdot \frac{1}{2} N \cdot \\ W \cdot \frac{1}{2} N \cdot \end{array}$	1·275 1·262	}017	1.251	·
3.		80 10	2 3	15 16 22 55	83 83	W. ½ N. W. ¼ N.	1.272	-:019	1.261	
4.	$-22\ 35$	78 08	2 3	15 42 23 20	83 83	$\frac{3}{4}$ N. $\frac{3}{4}$ N.	1.237	$\left.\right\}$ $015$	1.237	
5.	$-22\ 38$	76 10	2 3	15 31	82	$W.\frac{3}{4} N.$	1.252	-015	1.236	
6.		74 18	2	23 41 15 50	82 82	W. $\frac{3}{4}$ N. W. $\frac{3}{4}$ N.	1.250	$\left.\right\}$ $015$	1.216	
7.	-22 28 $-22 33$	72 20	3 2	23 58	82 81	$W \cdot \frac{3}{4} N \cdot W \cdot \frac{1}{2} N \cdot$	1·236 1·229	} <b>01</b> 6	1.211	
8.	-22 33 $-22 41$	69 54	3 2	24 11 15 38	81 · 81	$\mathbf{W} \cdot \frac{1}{2} \mathbf{N} \cdot \mathbf{W}$	1·225 1·240	} -·018	1.215	
10.	$-22  41 \\ -23  52$	69 54 64 59	3 2	24 13 15 58	81 84	$\mathbf{W}$ . $\mathbf{W}$ . $\frac{1}{2}$ S.	1·223 1·217	}022	1.196	
11.	-23 52 $-24 23$	62 54	3 2	24 20 16 13	84	$W_{\bullet} \frac{1}{2} S_{\bullet}$ $W_{\bullet} \frac{1}{2} S_{\bullet}$	1·218 1·199	022	1.177	
12.		61 11	3 2	24 44 16 01	83 84	$W \cdot \frac{1}{2} S \cdot W \cdot \frac{1}{2} N \cdot$	1·199 1·214	} - 018	1.197	
13.	-24 50 $-24 43$	59 46	3 2	24 22 16 17	84 85	$\begin{array}{c c} w \cdot \frac{1}{2} & N \cdot \\ w \cdot by & N \cdot \frac{1}{2} & N \cdot \end{array}$	1·216 1·194	-011	1.184	
14.	,	58 37	3 2	24 47 16 23	85 85	w. by N. $\frac{1}{2}$ N. w. by N. $\frac{1}{2}$ N.		\\ \011	1.178	
17.	-24 36 $-25 13$	1	3 2	24 55 16 46	84 84	$\begin{array}{c} \text{w. by N.} \frac{1}{2} \text{ N.} \\ \text{w.} \frac{1}{2} \text{ N.} \end{array}$	1·191 1·160	$\left.\right \right\} = 017$	1.139	
18.		49 06	3 2	25 49 17 09	84 82	W• ½ N• W•	1·152 1·135	020	1.114	
20.		49 06 42 18	3 2	26 16 17 43	81 81	W. w. ½ S.	1·133 1·100		1.086	
21.	-28 15 $-29 21$	i .	3 2	26 44 17 46	81 81	$\mathbf{w} \cdot \frac{1}{2} \mathbf{S} \cdot \mathbf{w}$	1·116 1·097	$\left \left\{\begin{array}{c} -022\\ -\cdot 020 \end{array}\right.\right $	1.081	
22.	$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$		3 2	26 59 17 55	81 82	w. w. <u>I</u> n.	1·106 1·088	$\left. \begin{array}{c}020 \\018 \end{array} \right.$	1.076	
24.	$-30 \ 10$ $-31 \ 19$	36 17	3 2	27 07 18 29	82 83	$W \cdot \frac{1}{4} N \cdot W \cdot \frac{1}{2} N \cdot$	1·101 1·056		1.046	
25.	$\begin{bmatrix} -31 & 19 \\ -32 & 17 \end{bmatrix}$	1	3 2	28 01 18 59	83 82	$W. \frac{1}{2} N. W. \frac{3}{4} N.$	1.068 1.029	$\left. \left. \right\} - 016 \right. $	1.026	
26.	$\begin{bmatrix} -32 & 17 \\ -34 & 02 \end{bmatrix}$	29 34	3 2	28 28 18 57	82 74	$W \cdot \frac{3}{4} N \cdot W \cdot$	1.052 1.030	-·014 -·018	1.026	
28.	-34 02 -34 36		3 2	28 37 18 38	74 71	S.W. 1/2 W.	1.047 1.047	$\left.\begin{array}{c}035 \\030 \end{array}\right.$	1.021	,
Mar. 1.	$-34 \ 36$	25 23	3 2	28 22 19 27	71 79	S.W. $\frac{1}{2}$ W. W.N.W.	1.056 1.005	$\left.\right\} = 0.00$	1.004	
5.	$\begin{bmatrix} -34 & 46 \\ -34 & 48 \end{bmatrix}$	24 16	3 2	29 35 19 51	79 71	W.N.W. N.W. $\frac{1}{2}$ N.	1.016 0.986	}		
	-34 48		3	30 46	70	$N.W. \frac{1}{2} N.$	0.981	.000	0.984	."

Observations of the Magnetic Declination, made on board Her Majesty's Ship Erebus, by Captain Sir James Clark Ross, between the Cape of Good Hope and Van Diemen Island.

Date   Lat   Long   \$\frac{1}{3}\$   Declination observed.   Ship's head   Inclination   Corrected Declination   Remarks.	Г		-	-		1			*******		<del></del>		
1840.   April 8.   -35   52   18   41   T.   +28   28   W.   C.   +31   52   E.   E.   E.   C.   +31   52   E.   E.   E.   -36   11   18   35   R.   +31   50   S.   E.   E.   S.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   E.   E.   E.   E.	١					.							
1840.   April 8.   -35   52   18   41   T.   +28   28   W.   C.   +31   52   E.   E.   E.   C.   +31   52   E.   E.   E.   -36   11   18   35   R.   +31   50   S.   E.   E.   S.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   E.   E.   E.   -36   12   20   53   T.   +33   20   S.   E.   E.   E.   E.   E.   E.   E.	1	Date	Lat		Lo	n.n.	rve	Declination	Shin's head	Inclination	tion for	Corrected Declination	Domonico
1840.   April 8.   -35   52   18   41   T.   +28   28   W.   T.   +31   52   E.S.E.   C.   +31   53   S.E.   by E.   S.E.   -53   30   -2   13   +29   37   +30   08   Compast G. H. under the finit	1	Date.	Liau	:	110	"g.	ose.	observed.	omp s nead.	inclination.		Corrected Decimation.	Remarks.
1840.   April 8.   -35   52   18   41   T.   +28   28   W.   T.   +31   52   E.S.E.   C.   +3   33   52   13   43   13   14   14   15   15   15   14   16   16   16   16   16   16   16	I						0						
April 8 35 52 18 41	ŀ												
T. +31 52 E.S.E. C. +32 13 S.E. by E. S. +30 44 S. +32 11 S. +32 12 S.E. by E. S. +30 44 S. +36 11 S. +35 12 E.S.E. by E. S. +36 11 S. +35 12 E.S.E. by E. S. +30 41 S. +36 12 20 55 T. +32 92 S.S.E. \( \frac{1}{2}\) E.S.E. by E. S. +30 13 S.E. by E. S. +30 14 S. S. by W. T. +30 19 S. S. by W. T. +30 19 S. S. by W. S. by W. S. S. S. by E. R. +31 10 S. S. by E. S. +30 11 S. \( \frac{1}{2}\) E.S. +30 14 S. S. by W. S. B. \( \frac{1}{2}\) E.S. +30 17 S. S. S. +30 17 S. S. S. +30 17 S. S. S. +30 17 S. S. S. E. +30 17 S. S. E. +30 17 S. S. S. E. +30 17 S. S. S. E. +30 17 S. S. S. E. +30 17 S. S. E. +30 17 S. S. E. +30 17 S. S. E. +30 17 S. S. E. +30 1	١		o	,	.0	,		0 1			0 /	0 /_ 0 /	
Co.   +31 50   T.   +32 10   S.   S.   E.   S.   E.   S.   S.   E.   S.   S	1	April 8.	-35	52	18	41			w.	1	+2 05	+30 33)	
T. + 32 13 s. e. by E. s. + 30 04 s. s. by E. s. + 30 14 s. s. by E. s. + 30 14 s. s. by E. s. + 30 14 s. s. by E. s. + 30 14 s. s. by E. s. + 30 17 s. s. by E. s. + 30 17 s. s. by E. s. + 30 19 s. by E. s. + 30 19 s. by E. s. + 30 19 s. by E. s. + 31 10 s. by E. s. + 31 10 s. by E. s. by E. s. + 31 10 s. by E. s. by E. s. + 31 10 s. by E. by E. s. by E.	1								E.S.E.			+29 39	
10	١							+31 50		<b>&gt;−53</b> 30	$ -2 \ 13$		Compass C. H. used
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		-							s.e. by e.				ing observations;
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	i						+30 44		J			no index error.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ı					35				-53 40	1		
1136 21 21 14 S. +32 02 S.S.E. \( \frac{7}{2} \)E. \( \) -36 21 21 14 S. +32 02 S. S.E. \( \frac{7}{2} \)E. \( \) -36 28 21 15 T. +33 026 S. \( \frac{7}{2} \)E. \( \) -36 28 21 15 T. +33 026 S. \( \frac{7}{2} \)E. \( \) -36 28 21 15 T. +33 020 S. \( \frac{7}{2} \)E. \( \) -36 28 21 15 T. +33 020 S. \( \frac{7}{2} \)E. \( \) -37 10 21 31 T. +31 50 S. \( \frac{7}{2} \)E. \( \) -37 10 21 31 T. +31 50 S. \( \frac{7}{2} \)E. \( \) -37 10 21 31 T. +31 50 S. \( \frac{7}{2} \)E. \( \) -37 27 21 20 R. +28 57 S. \( \frac{7}{2} \)E. \( \) -38 20 21 12 T. +31 10 S. \( \frac{7}{2} \)E. \( \) -38 20 21 12 T. +31 10 S. \( \frac{7}{2} \)E. \( \) -38 20 21 12 T. +31 10 S. \( \frac{7}{2} \)E. \( \) -41 15 22 22 S. +31 20 S. \( \frac{7}{2} \)E. \( \) -41 28 25 39 R. +32 40 S. S. \( \frac{7}{2} \)E. \( \) -41 32 25 31 T. +32 20 S. S. \( \frac{7}{2} \)E. \( \) -43 24 29 19 R. +33 58 8 S. S. E. \( \frac{7}{2} \)E. \( \) -33 39 S. S. E. \( \frac{7}{2} \)E. \( \) -43 39 38 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -43 34 38 S. E. \( \frac{7}{2} \)E. \( \) -33 58 S. E. \( \frac{7}{2} \)E. \( \) -44 34 38 38 R. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \frac{33}{2} \)B. \( \f	1	10.						$+31 \ 39$		-55 00			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	١									]	-1 23	+ 30 39 ]	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11.	-36	21	21	14	_			n	+200		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		•										
$ \begin{vmatrix} -36 & 28 & 21 & 15 & 15 & 15 & 15 & 15 & 15 & 15$	1								s. by w.			1'-!	
$ \begin{vmatrix} -36 & 28 & 21 & 15 & T. &   +30 & 90 & S. \\ R. & +30 & 14 & S. &   E. \\ O. & +31 & 00 & S. &   E. \\ S. & +30 & 41 & S. &   E. \\ R. & +31 & 11 & S. &   E. \\ R. & +31 & 12 & S. &   E. \\ R. & +31 & 12 & S. &   E. \\ R. & +31 & 12 & S. &   E. \\ R. & +30 & 01 & S. &   E. \\ T. & +31 & 50 & S. &   E. \\ T. & +31 & 50 & S. &   E. \\ T. & +31 & 50 & S. &   E. \\ O. & -31 & 00 & S. &   E. \\ R. & +30 & 01 & S. &   E. \\ T. & +32 & 10 & S. &   E. \\ O. & -31 & 02 & S. &   E. \\ T. & +32 & 10 & S. &   D. E. \\ S. & +31 & 16 & S. &   D. E. \\ S. & +31 & 16 & S. &   D. E. \\ S. & +31 & 16 & S. &   D. E. \\ S. & +31 & 16 & S. &   D. E. \\ S. & +31 & 16 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 10 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 20 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E. \\ S. & +31 & 30 & S. &   D. E$	1												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			_								1		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	I		-36	28	21	15					1 7 7		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										-55 30		> + 50 40	
$ \begin{bmatrix} S. & +30 & 41 & S. \frac{1}{2} E. \\ T. & +31 & 11 & S. \frac{1}{2} E. \\ R. & +30 & 22 & S. \frac{1}{2} E. \\ R. & +30 & 01 & S. \\ R. & +30 & 01 & S. \\ R. & +30 & 01 & S. \\ R. & +30 & 01 & S. \\ R. & +30 & 01 & S. \\ R. & +30 & 01 & S. \\ R. & +30 & 01 & S. \\ S. & \frac{1}{2} E. \\ R. & +30 & 01 & S. \\ S. & \frac{1}{2} E. \\ R. & +30 & 01 & S. \\ S. & \frac{1}{2} E. \\ R. & +30 & 01 & S. \\ S. & \frac{1}{2} E. \\ R. & +32 & 09 & S. \frac{1}{2} E. \\ O. & +31 & 09 & S. \frac{1}{2} E. \\ O. & +31 & 09 & S. \frac{1}{2} E. \\ O. & +31 & 09 & S. \frac{1}{2} E. \\ O. & +31 & 09 & S. \frac{1}{2} E. \\ O. & +31 & 16 & S. \text{ by E.} \\ S. & +31 & 16 & S. \text{ by E.} \\ S. & +31 & 16 & S. \text{ by E.} \\ S. & +31 & 16 & S. \text{ by E.} \\ S. & +31 & 12 & 27 & S. & 32 & 43 \\ -38 & 20 & 21 & 12 & T. & +31 & 10 \\ T. & +30 & 20 & S. E. & \frac{1}{2} E. \\ -41 & 15 & 22 & 22 & S. & 11 & 22 & 22 \\ S. & +31 & 20 & S. & 12 & E. \\ -41 & 24 & 24 & 32 & T. & +32 & 20 \\ 16. & -41 & 24 & 24 & 32 & T. & +32 & 20 \\ -41 & 25 & 25 & 39 & R. & +32 & 41 \\ S. & & & & & & & & & & & & & & & & & & $	٠						_		S. ½ E.	[		+ 30 00	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ı											l	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1										1		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												1 1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	١					.							
$ \begin{vmatrix} 12. & -37 & 10 & 21 & 31 & T. & +31 & 53 & s. \frac{1}{2} w. \\ T. & +32 & 20 & s. \frac{1}{2} E. \\ T. & +33 & 10 & s. by E. \\ O. & +31 & 09 & s. by E. \\ S. & +31 & 16 & s. by E. \\ S. & +31 & 14 & s. by E. \\ -37 & 27 & 21 & 20 & R. & +28 & 57 & s. by E. \\ -38 & 20 & 21 & 12 & T. & +31 & 10 & s. w. by W. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. w. \\ T. & +30 & 20 & s. E. by s. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s. E. by s. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +33 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & -1 & 26 & 43 & 32 \\ -41 & 28 & 25 & 39 & R. & +32 & 20 & -1 & 26 $	1												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ı	10	0.5	10	01					Ŋ.			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	12.	-37	10	21	31			S. ½ W.	].			·
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$													
$ \begin{vmatrix} 0 & +31 & 09 \\ S. & +31 & 16 \\ S. & by E. \\ T. & +31 & 14 \\ S. & by E. \\ S. & $	1										1	1 21 10	
$ \begin{vmatrix} -37 & 27 & 21 & 20 & R. & +31 & 16 & s. by E. \\ -38 & 20 & 21 & 12 & R. & +28 & 57 & s. E. \frac{1}{2} E. \\ -38 & 20 & 21 & 12 & T. & +31 & 10 & s. w. by W. \\ -38 & 20 & 21 & 12 & T. & +31 & 10 & s. w. by W. \\ -38 & 20 & 22 & 11 & T. & +32 & 10 & s. w. by W. \\ -41 & 4 & 4 & 24 & 32 & T. & +32 & 20 & s. E. by s. \\ -41 & 5 & 22 & 22 & S. & +31 & 20 & s. E. by s. \\ -41 & 5 & 25 & 39 & R. & +32 & 41 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 41 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 41 & s. s. E. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s. s. E. \\ -$	1						_			>-56~00			
$\begin{bmatrix} -37 & 27 & 21 & 20 & R. & +31 & 14 & s. \ by E. \\ -38 & 20 & 21 & 12 & T. & +31 & 10 \\ -38 & 20 & 21 & 12 & T. & +31 & 10 \\ -38 & 20 & 21 & 12 & T. & +31 & 10 \\ -38 & 20 & 21 & 12 & T. & +30 & 04 \\ T. & +30 & 04 & s.w. \ by w. \\ T. & +30 & 20 & s.w. \ s.w. \\ -41 & -39 & 55 & 20 & 35 & T. & +29 & 51 \\ -54 & 00 & 22 & 01 & T. & +32 & 30 \\ -41 & 15 & 22 & 22 & S. & +31 & 20 \\ -41 & 15 & 22 & 22 & S. & +31 & 20 \\ -41 & 24 & 24 & 32 & T. & +32 & 09 \\ -41 & 24 & 24 & 32 & T. & +32 & 09 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -41 & 28 & 25 & 39 & R. & +32 & 40 \\ -42 & 24 & 28 & 13 & T. & +34 & 43 \\ -43 & 24 & 29 & 19 & R. & +33 & 58 \\ -43 & 24 & 29 & 19 & R. & +33 & 58 \\ -43 & 24 & 29 & 19 & R. & +33 & 58 \\ -43 & 24 & 29 & 19 & R. & +33 & 58 \\ -43 & 24 & 29 & 19 & R. & +33 & 54 \\ 25 & -46 & 31 & 48 & 03 & R. & +35 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \\ 28 & -46 & 34 & 52 & 43 & T$	١												
$ \begin{vmatrix} -37 & 27 & 21 & 20 & R. & +28 & 57 & s. by E. \\ -38 & 20 & 21 & 12 & T. & +31 & 10 & s.w. by w. \\ -38 & 20 & 21 & 12 & T. & +31 & 10 & s.w. by w. \\ T. & +30 & 04 & s.w. & s.w. \\ T. & +30 & 20 & s.w. & s.w. \\ T. & +30 & 20 & s.w. & s.w. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.E. by s. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.E. by s. \\ -41 & 24 & 24 & 32 & T. & +32 & 45 & s.s.E. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.E. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.E. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.E. \\ -43 & 24 & 29 & 19 & R. & +34 & 43 & s.s.E. \\ -43 & 24 & 29 & 19 & R. & +33 & 58 & s.s.E. \\ -43 & 24 & 29 & 19 & R. & +33 & 58 & s.s.E. \\ -25 & -46 & 31 & 48 & 03 & R. & +33 & 58 & s.s.E. \\ -28 & -46 & 34 & 52 & 43 & T. & +31 & 44 & N.w. \end{vmatrix}$ $\begin{vmatrix} -37 & 27 & 21 & 20 & R. & +28 & 57 & s.by E. \\ -20 & 31 & 7 & +32 & 10 & s.E. by s. \\ -20 & 44 & 29 & 19 & R. & +32 & 45 & s.s.E. \\ -20 & 31 & 7 & +30 & 18 & s.s.E. \\ -20 & 31 & 7 & +30 & 18 & s.s.E. \\ -20 & 31 & 7 & +30 & 18 & s.s.E. \\ -20 & 31 & 7 & +30 & 36 & s.s.E. \\ -20 & 31 & 7 & +30 & 36 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 37 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 44 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 44 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & +33 & 44 & s.s.E. \\ -20 & 30 & -1 & 26 & +33 & 17 & $	١					-							
$ \begin{vmatrix} 13. & -38 & 11 & 21 & 27 \\ -38 & 20 & 21 & 12 \\ \hline 12. & T. & +31 & 10 \\ +30 & 04 & S.w. & by w. \\ T. & +30 & 20 & S.w. \\ T. & +30 & 20 & S.w. \\ T. & +30 & 20 & S.w. \\ T. & +32 & 30 & S.E. & by S. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & S.E. & by S. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & S.E. & by S. \\ -41 & 32 & 25 & 31 & T. & +32 & 45 & S.S.E. & \frac{1}{2} & S. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & S.S.E. & \frac{1}{2} & S. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & S.S.E. & \frac{1}{2} & S. \\ -43 & 24 & 29 & 19 & R. & +34 & 43 & S.S.E. & \frac{1}{2} & S. & S.E. & \frac{1}{2} & S. & \frac{1}{2} & S. & \frac{1}{2} $			27	07	<i>0</i> 1	an						1 ' 1	
$ \begin{vmatrix} -38 & 20 & 21 & 12 & T. & +31 & 10 & s.w. by w. \\ T. & +30 & 04 & s.w. \\ T. & +30 & 04 & s.w. \\ T. & +30 & 04 & s.w. \\ T. & +30 & 20 & s.w. \\ T. & +30 & 20 & s.w. \\ T. & +30 & 20 & s.w. \\ S.w. & s.w. \\ 15. & -41 & 00 & 22 & 01 & T. & +32 & 30 \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.s. by s. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.s. by s. \\ 16. & -41 & 24 & 24 & 32 & T. & +32 & 45 & s.s. by s. \\ -41 & 24 & 24 & 32 & T. & +32 & 45 & s.s. by s. \\ S. & +31 & 00 & s.w. & s.w. \\ S. & s.e. & by s. & s.s. by s. \\ S. & +31 & 00 & s.s. by s. \\ S. & s.e. & by s. \\ S. & s.s. by s. \\ S. & s. by s. \\ S. &$	ı	19								K			
$ \begin{bmatrix} T. & +30 & 04 & s.w. \\ T. & +30 & 20 & s.w. \\ 30 & 20 & s.w. \\ 15. & -41 & 00 & 22 & 01 & T. \\ -41 & 15 & 22 & 22 & S. \\ 16. & -41 & 24 & 24 & 32 & T. \\ -41 & 32 & 25 & 31 & T. \\ -41 & 50 & 26 & 24 & S. \\ R. & +32 & 41 & s.s.e. \\ R. & +32 & 41 & s.s.e. \\ 17. & -41 & 50 & 26 & 24 & S. \\ 18. & -42 & 54 & 28 & 13 & T. \\ -43 & 24 & 29 & 19 & R. \\ 25. & -46 & 31 & 48 & 03 & R. \\ 28. & -46 & 34 & 52 & 43 & T. \\ \end{bmatrix} \begin{bmatrix} T. & +30 & 04 & s.w. \\ +30 & 20 & s.w. \\ s.s.w. \\ s.s.w. \\ s.s.e. \\ s.s$	١	10.									t .	1 00 00 1	
$ \begin{bmatrix} 14. & -39 & 55 & 20 & 35 & T. & +30 & 20 & s.w. \\ 15. & -41 & 00 & 22 & 01 & T. & +32 & 30 & s.s.w. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.s.e. & by s. \\ 16. & -41 & 24 & 24 & 32 & T. & +32 & 29 & s.s.e. & \frac{1}{2} & E. \\ -41 & 32 & 25 & 31 & T. & +32 & 45 & s.s.e. & \frac{1}{2} & E. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.e. & \frac{1}{2} & E. \\ -41 & 50 & 26 & 24 & S. & +31 & 48 & s.s.e. & s.s.e. & s.s.e. \\ 17. & -41 & 50 & 26 & 24 & S. & +31 & 48 & s.s.e. \\ 18. & -42 & 54 & 28 & 13 & T. & +34 & 27 & s.s.e. & s.s.e. & s.s.e. \\ -43 & 24 & 29 & 19 & R. & +33 & 58 & s.s.e.$	ı		50	20	~1	1~				$  -57 \ 30  $			
$ \begin{vmatrix} 14. & -39 & 55 & 20 & 35 & T. & +29 & 51 \\ 15. & -41 & 00 & 22 & 01 & T. & +32 & 30 \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.e. by s. \\ 16. & -41 & 24 & 24 & 32 & T. & +32 & 09 & s.s.e. by s. \\ 16. & -41 & 24 & 24 & 32 & T. & +32 & 09 & s.s.e. by s. \\ -41 & 32 & 25 & 31 & T. & +32 & 45 & s.s.e. by s. \\ S. & +31 & 00 & s.s.e. by s. \\ S. & +31 & 00 & s.s.e. by s. \\ S. & +32 & 41 & s.s.e. by s. \\ S. & +32 & 41 & s.s.e. by s. \\ S. & +32 & 41 & s.s.e. by s. \\ S. & +32 & 41 & s.s.e. by s. \\ S. & +32 & 41 & s.s.e. by s. \\ S. & +34 & 43 & s.s.e. by s. \\ S. & +34 & 43 & s.s.e. by s. by$	١				,								
$ \begin{vmatrix} 15. & -41 & 00 & 22 & 01 & T. & +32 & 30 & s.e. \ by s. \\ -41 & 15 & 22 & 22 & S. & +31 & 20 & s.e. \ by s. \\ 16. & -41 & 24 & 24 & 32 & T. & +32 & 09 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 24 & 24 & 32 & T. & +32 & 45 & s.e. \ \frac{1}{2} \text{ S.} \\ -41 & 32 & 25 & 31 & T. & +32 & 45 & s.e. \ by s. \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +32 & 00 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +32 & 00 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +32 & 40 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +33 & 44 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +33 & 58 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ \frac{1}{2} \text{ E.} \\ -41 & 28 & 25 & 39 & R. & +34 & 43 & s.s.e. \ $	١	14.	-39	55	20	35				<b>□</b> -59 30			
$ \begin{vmatrix} -41 & 15 & 22 & 22 & S. \\ -41 & 24 & 24 & 32 & T. \\ -41 & 24 & 24 & 32 & T. \\ -41 & 24 & 24 & 32 & T. \\ +32 & 35 & S.E. & \frac{1}{2} E. \\ S. & +31 & 00 & S.E. & by S. \\ S. & +31 & 00 & S.E. & by S. \\ S. & +31 & 00 & S.E. & by S. \\ S. & +32 & 41 & S.E. & by S. \\ S. & +32 & 41 & S.S.E. & by S. \\ R. & +32 & 41 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ T. & +34 & 43 & S.S.E. & by S. \\ T. & +34 & 43 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ S. & +31 & 48 & S.S.E. & by S. \\ S. & +34 & 43 & S.S.E. & by S. \\ $	ı							+32 30		1		1 20 06 1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	١	- 30								> -59 40			
$\begin{bmatrix} T. & +32 & 35 & \text{s.e.} \frac{1}{2} \text{s.} \\ +31 & 00 & \text{s.e.} \frac{1}{2} \text{s.} \\ +32 & 45 & \text{s.e.} \frac{1}{2} \text{e.} \\ R. & +32 & 41 & \text{s.s.e.} \\ +32 & 41 & \text{s.s.e.} \end{bmatrix} = \begin{bmatrix} -62 & 00 & -2 & 17 & +30 & 18 \\ -2 & 03 & +28 & 57 \\ -1 & 46 & +30 & 59 \\ -1 & 24 & +31 & 17 \\ -1 & 24 & +30 & 36 \end{bmatrix} + 30 & 25 \\ -41 & 28 & 25 & 39 & \text{R.} & +32 & 00 & \text{s.s.e.} \\ -41 & 28 & 25 & 39 & \text{R.} & +32 & 00 & \text{s.s.e.} \\ -41 & 50 & 26 & 24 & \text{S.} & +31 & 48 & \text{s.s.e.} \\ T. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +34 & 43 & \text{s.s.e.} \\ S. & +35 & 58 & \text{s.s.e.} \\ S. & +35 & 58 & \text{s.s.e.} \\ 25. & -46 & 31 & 48 & 03 & \text{R.} & +35 & 44 & \text{s.e.} \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & \text{s.w.} \end{bmatrix} = \begin{bmatrix} -62 & 40 & -2 & 17 & +30 & 18 \\ -2 & 03 & +28 & 57 \\ -1 & 24 & +30 & 36 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +34 & 32 \\ -0 & 45 & +32 & 54 \\ -67 & 00 & -3 & 03 & +32 & 41 & +32 & 41 \\ -67 & 20 & +2 & 12 & +33 & 56 \end{bmatrix} = 32 & 28 \end{bmatrix}$	.	16.								К		+30 23	
$ \begin{vmatrix} -41 & 32 & 25 & 31 & S. & +31 & 00 & s.e. by s. \\ -41 & 32 & 25 & 31 & T. & +32 & 45 & s.s.e. \frac{1}{2} E. \\ -41 & 28 & 25 & 39 & R. & +32 & 00 & s.s.e. \\ -41 & 50 & 26 & 24 & S. & +31 & 48 & s.s.e. \\ T. & +34 & 43 & s.s.e. & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ S. & +35 & 58 & s.s.e. & s.s.e. \\ O. & +35 & 58 & s.s.e. & s.s.e. \\ S. & +33 & 44 & s.s.e. & s.s.e. \\ 25. & -46 & 31 & 48 & 03 & R. & +35 & 44 & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.w. \end{vmatrix} $ $ \begin{vmatrix} -62 & 00 & -2 & 03 + 28 & 57 \\ -1 & 46 & +30 & 59 \\ -1 & 24 & +31 & 17 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +34 & 32 \\ -67 & 00 & -3 & 03 + 32 & 41 & +32 & 41 \\ -67 & 00 & -3 & 03 + 32 & 41 & +32 & 41 \\ -67 & 20 & +2 & 12 + 33 & 56 \\ -1 & 26 & +32 & 32 \\ -1 & 26 & +33 & 32 \\ -1 & 26 & +33 & $	ı							$+32\ 35$		-	-2 17	+30 18	
$ \begin{bmatrix} -41 & 32 & 25 & 31 & T. & +32 & 45 & s.s.e. \frac{1}{2} E. \\ -41 & 28 & 25 & 39 & R. & +32 & 00 & s.s.e. \\ -41 & 50 & 26 & 24 & S. & +31 & 48 & s.s.e. \\ T. & +34 & 43 & s.s.e. \\ S. & +34 & 43 & s.s.e. \\ S. & +34 & 43 & s.s.e. \\ O. & +35 & 58 & s.s.e. \\ O. & +35 & 58 & s.s.e. \\ S. & -43 & 29 & 19 & R. & +33 & 58 \\ T. & +33 & 39 & s.by E. \\ 25. & -46 & 31 & 48 & 03 & R. & +35 & 44 & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.w. \end{bmatrix} \begin{bmatrix} -62 & 40 & -1 & 46 & +30 & 59 \\ -1 & 24 & +31 & 17 \\ -1 & 24 & +30 & 36 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 32 \\ -67 & 00 & -3 & 03 & +32 & 41 & +32 & 41 \\ -67 & 20 & +2 & 12 & +33 & 56 \end{bmatrix} \begin{bmatrix} +30 & 23 \\ +31 & 49 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 32 \\ -67 & 00 & -3 & 03 & +32 & 41 & +32 & 41 \\ -67 & 20 & +2 & 12 & +33 & 56 \end{bmatrix} \begin{bmatrix} +30 & 25 \\ -1 & 24 & +31 & 17 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 32 \\ -67 & 00 & -3 & 03 & +32 & 41 & +32 & 41 \\ -67 & 20 & +2 & 12 & +33 & 56 \end{bmatrix} \begin{bmatrix} +30 & 25 \\ -1 & 24 & +31 & 17 \\ -1 & 24 & +30 & 36 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 32 \\ -1 & 26 & +33 $	١						S.	+31 00		60 00	-2 03	$ +28 \ 57 \left( \begin{array}{c} +30 \ 25 \end{array} \right)$	
$\begin{bmatrix} -41 & 28 & 25 & 39 & R. & +32 & 41 & s.s.e. \\ -41 & 50 & 26 & 24 & S. & +31 & 48 & s.s.e. \\ 18. & -42 & 54 & 28 & 13 & T. & +34 & 27 & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ O. & +35 & 58 & s.s.e. \\ O. & +35 & 58 & s.s.e. \\ 25. & -46 & 31 & 48 & 03 & R. & +33 & 44 & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.w. \end{bmatrix} \begin{bmatrix} -1 & 24 + 31 & 17 \\ -1 & 24 + 30 & 36 \\ S.s.e. $	١		-41	32	25	31	Т.	$+32 \ 45$	S.S.E. $\frac{1}{2}$ E.	>-0z 00	-1 46	$ +30 59 ^{+30 25}$	
$ \begin{bmatrix} -41 & 28 & 25 & 39 & R. & +32 & 00 \\ 17 & -41 & 50 & 26 & 24 & S. & +31 & 48 \\ 18 & -42 & 54 & 28 & 13 & T. & +34 & 27 & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ O. & +35 & 58 & s.s.e. \\ O. & +35 & 58 & s.s.e. \\ 25 & -46 & 31 & 48 & 03 & R. & +35 & 44 \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 \end{bmatrix} $ $ \begin{bmatrix} -43 & 24 & 29 & 19 & R. & +33 & 58 \\ T. & +33 & 39 & s. & by & e. \\ S. & -43 & 34 & 52 & 43 & T. & +31 & 44 \end{bmatrix} $ $ \begin{bmatrix} -62 & 10 & -1 & 24 & +30 & 36 \\ -1 & 26 & +30 & 22 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +33 & 37 \\ -1 & 26 & +34 & 32 \\ -67 & 00 & -3 & 33 & 54 \\ -67 & 00 & -3 & 03 & +32 & 41 & +32 & 41 \\ -67 & 20 & +2 & 12 & +33 & 56 \end{bmatrix} $	١							+3241					
$ \begin{bmatrix} 17 & -41 & 50 & 26 & 24 & S. & +31 & 48 & s.s.e. \\ 18 & -42 & 54 & 28 & 13 & T. & +34 & 27 & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ S. & +35 & 58 & s.s.e. & s.s.e. \\ O. & +35 & 58 & s.s.e. & s.s.e. \\ T. & +33 & 58 & s.s.e. & s.s.e. \\ 25. & -46 & 31 & 48 & 03 & R. & +35 & 44 & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.w. \end{bmatrix} \begin{bmatrix} -62 & 10 & -1 & 26 & +30 & 22 \\ -1 & 26 & +33 & 17 \\ -1 & 26 & +33 & 31 \\ -62 & 40 & -1 & 26 & +33 & 37 \\ -1 & 26 & +34 & 32 \\ -67 & 00 & -3 & 32 & 54 \\ -67 & 00 & +35 & 32 & 54 \\ -67 & 20 & +2 & 12 & +33 & 56 \\ -27 & 20 & +2 & +2 & +33 & +33 & +33 \\ -27 & 20 & +2 & +2 & +33 & +33 & +33 \\ -27 & 20 & +2 & +33 & +33 & +33 & +33 \\ -27 & 20 & +2 & +33 & +33 & +33 & +33 \\ -27 & 20 & +2 & +33 & +33 & +33 & +33 \\ -27 & 20 & +2 & +33 & +33 & +33 & +33 \\ -27$	١						R.	+3200	S.S.E.	J	-1 24	[+30 36]	
$ \begin{vmatrix} 18 & -42 & 54 & 28 & 13 & T. & +34 & 27 & s.s.e. \\ -42 & 54 & 28 & 13 & T. & +34 & 27 & s.s.e. \\ S. & +34 & 43 & s.s.e. & s.s.e. \\ O. & +35 & 58 & s.s.e. & s.s.e. \\ O. & +35 & 58 & s.s.e. & s.s.e. \\ T. & +33 & 58 & s.s.e. & s.s.e. \\ 25. & -46 & 31 & 48 & 03 & R. & +35 & 44 & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.w. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.w. & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. & s.e. \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. & s.e. & s.e. \\ 29. & -43 & 24 & 32 & 32 & 32 & 32 & 32 & 32 & $	ı	17.	<del> 4</del> 1	50	26	24		+31 48	S.S.E.	60 10	-1 26	$ +30 \ 22 \  _{+31 \ 40}$	
$ \begin{vmatrix} S. & +34 & 43 \\ O. & +35 & 58 \\ O. & +35 & 58 \\ S.S.E. \\ S.S.$	1			,				+34 43	S.S.E.		-1 26	+ 00 1/ 1	
$ \begin{vmatrix} -43 & 24 & 29 & 19 & R. & +35 & 58 & s.s.e. \\ 25 & -46 & 31 & 48 & 03 & R. & +35 & 44 & s.e. \\ 28 & -46 & 34 & 52 & 43 & T. & +31 & 44 & s.e. \\ \end{vmatrix}                                 $	ı	18.	-42	<b>54</b>	28	13					$ -1 ^{26}$	+33 01	
$ \begin{bmatrix} -43 & 24 & 29 & 19 & R. & +33 & 58 \\ T. & +33 & 39 & s. s. E. \\ 25. & -46 & 31 & 48 & 03 & R. & +35 & 44 \\ 28. & -46 & 34 & 52 & 43 & T. & +31 & 44 \end{bmatrix}                                $	1								i .	$  > -62 \ 30$			
$ \left[ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		ü		٠.			i		l .	اِ			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	-		-43	24	29	19				$\frac{1}{1}$ -62 40			
$\begin{bmatrix} 28 & -46 & 34 & 52 & 43 & T. &   +31 & 44 & N.W. &   \end{bmatrix}$ $\begin{bmatrix} 67 & 20 &   +2 & 12 &   +33 & 56 \\ & & & & & \end{bmatrix}$	-	0.5	AC	91	40	00				1 1		+ 32 34	
$\left \begin{array}{c cccccccccccccccccccccccccccccccccc$									!	15	-3 U3	1.00 *()	
1.   +01 00   N.N.W.   J   +1 0/ +00 00 J		28.	-40	54	52	40			l .	$  \ \rangle -67 \ 30$	+ 2 12	$\begin{vmatrix} +33 & 30 \\ +33 & 00 \end{vmatrix} + 33 & 28 \end{vmatrix}$	
							1.	+91 99	N·N·W·	J	+ 1 0/	T 99 00 J	

## Observations of Declination. (Continued.)

Date.	Lat.	Long.	Observer.	Declination observed.	Ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Remarks.
1840. April 30. May 1. 2.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	52 01 56 17 56 28	R. S. T. R.	+31 40 +37 06 +36 34 +33 48 +33 34 +32 21	N. by E. ½ E. S.E. S.E. S.E. S.E.	$ \begin{cases} -67 & 30 \\ -67 & 50 \end{cases} $	$ \begin{array}{c cccc} + & & & 53 \\ -3 & & 07 \\ -3 & & 07 \\ -3 & & 07 \\ -3 & & 07 \\ -3 & & 15 \end{array} $	$ \begin{vmatrix} +32 & 33 \\ +33 & 59 \\ +33 & 27 \\ +30 & 41 \\ +30 & 27 \\ +29 & 06 \end{vmatrix} +30 & 00$	
	<b>-47</b> 18		S.	$\begin{vmatrix} +32 & 10 \\ +30 & 00 \\ +31 & 50 \\ +30 & 32 \\ +29 & 39 \end{vmatrix}$	s.e. by e. ½ e. s.e. by e. ½ e. s.e. by e. ½ e. s.e. by e. ½ e. s.e. by e. ½ e.		-3 15 -4 41	$\begin{array}{c} +29 & 00 \\ +28 & 55 \end{array} + 29 & 00 \\ +25 & 38 \end{array}$	
31. Aug. 2. 4.		113 49	T. T.		s.e. by E. $\frac{1}{2}$ E.		-5 10 $-5 49$	+18 59 +11 29	
	<b>—46 36</b>		R. R. T. T. T. R.	$ \begin{vmatrix} +15 & 11 \\ +15 & 39 \\ +1 & 58 \\ +3 & 44 \\ +3 & 08 \\ +5 & 43 \\ +5 & 58 \end{vmatrix} $	E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ S. E. $\frac{1}{2}$ N. E. by N. E. $\frac{1}{2}$ N. E. $\frac{1}{2}$ N.		-5 51 -5 35 -5 27 -5 35 -5 35 -5 43	+ 9 34	
	-46 13 -46 06	132 00 132 12	R. R. R. R. R. R.	$ \begin{vmatrix} + 6 & 30 \\ + 4 & 29 \\ + 5 & 16 \\ + 2 & 09 \\ + 6 & 17 \\ + 6 & 53 \\ + 7 & 25 \\ - 3 & 06 \end{vmatrix} $	E. E. E. \frac{1}{2} N. E. \frac{1}{2} N. E. \frac{1}{2} N.	$\left. \begin{array}{c} \\ \\ \\ \end{array} \right. = 75  00$	-5 43 -5 43 -5 43 -5 35 -5 35 -5 35 0 00	\[ \] \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
10.	<b>—44 23</b>	141 11		- 4 19 - 3 12 - 3 12 - 4 01 - 3 39 - 4 24 - 2 01	E.N.E. E.N.E. E.N.E. E.N.E. E.N.E. E.N.E.	\bigg\}-73 00			

The observers are distinguished by their initials as follows:-

R., Sir James Ross; S., Lieut. Sibbald; T., Mr. Tucker, Master; O., Mr. Oakley, Mate.

Observations of the Magnetic Inclination taken on board Her Majesty's Ship Erebus, by Captain Sir James Clark Ross, with Needle F. 1., between the Cape of Good Hope and Kerguelen Island.

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's	l	Corrected Inclination.	Remarks.
			. 62			attrac- tion.	Index.		
1840. April <b>7.</b>	$-3\overset{\circ}{5}\ 1\overset{\prime}{4}$	18 04	Direct.	$-5\mathring{4}$ 23	s. by E.	.,	,	) ° ′	
-			S.	-54 30	-	-04	-2.0	$\left.\right\}$ -54 32	
8.	-35 48	18 47	Direct. S.	$\begin{vmatrix} -54 & 34 \\ -54 & 39 \end{vmatrix}$	E.S.E.	+23	-2.0	-54 18	
			Direct. S.	$-54 38 \\ -54 47$	w. by s.	7 20			
9.	-36 00	19 00	Direct.	$     \begin{array}{r rrr}     -55 & 42 \\     -56 & 10     \end{array} $		+34	-2.0	$\left55 \ 24 \right $	
10.	-36 07	20 55	Direct. S.		s.e. by s.	+02	-2.0	$\left55 50 \right.$	
11.	-3629	21 16	Direct.	$ -55 \ 30 $	s.			}	
	•		s.n.	$\begin{bmatrix} -55 & 36 \\ -55 & 26 \end{bmatrix}$		-10	-2.0	$-55 \ 38$	
12.	-37 19	21 37	N. Direct.		s.			1	
			S. Direct.	$\begin{bmatrix} -56 & 01 \\ -55 & 42 \end{bmatrix}$		-10	-2.0	>-56 03	
			S. Direct.	-56 11 $-55$ 56					
13.	-38 11	22 00	Direct.	$-55 \ 41$ $-56 \ 09$	w.s.w.	+22	-2.0	$\left.\right\} -55 \ 35$	Much motion.
14.	<b>-40 05</b>	20 38	S. Direct.	-56 27	s.s.e.	-08	-2.0	$\left.\right\} -56 \ 33$	
15.	-40 29	22 22	S. Direct.	$\begin{vmatrix} -56 & 19 \\ -57 & 13 \end{vmatrix}$	s.e. by s.	-06	-2.0	$\left.\right\} -57 28$	
16.	-41 24	25 00	S. Direct.	$\begin{vmatrix} -57 & 28 \\ -58 & 00 \end{vmatrix}$	s.e. by s.		, .		
4.			S. S.N.	$\begin{bmatrix} -58 & 24 \\ -58 & 11 \end{bmatrix}$		-08	-2.0	<b>-58 21</b>	
17.	-41 47	26 38	N. Direct.	$\begin{bmatrix} -58 & 11 \\ -58 & 22 \end{bmatrix}$	S.S.E.	,,	2.0	ll	
	<b>-43 02</b>		S. Direct.	$     \begin{array}{r rrr}     -58 & 31 \\     -59 & 01   \end{array} $	s.s.e.	-15	-2.0	$\left.\right\} -58  43$	
			S.	-59 20	5.5.2.	-19	-2.0	$\left.\right\}$ -59 31	
	<b>-43 07</b>	28 43	S.N. N.	$\begin{vmatrix} -59 & 20 \\ -59 & 21 \end{vmatrix}$		-20	-2.0	<b>-59 37</b>	
19.	-44 19	31 06	Direct. Direct.	$     \begin{array}{r rrr}     -59 & 05 \\     -60 & 30     \end{array} $	s. by E.	-29	-2.0	$\left.\right\} -60 52$	
20.	-45 40	34 08	S. Direct.	$\begin{vmatrix} -60 & 13 \\ -61 & 41 \end{vmatrix}$	S.S.E.	-30	-2.0	$\begin{cases} -62 & 23 \end{cases}$	-
21.	<b>-46 59</b>	37 14	S. Direct.		s.e. by s.			١	
			S. Direct.	$ \begin{array}{rrr} -63 & 32 \\ -63 & 52 \end{array} $	s.e. by s.	-28	-2.0	$\left.\right\}$ -64 00	·
	-46   46		S. Direct.	$ \begin{array}{r rrrr} -64 & 06 \\ -64 & 59 \end{array} $	s.e. by s.	29	-2.0	$\left.\right\} -64,30$	Much motion.
20.	30 30	TW 20	$\mathbf{S}.$		Demony Se	-32	-2.0	-65 47	mauch Houvile
24.	<b>-47 01</b>	46 10	Direct. Direct.	-66 18	S.E. ½ E.	-15	-2.0	$\left.\right\} -66 \ 36$	Very steady.
26.	<b>-46 41</b>	50 52	S. Direct.	$ \begin{array}{r rrrr} -66 & 20 \\ -67 & 00 \end{array} $	s.e. by s.	-36	-2.0	$\left.\right\}$ -67 41	
28.	-46 28	52 31	S. Direct.	$\begin{vmatrix} -67 & 06 \\ -67 & 31 \end{vmatrix}$	w.s.w.		-2·0	1	
			S.	-67 32		+03	-2.0	$\left  \begin{array}{c} -67 & 30 \end{array} \right $	

Observations of the Magnetic Inclination. (Continued.)

						Corre	ctions.		
Date.	Lat.	Long.	Method employed.	Observed Inclination.	Ship's head.	Ship's attraction.	Index.	Corrected Inclination.	Remarks.
1	$-46^{\circ} 28^{\circ}$ $-46^{\circ} 17^{\circ}$		Direct. S. Direct.	$\begin{bmatrix} -67 & 11 \\ -67 & 21 \\ -66 & 20 \end{bmatrix}$	s.w. by w.	-11 -45	-2·0 -2·0	$\left. \begin{array}{c} 0.00000000000000000000000000000000000$	
May 1.	<b>-46</b> 25	52 01	S. Direct. S. S.N.	$ \begin{array}{rrrr} -66 & 27 \\ -66 & 26 \\ -66 & 39 \\ -66 & 40 \end{array} $	s. by E. ½ E.	-47	-2.0	$\left.\right\}$ -67 30	
	-46 57 $-47 19$		N. Direct. S. Direct.	$ \begin{array}{rrrr} -67 & 00 \\ -67 & 37 \\ -67 & 51 \\ -68 & 19 \end{array} $	S.E.	-26	-2.0	$\left. \begin{array}{c} \ \ \ \end{array} \right\} -68   12  \left. \begin{array}{c} \ \ \ \end{array} \right.$	
			S. S.N. N.	$ \begin{vmatrix} -68 & 27 \\ -67 & 59 \\ -68 & 09 \end{vmatrix} $		-27	-2.0		
4.	-•		Direct.	$ \begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	S.E.	-28	-2.0	$\left  \right\} - 69 37$	
7.			Direct.	$\begin{vmatrix} -71 & 23 \\ -71 & 36 \\ 60 & 19 \end{vmatrix}$	N.N.W.	+69	-2.0	<b>}</b> −70 12	
	-48 36	3 11 , .	Direct.	$ \begin{array}{c cccc} -69 & 12 \\ -69 & 25 \\ 60 & 10 \end{array} $	s.w. by s.	-42	-2.0		
	-48 24 48 40		Direct. S.	-69 28	s.w.byw. <u>1</u> w.	-08	-2.0	$\left.\right\} -69 \ 33$	
12.	-48 40	US 38	Direct. S. Direct. S.	$ \begin{array}{rrrr} -71 & 47 \\ -72 & 03 \\ -69 & 46 \\ -69 & 59 \end{array} $	N. s.w.byw. <u>1</u> 2w.	-72 -08	-2·0 -2·0		

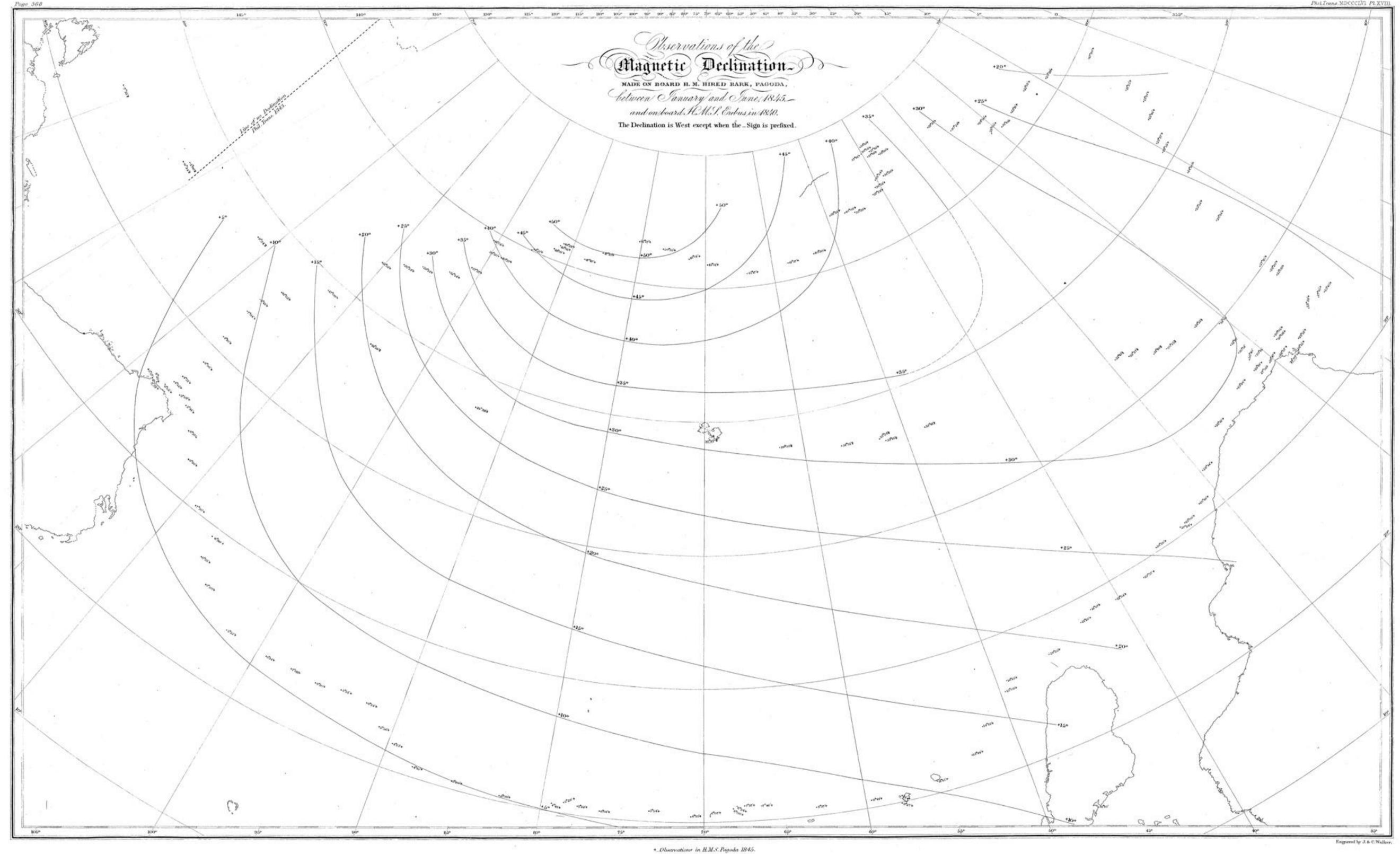
Abstract of Observations of the Magnetic Force between the Cape of Good Hope and Kerguelen Island, made in Her Majesty's Ships Erebus and Terror in 1840\*.

Posi	tion.	Inter	nsity.	Posi	tion.	Intensity.	
Lat.	Long.	Cape = 0.981.	Cape =1.000.	Lat.	Long.	Cape = $0.981$ .	Cape = 1.000.
-34 11 -37 44 -35 14 -36 04 -37 16 -36 16 -36 52 -36 11 -35 48 -38 47 -36 35 -40 05 -40 45 -38 13 -42 40 -41 24 -42 56 -40 29 -41 58 -44 28	18 26 16 36 18 27 19 19 17 24 20 04 18 25 20 42 18 47 17 00 21 20 17 26 20 38 19 20 21 30 22 02 25 00 23 12 22 22 26 38 24 55	0.981 0.983 0.984 0.988 0.989 0.995 0.996 0.997 0.998 0.999 1.010 1.020 1.021 1.036 1.045 1.058 1.063 1.073 1.079 1.088 1.096	1.000† 1.003 1.004 1.008 1.009 1.015 1.016 1.017 1.018 1.019 1.030 1.040 1.041 1.057 1.066 1.079 1.084 1.100 1.110 1.118	-43 07 -47 00 -45 44 -46 45 -47 00 -47 00 -47 50 -47 01 -46 41 -46 28 -46 29 -46 25 -46 57 -46 18 -47 19 -47 41 -48 41 -48 39 -48 36	28 43 38 48 34 16 40 05 37 14 43 48 42 41 45 20 46 10 50 52 52 43 52 26 52 01 55 39 52 04 59 10 62 59 68 54 68 57 69 07	1·134 1·170 1·171 1·183 1·186 1·230 1·232 1·261 1·269 1·277 1·288 1·314 1·323 1·326 1·328 1·377 1·459 1·465 1·471 1·488 1·489	1·157 1·193 1·194 1·206 1·209 1·255 1·257 1·286 1·294 1·302 1·316 1·340 1·349 1·352 1·354 1·404 1·487 1·493 1·499‡ 1·517 1·518
$ \begin{vmatrix} -46 & 41 \\ -46 & 00 \\ -44 & 19 \end{vmatrix} $	29 00 26 12 31 06	1·122 1·128 1·131	1·144 1·150 1·154	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	69 21 69 52	1·490 1·497	1·520 1·527

<sup>\*</sup> Philosophical Transactions, 1842, p. 41. † On she

<sup>†</sup> On shore in Simon's Bay.

<sup>‡</sup> On shore at Kerguelen Island.



Observations in the Pagoda
Expedition of Sir J. C. Ross
by Lieu! A. Smith R.N.
by Lieu! J. Dayman R.N.